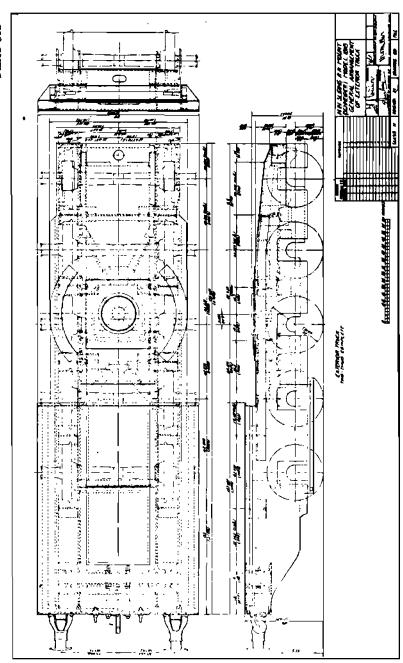
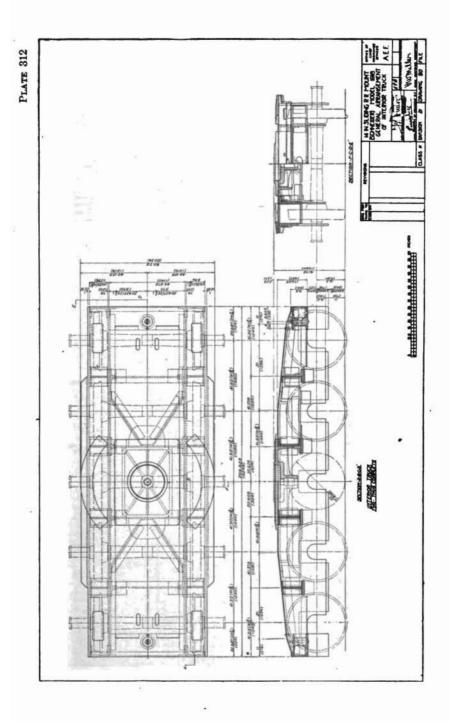
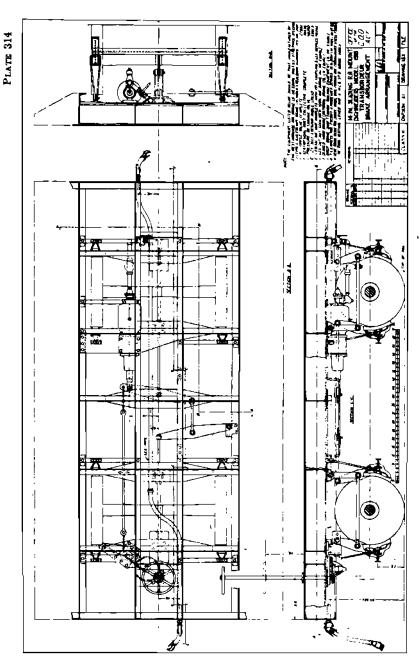


PLATE 308 SECTION 12 PLATE 309 CAN LEANS SCRIV JKK







181768—21——26

13.—AMERICAN 14-INCH GUN ON SLIDING-TYPE BAILWAY MOUNT, MODEL 1919.(26)

265. This is the alternate design that was made up in France in 1918 for 14-inch, 50-caliber guns. As noted under the description of the model 1918 design, this mount was so designed as to contain a maximum of steel castings. The truck frames, span bolsters, sleeper housings, etc., are all steel castings. The decision to attempt to make these very large parts in the form of castings was the result of difficult manufacturing conditions prevailing in America at that time. It was felt that time could be saved and better results secured from the use of steel castings than from similar parts made of structural steel. Circumstances connected with this mount are mentioned in the description of the model 1918 mount. General views are given on plates 317 to 320.

266. Gun.—The gun employed with this mount is the 14-inch naval rifle, Mark V, Modification I, of 50-caliber length. It is identical in all of its details with the gun described under the model 1918 design.

267. RECOIL MECHANISM.—No recoil mechanism, as it is ordinarily understood, is used in this mount. When the gun is fired, the shock of recoil is transmitted by the trunnions directly into the car body and the entire mount slides back on the track, being stopped by the friction between the sleepers in the bottom of the car and the special firing beams laid on the ties.

268. ELEVATING MECHANISM.—The elevating mechanism provides for a movement of the gun from the loading angle, 0 degree to 38 degrees. It consists of a circular rack bolted to the counterweight on the breech end of the gun, plate 321, a pinion meshing with it and two spur gears, a slip-friction device, a wormwheel and worm, and miter gears on a cross-shaft mounting handwheels on each side of the car body. A chain drive extends from the worm shaft to a 7½-horsepower electric motor and a clutch is provided so that the handwheel does not rotate when the motor is being used. When operated by hand, one revolution of the handwheel moves the gun through 20 minutes in elevation. An antifriction device, of the design shown on plate 322, is provided on the trunnions to reduce the effort required in elevating and depressing the gun. This design is the same in principle but differs slightly in its details from that of the model 1918 mount.

269. Traversing Mechanism.—It is necessary to operate this mount on a curved track to secure a wide range of traverse. It is possible to traverse the car body on span bolsters by a mechanism, the design of which is shown on plates 323 and 324, and the location and general arrangement of which is shown on plates 319 and 320. Through this mechanism it is possible to secure a traverse of 2.5 degrees on each side of the center line. Attention is invited to the differences in the details of design between this mechanism and the

traversing mechanism for the model 1918 mount. Electric-translating mechanisms are mounted on the two outside trucks and each consists of a 25-horsepower motor connected through spur and bevel gears and two sets of reducing gears to a crank shaft on the outer end of the truck. From the crank pins on this shaft-connecting rods extend on each side to three of the five axles, plates 325 to 327.

270. Gun Carriage.—The gun carriage is incorporated with the car body and the two are described together in the next paragraph.

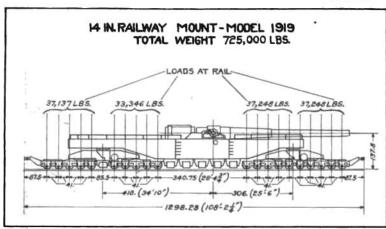
271. CAR BODY.—The car body consists of two structural-steel box girders connected by heavy deck plates and a series of structural and cast steel transoms, plates 328, 329, and 330. One of the essential differences between the design of these girders and the girders of the 1918 model is that provision was made for a maximum of machine riveting. The 1918 model follows more nearly the French design and requires considerable hand riveting. Another apparent difference is in the scheme of bracing the trunnion bearings. The trunnion bearings on this mount are braced at the rear by extensions of the web plates passing through slots in the top cover plates. Special center-pin castings of large size form the pivots for the span bolsters at either end.

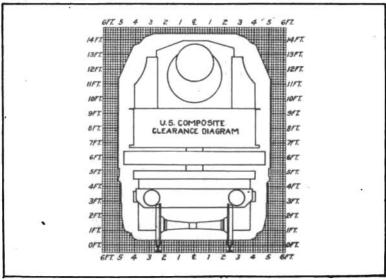
272. ANCHORAGE.—The scheme of anchoring this mount is identical with that described under the previous mount and for the 10-inch and 12-inch mounts as well. Eight lines of 10-inch, 40-pound 1-beam bearing stringers are laid on the ties and the weight of the mount rests on these through five sleepers. The sleeper under the rear span bolster receives its main load on the firing of the gun and prevents excessive stressing of the trucks. To facilitate manufacturing of the girders, the sleepers are carried in castings instead of between extensions of the web of the side girders, as is the case with the model 1918 mount. The design of the jack castings, jacks, and sleepers is shown on plates 331 and 332. It will be observed on plate 343 that the rear span bolster sleeper bears directly on the rails through steel shoes and does not rest on the 1-beam stringers.

273. TRUCKS.—The trucks are special five-axle locomotive type with 6.5 by 12 inch inside journals, 28-inch cast-steel wheels, and cast-steel side frames and transoms. Hand and air brakes are installed on the exterior trucks, plate 333. The car body is supported on these four trucks by means of cast-steel bolsters of a design shown on plate 334. The traversing mechanism already described is installed in the span bolsters.

274. Ammunition Supply System.—Ammunition is supplied from the ammunition car to the mount by a shuttle car or transbordeur identical in design with that described for the model 1918 mount. The same design of jib crane, shell tray, and track are likewise used. This gun loads at 0 degree elevation. It will be remembered that the model 1918 loads at plus 1 degree 30 minutes elevation.

PLATE 316





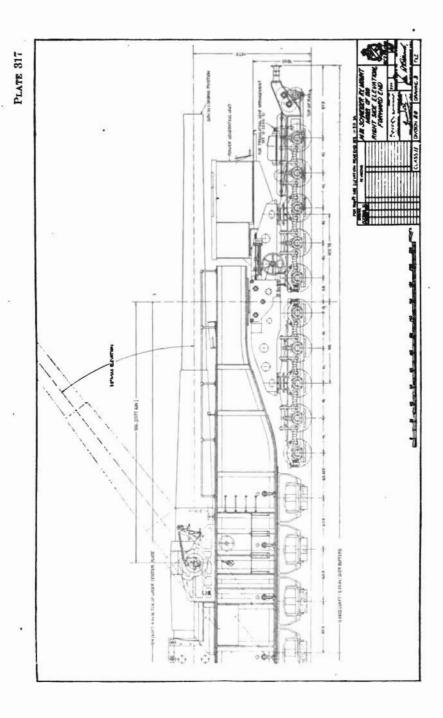
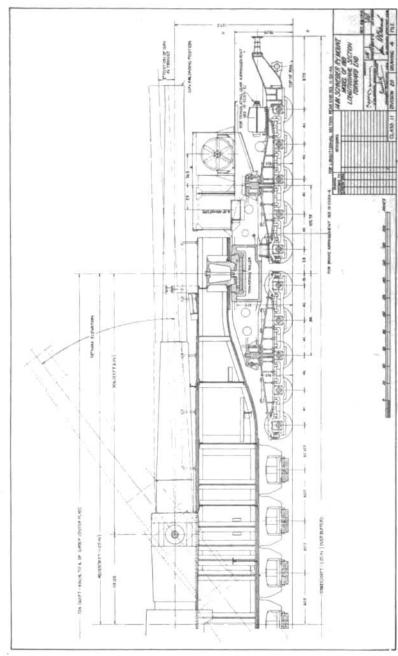
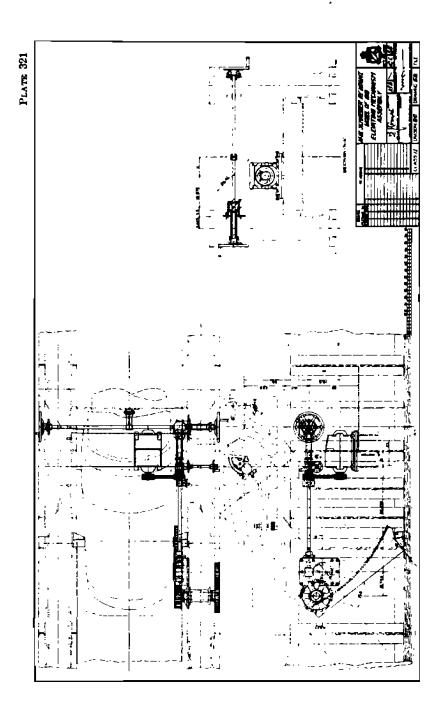
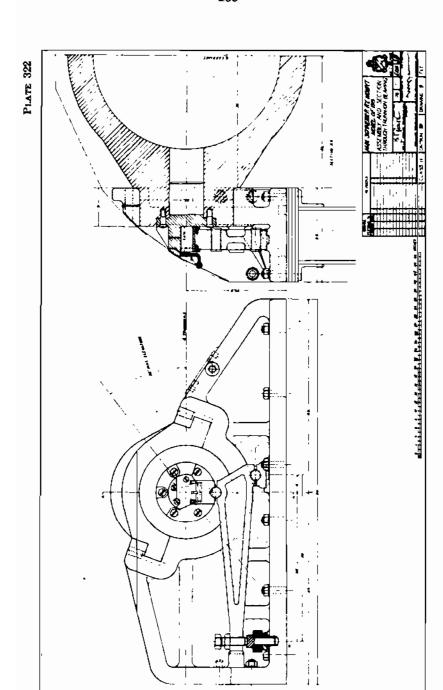


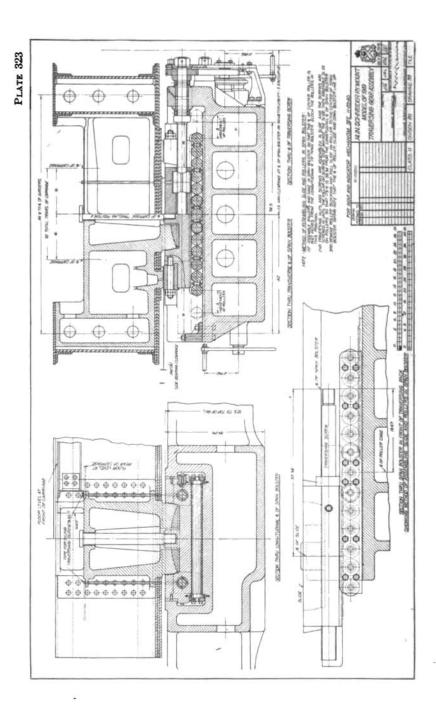
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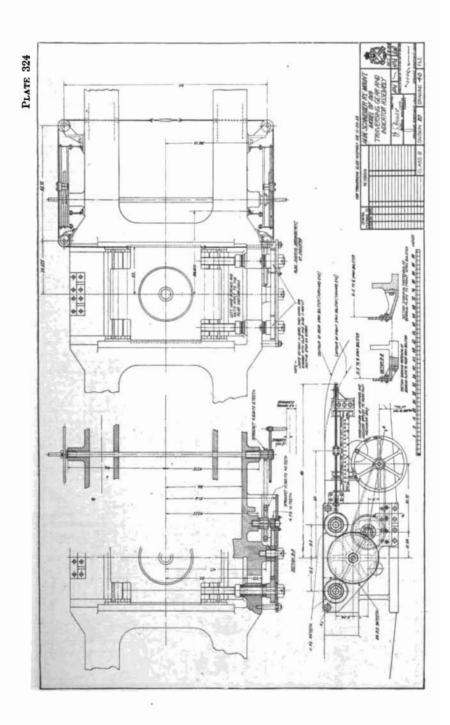


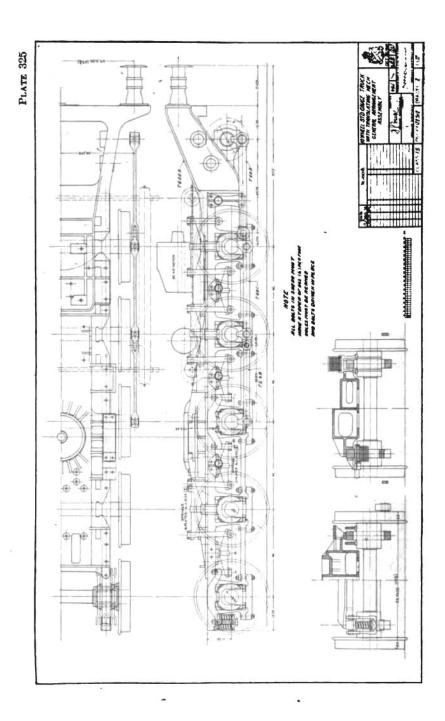


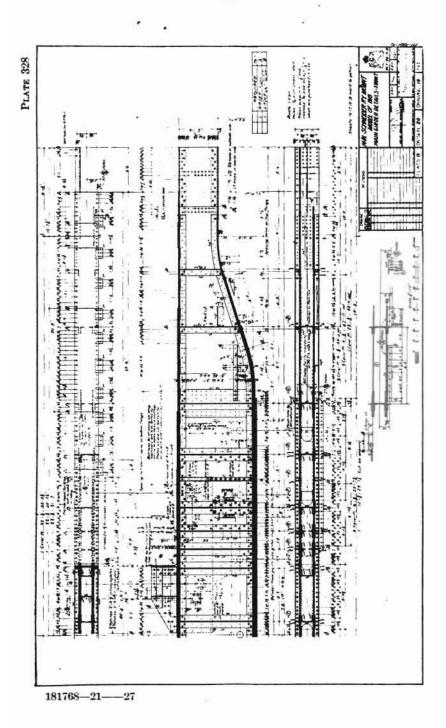


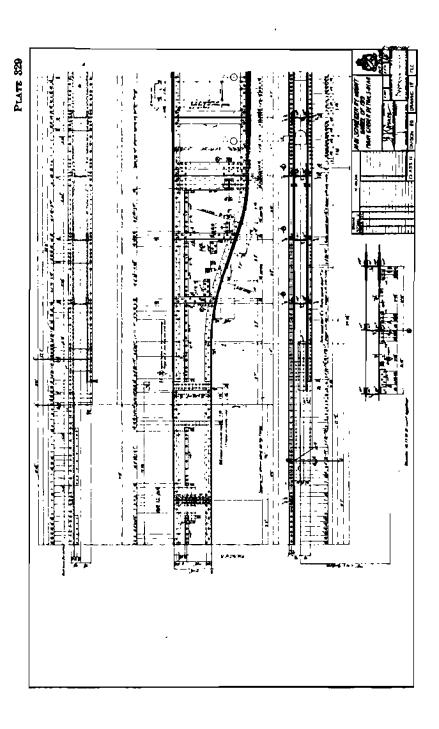


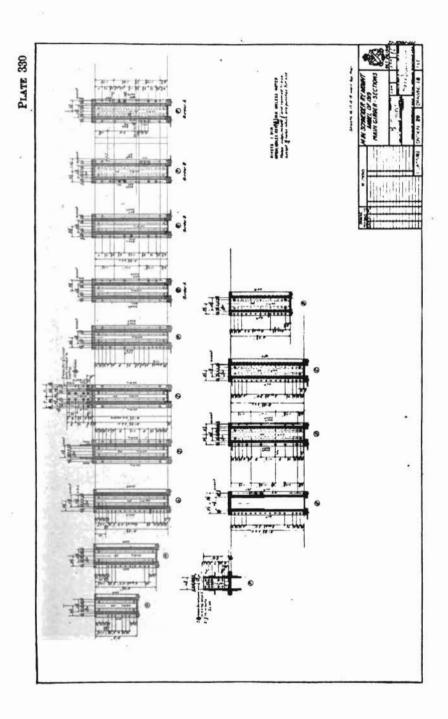


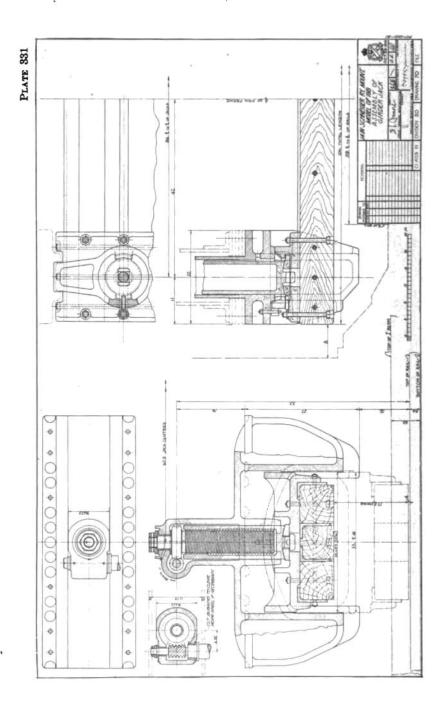


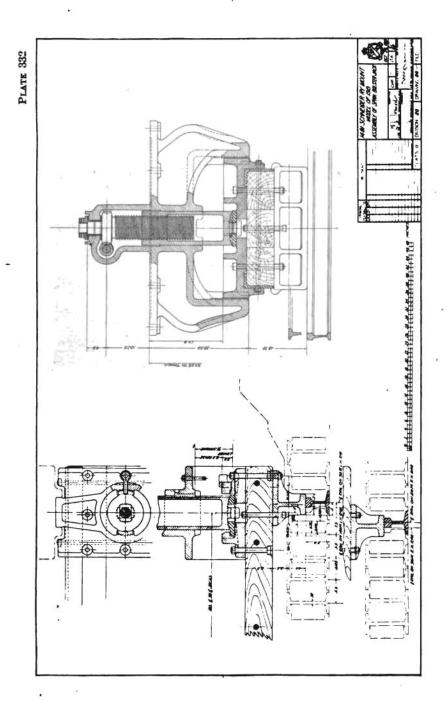


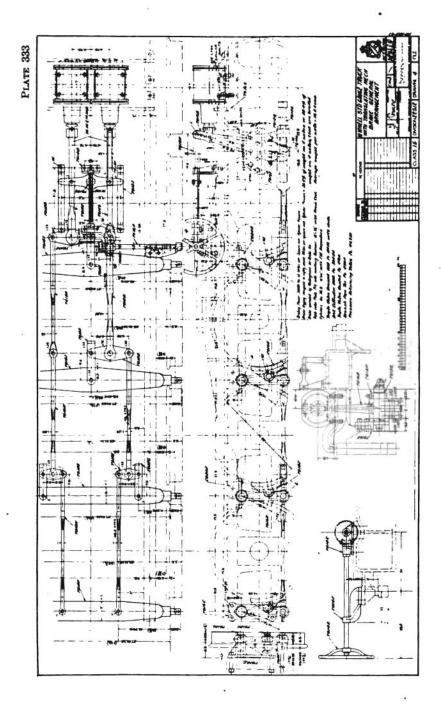


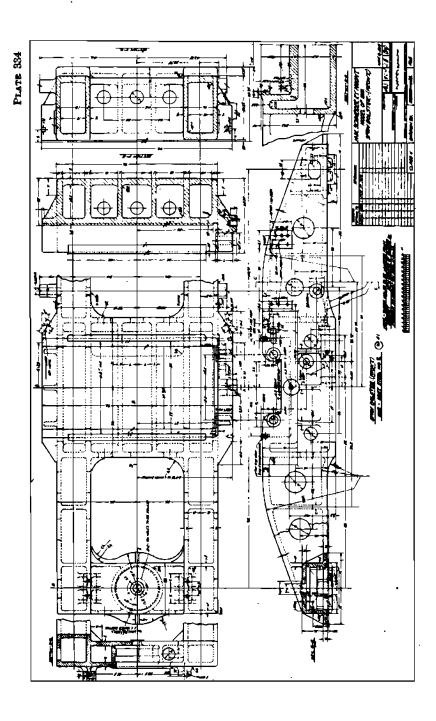












14.—AMERICAN 16-INCH HOWITZER ON RAILWAY MOUNT, MODEL E. (27)

275. The design of this mount was begun in 1915 at about the time the design for the 4.7-inch howitzer was being completed. In other mounts already described it has been clear that the design has been effected quite largely by French and British development in this type of artillery. The designs for the 4.7-inch gun, the 14-inch gun, model E carriage, and the 16-inch howitzer model E carriage were all designed before American Ordnance engineers had had the opportunity to study any European designs or to learn anything about their developments. It is very gratifying that these designs, especially the 14-inch model E embody features which were considered quite admirable and indicated considerable progress by European designers even at the close of the war.

276. The design of the 16-inch model E carriage was completed in September, 1916, and the work of manufacturing was well underway before America entered the war. A number of characteristics in this design point to a lack of comprehension of the possibility of the railway type of artillery and indicate likewise that the work of design on railway mounts was at the beginning of its development. Apparently it was not realized that it was desirable to avoid the necessity for digging a pit 90 inches deep for the gun to recoil in. trunnions of the gun cradle, which is the same as the cradle used in the 1918 carriage, might have been mounted at such a height as to reduce the depth of the pit to 2 feet. The other characteristic in mind is the use of so clumsy a device as the radial truck frames for attaching the traversing rollers to the mount. In spite of these obvious defects the carriage stands in point of possibilities for both field and coast service as practically equivalent to the most modern designs in that its emplacement can be installed in a moderate length of time; it can be traversed in any direction from any position, and the howitzer can be operated to a maximum elevation of 65 degrees. General views of the howitzer as it arrived from the arsenal for proving are shown on plates 335 to 339. The general design of the carriage is shown on plates 340, 341, and 342.

277. Gun.—The gun used with this mount is the 16-inch howitzer, model 1918, Mark I, of 18-caliber length. It is carried on the mount in a cradle containing the hydraulic recoil mechanism and spring recuperator system. The gun is fitted with splines which slide in spline ways in the cradle to prevent rotation of the gun. It is rifled with 144 grooves which twist to the right at a pitch increasing from one turn in 40 calibers to one turn in 20 calibers. It is provided with an interrupted thread breech block, which is fitted with a mechanical firing mechanism.

278. RECOIL MECHANISM.—The recoil mechanism is of the hydrospring type and comprises two hydraulic recoil cylinders mounted at the top and bottom of the cradle in the center, and four spring recuperator cylinders, mounted two above and two below. The

design of the spring recuperator cylinders, as well as the recoil cylinders, is shown on plate 343. The recoil and recuperator systems of the two carriages, models E and 1918, are identical. On plate 362, a by-pass tube can be seen connecting the front end of the buffer with the rear of the recuperator cylinder. A similar by-pass is provided on the lower cylinder. These by-passes are provided for the purpose of adjusting the length of recoil for various weights of projectiles and powder charges. The maximum length of recoil is 48 inches.

279. ELEVATING MECHANISM.—Elevation is provided from 0 degrees, the loading angle, to plus 65 degrees. The mechanism comprises two segmental circular worm racks attached to the sides of the cradle, Hindley worms, miter gears and bevel gears leading to the cross shaft mounting handwheels on either side of the car. The design of this mechanism is shown on plate 344. To reduce the effort required in elevating and depressing the gun, the trunnions of the cradle are provided with antifriction devices of the rolling wedge or knife-edge type, plate 345. This same design of antifriction device has been used on the 14-inch gun carriage, model E and the two 14-inch naval carriages Marks I and IJ. One turn of the handwheel moves the gun through 1 degree in elevation.

280. Traversing Mechanism.—The gun and cradle are fixed with respect to the car body and it is necessary to rotate the entire mount to train the gun in azimuth. The gun and carriage rest by means of 16 rollers carried in radial truck frames, plate 346, on curved railway rails attached to the base ring, plate 341. On either side of the mount, plate 342, identical traversing mechanisms rest on the curved rails of the base ring by means of four rollers and are attached to the mount by means of tie-rods. In each of these a vertical shaft carrying a pinion at its lower end meshing with the traversing rack is driven by two handles through bevel gears. As the mechanism was originally designed, one turn of the crank traversed the gun through 5.75 degrees. This ratio was so high as to make it practically impossible for four men to traverse the mount. The mechanism has been modified and the ratio is now one turn of the handwheel to 0.5 degree in azimuth.

281. Gun Carriage.—The gun carriage is incorporated with the car body and will be described in the next paragraph.

282. CAR Body.—The gun with its cradle is supported directly by means of the cradle trunnions in cast-steel bearings bolted to the inside of the side girders of the car. The car body is made up of two single web structural steel girders connected, by cast-steel transoms at the ends, and by a cast-steel yoke in the center, plate 347. The cast-steel transoms at the ends serve likewise as body bolsters and carry the body center plate which rests in the center plate of the truck. Examination of the top view, on plate 345, gives one the impression that the girders are not sufficiently braced with transoms and deck plates. It is probable that some weaving of the side girders will be experienced in traveling and consequent difficulty in the operating

of the elevating mechanism, similar to that experienced in the 12-inch, 50-caliber, mount may be the result.

283. Anchorage.—The scheme of emplacing the mount is shown on plates 348, 349, and 341. A conical pit 90 inches deep by 192 inches in diameter at the top and 70 inches in diameter at the bottom must be dug to receive the gun in recoil. A circular trench must likewise be prepared about this pit to receive the base ring. The base ring is cast steel and is made in four parts, plates 350 and 351. This base ring may be carried in four parts in an ordinary flat car or in halves in a special flat car, as shown on plate 348. Seats are machined on top of the base ring for two complete circles of standard 80-pound rails. On the inside of each of the quarter sections are two lugs, the one which serves as an attachment for the lifting beam and the other supports one of the I-beam stringers which carry the service rails used in placing the mount on the emplacement. Timber supports are placed in the conical pit and two I-beam stringers carrying railway rails are placed across the pit, resting on the lugs just mentioned and on the timber support on the center. The traversing rack of each quarter section, plate 350, is cut in order that short sections of rail may be laid across the ring. Small sections of traversing rack are bolted into these openings to complete the rack when the mount has been set in place.

284. Four radial truck frames of a design shown on plate 346, two with inclined top surfaces and two with horizontal top surfaces and each containing four rollers, are placed on the base ring on either side of the mount. Key plates are provided on the inclined surfaces of the lower cords of the side girders forward of the center to receive the forward truck frames. The mount is raised about an inch by means of four hydraulic jacks under the ends of two H beams placed between the car body and the trucks as far forward and back as possible and the trucks removed. The radial trucks are then run under, the mount lowered and bolted to them. Cast-steel transoms connect the radial trucks in pairs and outside clips on the trucks engage with the outside of the traversing rack to prevent overturning of the mount in firing, plate 341. The traversing trucks, which have been placed on the base ring by means of the crane, are now connected to the mount by means of tie-rods. The base ring is placed on well-tamped earth or preferably on a bed of good rock ballast. A minimum of 11 days is probably required for the preparation of the pit and the placing of the mount ready for firing.

285. TRUCKS.—The trucks are two in number and of standard M. C. B. design. Each has three axles with 6 by 11 inch journals and 28-inch wheels. The trucks are equipped with both hand and air brakes.

286. Ammunition Supply System.—On the rear of the mount a structural steel frame has been constructed to carry the I-beam track for the ammunition trolley, plates 336 and 340. This I-beam track can be slid to the rear so that it overhangs the track for a considerable

length and the projectile can be picked up either from the track or from a flat car at the rear. No special scheme has been worked out for placing the ammunition at the rear of the mount, but it is assumed that it would be supplied in the standard 8-inch type of ammunition car, plate 106, with special fixtures for 16-inch projectiles, and that it would probably be placed from this ammunition car on a narrow-gauge truck running to the rear of the mount. A special tray has been provided, plate 341, by means of which the projectiles can be carried to the breech of the gun and rammed from it. The powder charge is conveyed to the gun in the same manner.

287. MAINTENANCE.—It is not anticipated that any difficulties would be experienced in the maintenance of this mount. All of its parts are certainly sufficiently sturdy to stand the service for which it was intended. If any difficulty will be experienced it will be in

the service rather than in the maintenance of the mount.

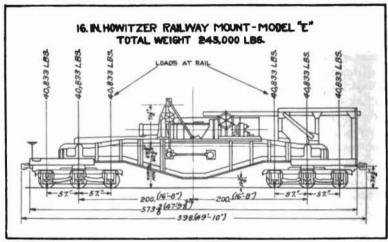
288. DIFFICULTIES INVOLVED IN SERVICE.—The necessity, for preparing so deep a pit to receive the gun in recoil can be classed as a difficulty involved in service of a railway mount. In the event that it is not found possible to operate with the base ring on tamped earth or ballast it becomes necessary to use concrete. This will also be classed as a difficulty in service, because in the European war it was found exceedingly difficult to secure a supply of cement for such uses on the front. It has not been determined whether the noticeable lack of bracing between the side girders will result in difficulties in the operation of the elevating mechanism. This is entirely possible, since the construction is somewhat similar to that of the 12-inch, 50-caliber gun mount on which serious difficulties have been experienced with the elevating mechanism.

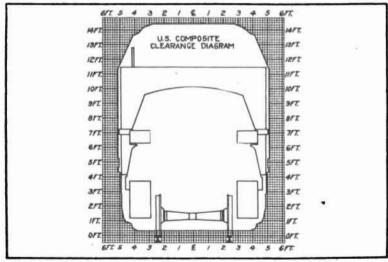
289. Merits.—The possibilities of operating this mount at an elevation as great as 65 degrees and in any direction from any position on the emplacement may be classed as merits. It will be remembered that the necessity for constructing a long curved track to secure sufficient traverse of the gun has been classed as a difficulty involved in service. Such an emplacement as this can be concealed perfectly while the curved track can not. The ammunition supply system may likewise be considered satisfactory in that it is quite simple in design and operates entirely by hand without any difficulty.

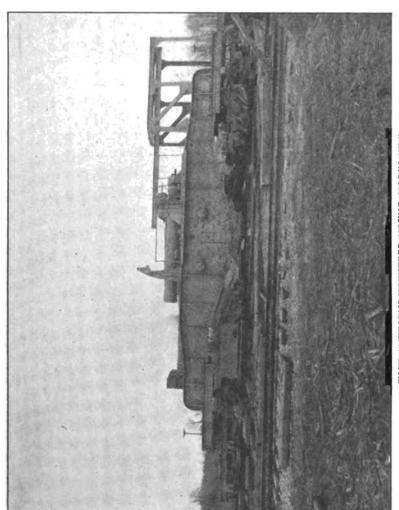
290. Demerits.—The necessity for having a pit as deep as 90 inches, when this might have been avoided, is a demerit. The clumsy traversing mechanism is likewise a demerit. This mechanism involves the use of four extremely heavy radial truck frames which are separate pieces of equipment in transit and require a heavy crane for their installation. The elevating mechanism includes Hindley worms which it is felt will give serious difficulty in field service. This type of mechanism is not efficient in comparison with mechanism composed entirely of spur gears, and when compared with the mechanism used on the alternate 16-inch howitzer carriage,

it is not a commendable design. In the near future the necessity for providing so elaborate a piece of accessory equipment as a 120-ton locomotive crane for the installation of a base ring may be considered a serious demerit, although this is not certain. At present one has the choice of using a timber firing platform giving a limited traverse and installed by a Gantry crane of light construction, a curved firing track which can not be concealed from air photographs and requires at least two days for its installation, or a steel base ring which can be installed in about 12 hours and which requires a locomotive crane of 100-tons capacity or more. Since a locomotive crane will in general be included with the equipment of railway artillery parks the necessity for its use on the front may not be a reasonable criticism.

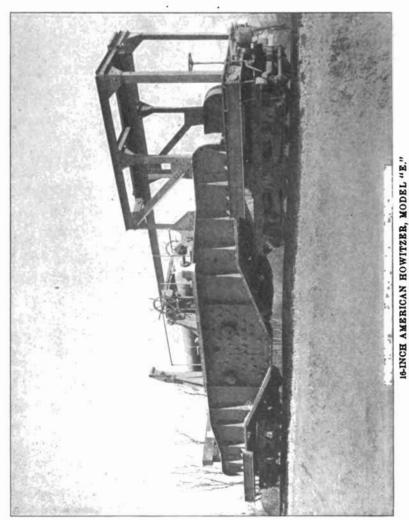
PLATE 335

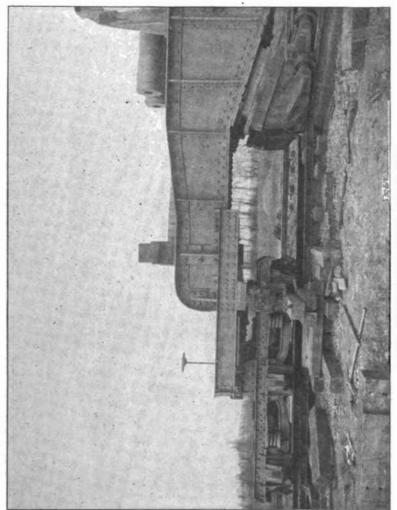




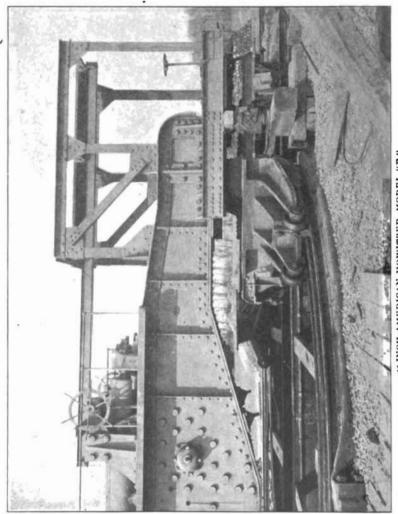


16-INCH AMERICAN HOWITZER MOUNT, MODEL "E."

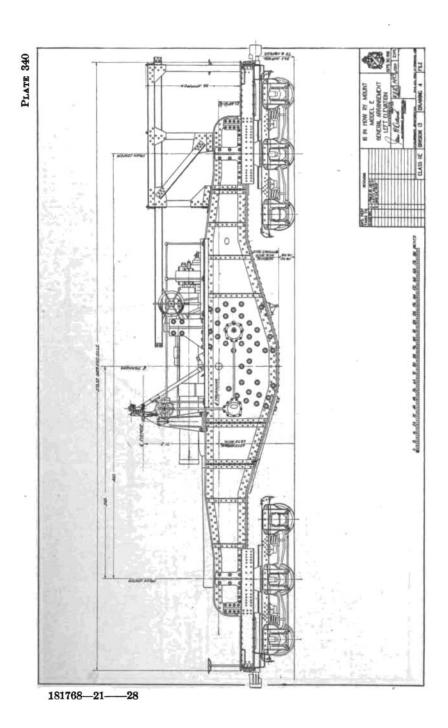


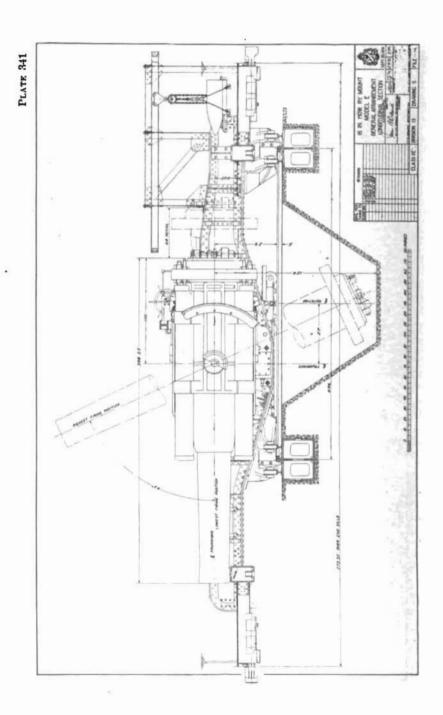


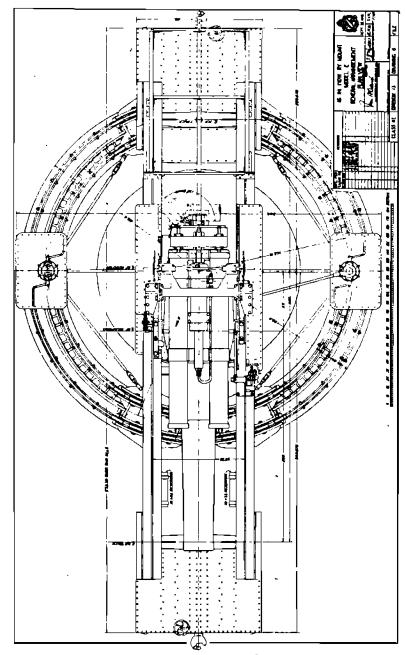
16-INCH AMERICAN HOWITZER, MODEL "E."



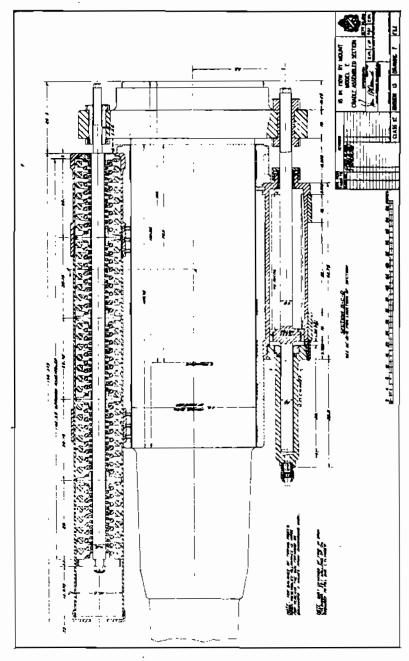
16-INCH AMERICAN HOWITZER, MODEL "E."

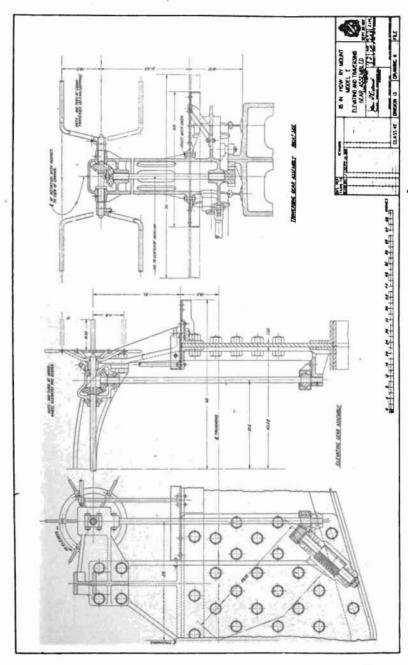


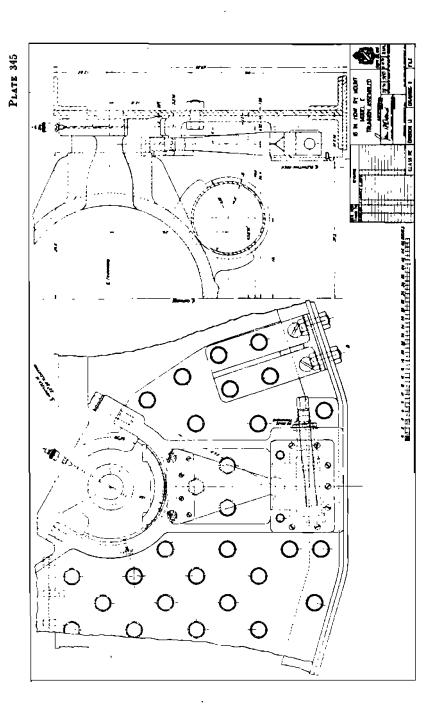


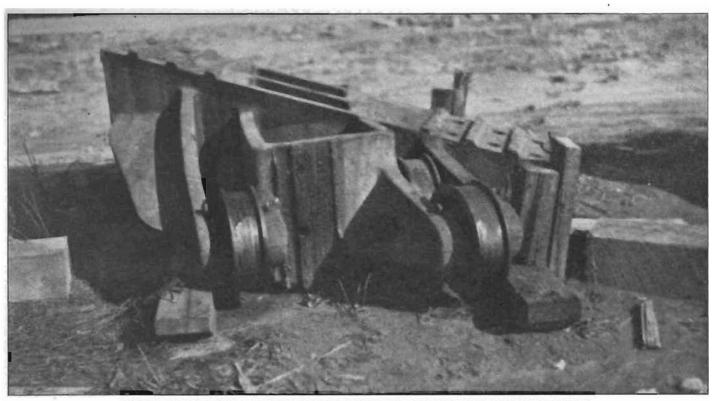




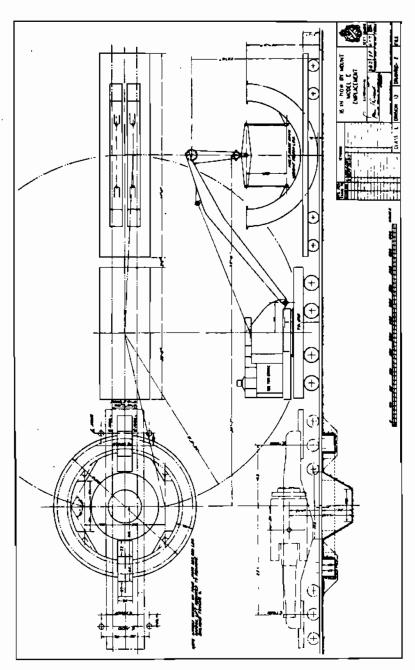


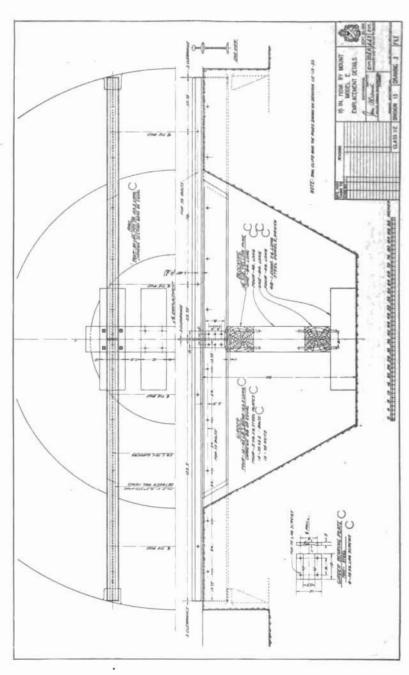


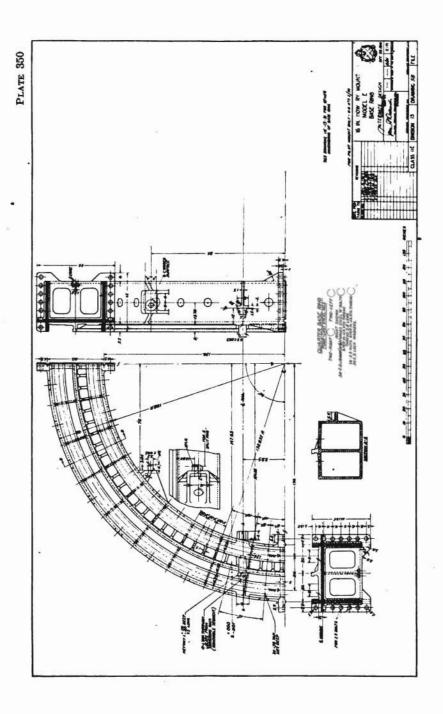




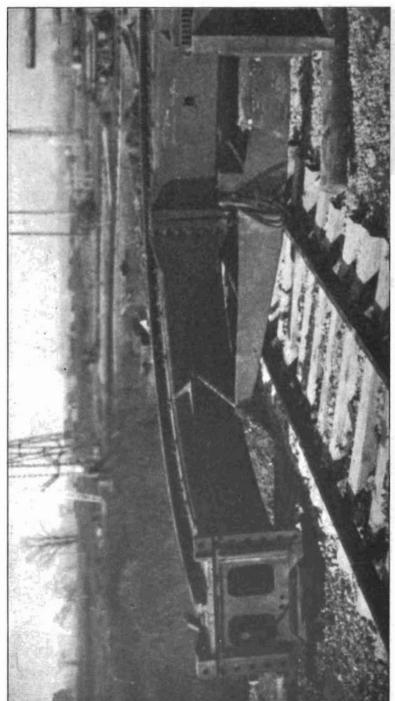
. FRONT RADIAL TRUCK FRAME OF THE 16-INCH AMERICAN HOWITZER MOUNT, MODEL "E."











BASE RING FOR IGINCH AMERICAN HOWITZER MOUNT' MODEL"E."

15.—AMERICAN 16-INCH HOWITZER ON RAILWAY MOUNT, MODEL OF 1918, MARK I. (28)

291. This carriage was designed as an alternate mounting for the 16-inch howitzer, model of 1918, Mark I. The howitzer was originally designed in connection with the 16-inch howitzer carriage. "model E," already described. This mount is of the cradle recoil mechanism type, model 1918, or combined cradle and rolling recoil type, model of 1918, Mark I, in each case with limited traverse. The design is, in general, similar to that of the French 400-millimeter howitzer carriage, plate 25, and the design of its emplacement is likewise similar to that of the 400-millimeter howitzer emplacement. Before the carriage was completed the principle of rolling recoil was receiving considerable attention and a number of trials were made with this carriage operating as a rolling recoil carriage. It functioned very satisfactorily, but it was found that it would be necessary to replace the original five-axle trucks with a stronger type of truck having six axles. The mount can now be used either on the emplacement originally designed in connection with it, or it can be operated as a rolling recoil mount. The maximum elevation obtainable on the emplacement is 65 degrees and the maximum elevation when used as a rolling recoil mount is 45 degrees. The top carriage has a traverse of 5 degrees on either side of the center, which is of course the maximum traverse that can be secured when the mount is used on an emplacement. When it is being used as a rolling recoil mount, any desired amount of traverse can be secured by operating it on a curved firing track. General views are given on plates 353 to 361 and 35.

292. Gun.—The gun used with this mount is the 16-inch howitzer, model 1918, Mark I, of 18-caliber length. It is carried on the mount in a cradle which is provided with hydraulic recoil mechanism and spring recuperator system. The gun is fitted with splines which slide in spline ways in the cradle to prevent rotation of the gun. It is rifled with 144 grooves, which twist to the right at a pitch increasing from one turn in 40 calibers to one turn in 20 calibers. It is provided with an interrupted thread breechblock, which is fitted with a mechanical firing mechanism.

293. RECOIL MECHANISM.—The recoil mechanism is of the hydrospring type and comprises two hydraulic recoil cylinders mounted at the top and bottom of the cradle in the center, and four spring recuperator cylinders mounted two above and two below. The design of the recoil cylinders is shown on plate 35 and the design of the spring recuperator cylinders, as well as the recoil cylinders, on plate 343, of the model E howitzer carriage. The recoil and recuperator systems of the two carriages are identical. On plate 362 a by-pass tube can be seen connecting the front end of the buffer with the rear of

the recoil cylinder. A similar by-pass is provided on the lower cylinder. These by-passes are provided for the purpose of adjusting the length of recoil for various weights of projectiles and powder charges. The maximum length of recoil is 48 inches.

294. ELEVATING MECHANISM.—Elevation is provided from minus 8 degrees, the loading angle, to plus 65 degrees. The mechanism comprises a segmental circular rack attached to one side of the cradle, a pinion, and a train of four spur gears leading to the operating hand-A band brake is provided on the handwheel to prevent undue stressing of the elevating mechanism from the reaction of firing. This band brake is substituted for the slip friction device ordinarily incorporated in the worm wheel of a worm-gear transmission. turn of the handwheel moves the gun through 1.8 degrees in elevation. The effort required to elevate and depress the gun is reduced by antifriction devices installed on the trunnions and of a design shown on plate 356. This device has proved particularly efficient and makes it possible to operate the elevating mechanism with very small effort. The details of design of the elevating mechanism proper are shown on This is the first design completed on which the elevating mechanism is composed entirely of spur gears. It has proved so much more efficient than other mechanisms which include the worm gears that practically all designs made up since this carriage was completed have been provided with similar types of elevating mechanisms.

295. Traversing Mechanism.—The gun can be traversed with respect to the car body 5 degrees on each side of the center through rotation of the top carriage about its pintle, by means of a mechanism whose design is shown on plate 358. The rear of the top carriage rests on the car body by means of two Belleville spring-supported rollers, and the carriage is rotated about its pintle, plate 335, by turning the vertical shaft which carries on its lower end a pinion meshing with the traversing rack. This shaft is operated by a long ratchet handle. The upper end of the vertical shaft can be seen just in front of the ammunition table on plate 256. The upper end is held in a bearing which is attached to the table. One rotation of the lever traverses the carriage 4.14 degrees in azimuth. When the mount is operated as a rolling mount any desired extent of traverse can be secured through the use of a curved firing track. Under such circumstances only fine adjustments in azimuth are made by means of the top carriage traversing mechanism. It is probable that a very great displacement of the track would result from the operation of the mount with the gun at either of its extreme positions. personnel operating British 12-inch railway mounts having a maximum traverse of 1 degree on each side of the center reported slight difficulty in the displacement of their track when the gun was operated at even the extreme position of 1 degree traverse.

296. Gun Carriage.—The gun carriage, plates 256 and 53, comprises the cradle carrying the recoil mechanism, and the elevating and traversing mechanisms already described, all mounted, or carried on a structure of cast-steel side frames and transoms. The carriage is provided with a heavy pintle at its forward end, which fits into a bearing machined in a cast-steel transom of the car body. The rear of the carriage rests on the car body by means of spring-supported rollers already described under Traversing mechanism. A structural-steel working platform carrying the ammunition table and crane is bolted to the rear of the cast-steel top carriage. Between the cradle trunnions and side frames antifriction devices already described under elevating mechanism are incorporated to reduce the effort required to elevate and depress the gun.

297. CAR BODY.—The car body, plates 35 and 53, is made up of two single web structural steel side girders connected by structural and cast steel transoms. Toward the forward end a cast steel transom, machined at its center to serve as a bearing for the pintle of the top carriage, is bolted to the side girders. Center plates and side bearings are provided at either end of the car through which it is supported on two trucks. Outrigger struts, jack supports and ties are attached to the lower cord of the side girders for use in anchoring the mount to its emplacement.

298. Anchorage.—When the mount was designed it was intended to operate it on a timber platform of the design shown on plate The platform is in two principal parts. The one comprises a horizontal bed of timbers on which the mount rests through four jack screws and which takes the dead-weight of the car and vertical component of the shock of recoil. The other is composed of two triangular braces resting against a timber pad. These braces are connected with the mount by means of ball end struts hinged to the mount and resting in foot plates on the ends of the braces, plate 359. This part of the platform takes the horizontal component of the shock of recoil. When the gun is being operated above elevations of 45 degrees, it is necessary to have a pit about 2 feet deep between the two heavy horizontal timber beds, into which the gun may recoil. The rails which bridge this pit and on which the mount is run, are carried on I-beam stringers, plate 53. They are removed for firing. The time required for the installation of platforms for similar French 340 millimeter gun and 400 millimeter howitzer carriages, varies between two and five days according to the nature of the ground and weather. When the gun is fired at angles of 45 degrees or less, the mount may be operated on a track of heavy construction without the use of any firing platform. The brakes are set at a pressure to barely permit rolling of the wheels and the entire mount rolls back a distance of from 30 to 40 feet. To secure any large degree of traverse

it must be operated on a curved track. The mount is drawn back to its firing position by means of a winch mounted on the front truck. This winch is connected with the track some distance ahead by means of a cable.

299. Trucks.—The trucks, two in number, are five axle (model 1918) and six axle (model 1918, Mark I), locomotive type with inside journals. The body and bolster are made up entirely of structural steel. The journals are 6.5 inches by 12 inches and the wheels 28 inches in diameter. The axles are equalized throughout, thereby distributing the load evenly over the entire truck. Each truck is equipped with both hand and air brakes. French type couplers and buffers were provided during the active period of the war, but have since been replaced by the standard M. C. B. type.

300. Ammunition Supply System.—The ammunition car used with this mount is identical in design with that employed with the 8-inch railway mounts, plate 106, with special racks of course, to hold the 16-inch projectiles and powder cans. No special provision has yet been worked out for transferring the ammunition from the ammunition car to the mount. A crane is provided on the rear of the mount by means of which the ammunition may be lifted from the ground on either side of the mount, or from a flat car or from the track at the rear of the mount. After being lifted by means of the crane the ammunition is placed on a tipping tray on the top of the loading stand located on the working platform. When the rear of this tray is tipped up, the projectile slides forward with slight assistance along the removable tray into the breech of the gun and scats itself. The loading angle is minus 8 degrees. This loading apparatus is shown on plate 53.

301. Maintenance.—Every mechanism of this mount has functioned very well on proof tests and no serious difficulty in the nature of maintenance is anticipated. There is one possibility of trouble which may be mentioned under this head. When firing with full charges and at 45 degrees elevation from the emplacement a slight lifting of the mount from the bed at the forward end, and a bending of the struts under the vertical braces at the rear, was noted on two occasions. This bending was due to crushing of the wood under the bearing of the strut and to the fact that the strut had a reduced section near the vertical brace. It is probable that the substitution of another strut with large section and strengthening of the wood beam along the top of the triangular braces will eliminate any future trouble of this character.

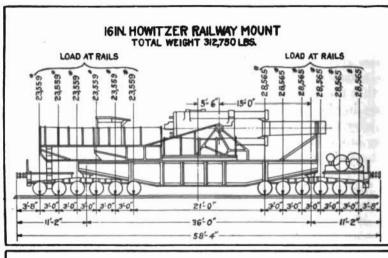
302. DIFFICULTIES INVOLVED IN THE SERVICE.—The only difficulty involved in the service with a piece of this type that need receive consideration is the time and care required in the preparation of the emplacement. This has already been discussed at some length under

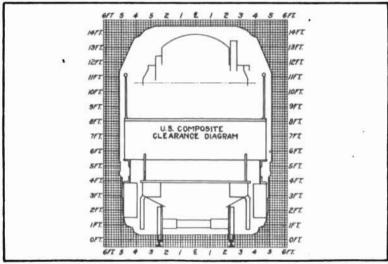
the 14-inch naval mount. Mark I. It is essential either that the emplacement be made in firm soil or that a sufficient bed of cinders, gravel or stone be put under it to insure it against undue settling. It has been mentioned that the mount can be operated as a rolling recoil mount to a maximum elevation of 45 degrees. Since it is probable that for the majority of targets a new track would have to be installed to give the proper direction in azimuth, the difficulty involved in the laying of this track must be considered. Such a firing track must be well constructed and be made up entirely of very heavy components. The firing so far conducted from this mount indicates that a track similar in construction to that employed in heavy commercial service will be satisfactory. The deduction is, then, that the only point in this connection that can be raised is the increase in time required (two days) for placing a special curved track, over that required for another mount carrying a gun of similar caliber, but using an emplacement, possibly of the type employed with the 14-inch model E mount, which can be installed in about 12 hours. No ammunition-handling system has as yet been carefully worked out, but it is not felt that any particular difficulties will be encountered in finding a satisfactory solution.

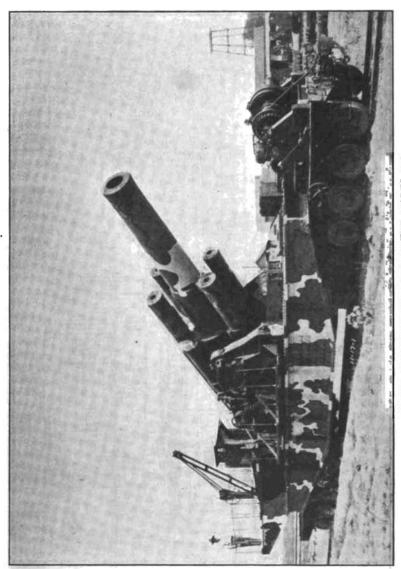
303. Merits.—This mount has an elevating mechanism of excellent design. As mentioned before, this was the first mount completed on which the elevating mechanism was composed entirely of spur gears. Tests have proved its excellence. The antifriction device has proved equally excellent and the design has been followed on other mounts.

304. Demerits.—The necessity for the use of so cumbersome an emplacement for the operation of the howitzer at high elevation is a serious demerit. What has been said in this respect under the 14-inch naval mount, Mark I, applies equally here. The limiting of the maximum elevation to 45 degrees when the mount is used as a rolling recoil mount is unfortunate. This point is mentioned here, however, only in comparing the mount with the ideal type of mount, for it was originally intended to operate it from the emplacement only; the possibility of operating this particular mount at so great an elevation as 45 degrees without the use of an emplacement is distinctly favorable. It seems certain now that a carriage can be designed on which the gun can be operated to an elevation as great as 65 degrees with the mount operating either as a combined sliding and cradle recoil mount or as a fixed emplacement mount, the emplacement involving no more elaborate components than those employed with the 8-inch gun and 12-inch mortar.

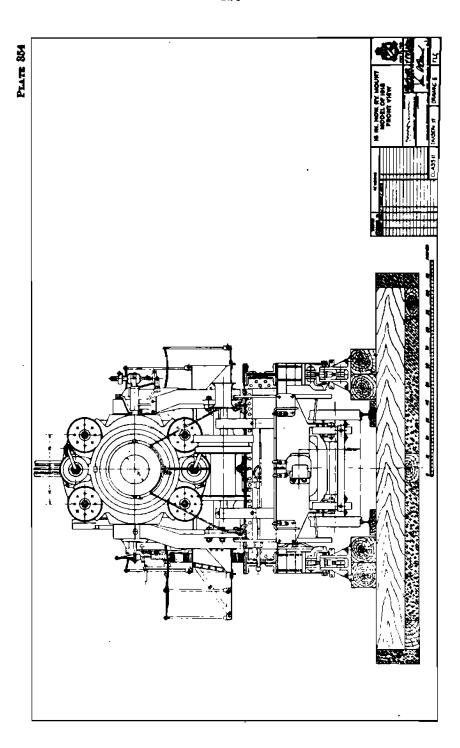
PLATE 352

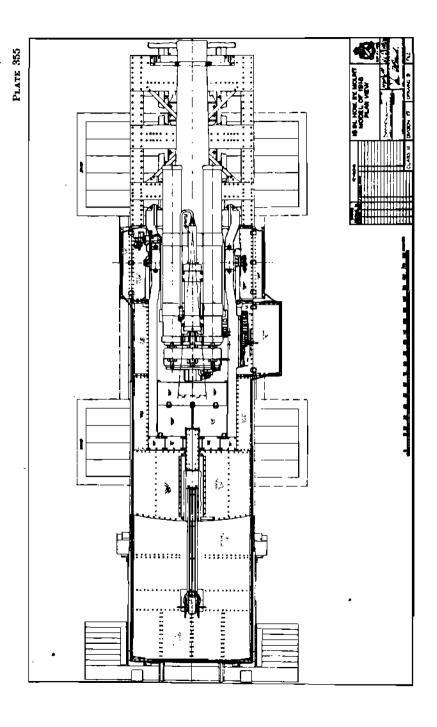


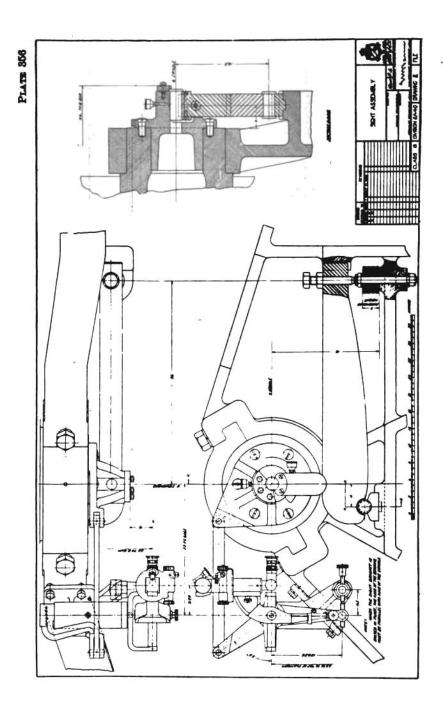


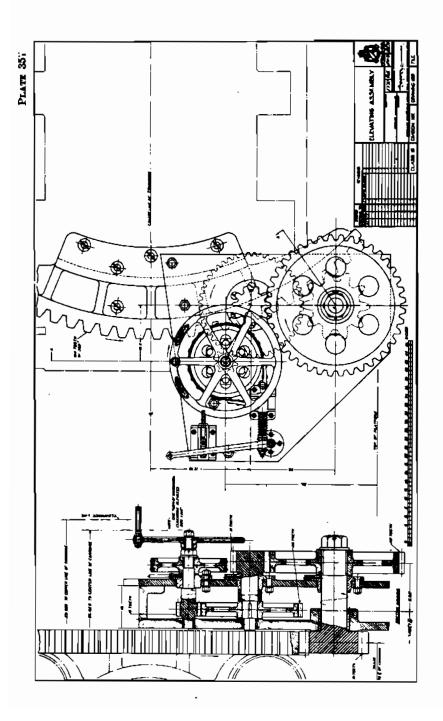


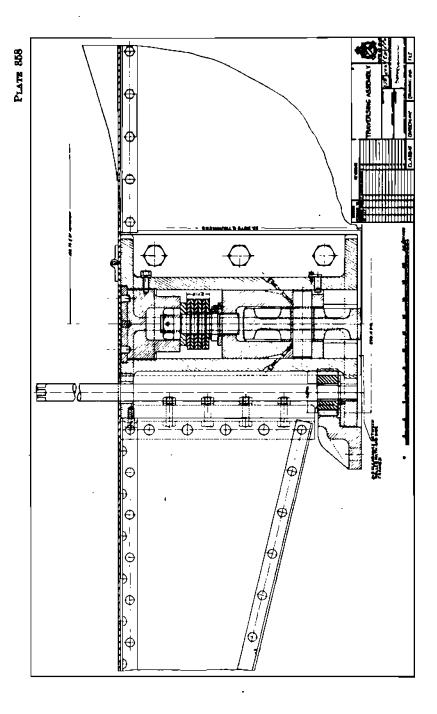
16-INCH AMERICAN HOWITZER MOUNT, MODEL 1918.

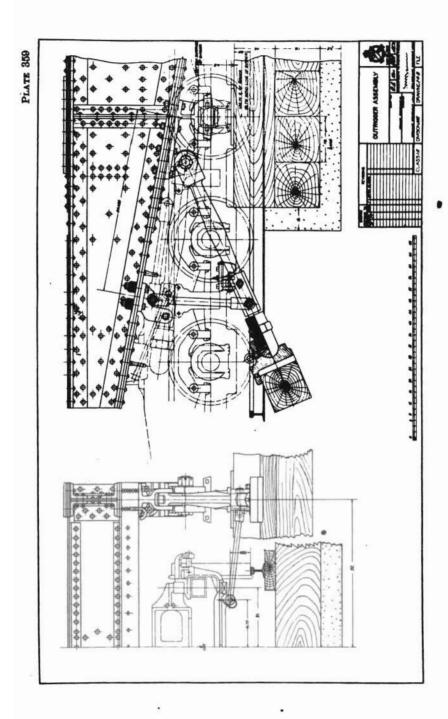


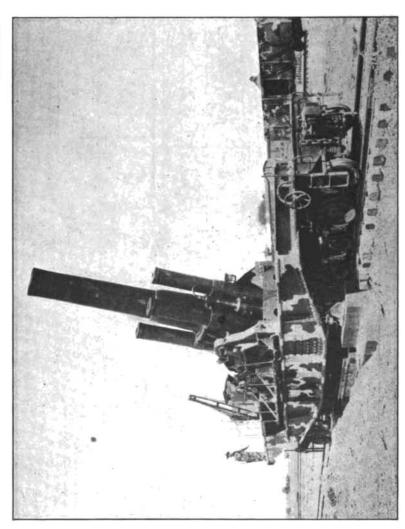


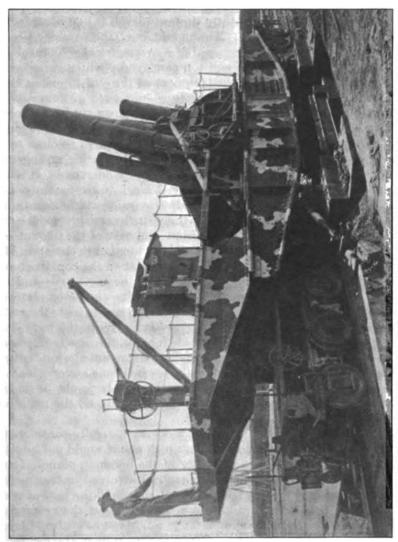












ISINCH AMERICAN HOWITZER MOUNT, MODEL 1918 (EMPLACED FOR HIGH ANGLE FIRING).

16.—AMERICAN 16-INCH GUN ON BAILWAY MOUNT. (29)

305. The description that follows is of what represents perhaps a study rather than an actual design of a railway carriage for the 16-inch 50-caliber American Army gun. It was made up during tht early summer of 1918, in anticipation of a need for such equipmene in France, and it is probable that the actual design would have followed very closely if not exactly these studies if it had been decided to construct such a mount. The mount is of the combined cradle rolling recoil type and is composed of a symmetrical structural steel girder carrying a unique type of top carriage by which it is possible to elevate the center line of the trunnions of the gun 40 inches above the traveling position, and the whole is supported on four six-axle trucks, plate 363. This represents the first known study of a mount in which provision is made for elevating the trunnions of the gun in this particular manner. The trunnions are mounted so close to the breech of the gun as to necessitate a counterbalancing arrangement to compensate for the considerable muzzle preponderance. It is necessary to operate the mount on a curved track to secure any considerable degree of traverse, but car body traversing mechanisms somewhat similar to those incorporated in the 14-inch carriages, models 1918 and 1919, are incorporated in the front and rear of the mount over each span bolster. The gun can be fired to a maximum elevation of 40 degrees without any other track preparation than the construction of a heavily ballasted curved track made of the heaviest rails and ties.

306. Accessory crane equipment, transporting cars, etc., plate 364, were to be provided for removing the gun and cradle from the mount and carrying it on a separate transport car. With the very large cradle that it was necessary to provide for this gun it was impossible to keep the mount, with the gun and cradle mounted on it, entirely within the clearance lines of all railways in France over which the mount would probably have had to operate. It would be possible to transport the mount complete over practically all the main lines of American railways.

307. The need for such a mount was very carefully considered in France and it was finally decided that such a unit would not be either an efficient or economical competitor of the bombing plane. It was felt that in consideration of the difficulties involved in transporting such a mount over roads which were not always in the best of condition, and in consideration likewise of the fact that the accuracy of fire of such a gun at its maximum range would not be such as to make it possible to operate effectively against any targets smaller than a large railway yard or a city, both of which could be operated against more effectively both as to accuracy in placing the explosive charges and as to the extent of destruction, by bombing planes, it would not be wise to divert our limited manufacturing facilities from absolutely essential ordnance to this experiment.

308. In the autumn of 1918 the Navy Department, on finding that the axles of the 14-inch mount, Mark I, were so heavily loaded

as to give continual trouble from overheated journals, designed and began the construction of a mount whose characteristics were almost identical with this 16-inch mount. This mount, which is termed the Navy 14-inch Mark II mount, has since been finished. Its total weight is such as to require only 20 axles as against 24 for the 16-inch mount.

309. Gun.—The gun for which this mount was to be designed is the 16-inch, model E, of 50-caliber length. It is fitted with splines above and below, which slide in spline ways in the cradle to prevent rotation of the gun, and a heavy lug or yoke is shrunk on over the breech, to which lug the four recoil and two recuperator pistons are attached. The gun is rifled with 144 grooves which twist to the right at a pitch increasing from one turn in 50 calibers to one turn in 25 calibers. The breech is of the Welin or stepped thread type and is equipped with a mechanical firing mechanism.

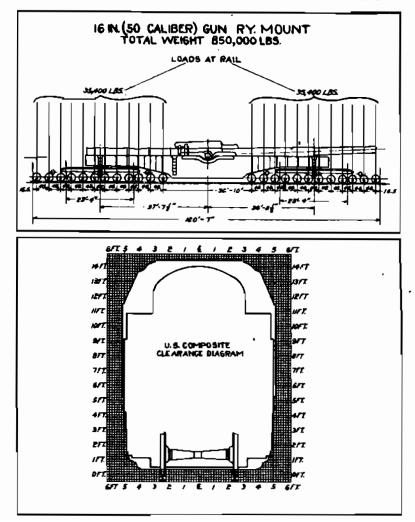
- 310. Recoil Mechanism.—The recoil mechanism is of the hydropneumatic type and comprises four hydraulic recoil cylinders arranged symmetrically about the cradle, two above and two below. and two pneumatic recuperators, placed one in the center at the top of the cradle and the other in the center at the bottom. length of recoil is 48 inches and the maximum length of recoil is 49.67 The mount itself is likewise of the rolling recoil type and while some of the energy of recoil is dissipated in the recoil mechanism proper, most of it is absorbed in the friction of the brakes as the mount rolls back on the track. Most rolling recoil mounts that have been observed roll back on the track a distance of from 30 to 50 feet. It is assumed that this might represent the probable length of recoil of this mount also. The design of the recoil cylinders is practically the same as that of the recoil cylinders of the mounts already described. The design of the pneumatic recuperators is practically identical with that of the pneumatic recuperators used on the 12-inch mortar and the 12-inch Batignolles mounts.
- 311. ELEVATING MECHANISM.—Elevation is provided from minus 3.3 degrees, the loading angle, to plus 40 degrees, the maximum firing The mechanism comprises two worm racks, worms meshing with these, and a series of bevel and spur gears leading to the driving motor and to the handwheels on either side of the mount. mechanism is driven by an electric motor under normal conditions. but provision was made for hand operation in the event that this should at any time be necessary. Provision is made likewise for disengaging the worms from the elevating racks when the gun is in transporting position. An accessory to this mechanism is the compensating cylinder shown on plate 364, directly below the trunnions. It was necessary to place the trunnions close to the breech. resulted in a large muzzle preponderance, which is compensated for by the balancing cylinder. This compensating arrangement is an adaptation of the pneumatic recuperator and consists of a cylinder placed within a larger cylinder, the inner cylinder sliding in and out as the gun is depressed or elevated. Tie-rods connect the front of the inner cylinder with the bottom of the cradle. The stroke of the

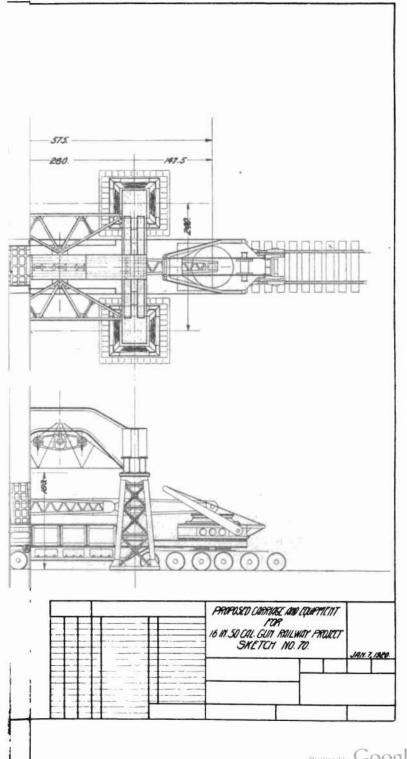
inner cylinder or piston is 75.52 inches, and the maximum pressure in the cylinder is 1.950 pounds.

- 312. Traversing Mechanism.—It is necessary to operate this mount on a curved track to secure any considerable traverse. Electrically driven translating mechanisms similar in design to those used on the 14-inch mounts, models 1918 and 1919, are incorporated in the trucks, for the purpose of training the gun on the curved track. It is quite probable, however, that the mount would ordinarily be returned to battery by a locomotive, inasmuch as the length of recoil of from 30 to 50 feet is so great as to make the time necessary to return it by means of the translating mechanisms excessive. An additional mechanism is incorporated in the mount at either end over the center of the span bolsters. This mechanism is of a design similar in principle to those mechanisms used on the 14-inch mounts, models 1918 and 1919, and affords a total traverse of 1.3 degrees.
- 313. Gun Carriage.—The gun carriage comprises a cradle of gridiron design with its four recoil and two recuperator cylinders and the cast-steel slide, by means of which the gun can be elevated 40 inches for firing. This slide is composed of two cast-steel side members joined by transoms, plate 364, and carries the cradle by means of trunnions resting in the bearings machined in the top. riage is raised a distance of 40 inches by means of eight hydraulic jacks. The pressure necessary in these jacks is approximately 2,100 pounds per square inch. When either at its upper or lower position the carriage is fixed rigidly to the car body by means of four large pins inserted through the side girders and the carriage castings, Additional safety devices are provided at the front and rear of this carriage on top of the side girders in the shape of screw-operated caststeel supports, which can be run under the extensions of the carriage. thereby relieving the pins from excessive load. The carriage castings have four pin holes, the top ones of which are used when the gun is transported and the lower ones of which are used when the gun is in battery position. The carriage slides between the webs of the side girders on fixed grooved guides. The slides or supports mentioned above are provided with stepped surfaces which are intended to serve as supports when the carriage is being raised.
- 314. Car Body.—The car body is composed of two single web structural steel girders joined by a series of structural and cast-steel transoms and supported at the front and the rear on the trucks by means of span bolsters. The construction of the girders is symmetrical about a vertical center line.
- 315. Anchorage.—The only anchorage that this mount has in firing is the friction of the brakes. It rolls back a distance of approximately 40 feet on the track. The brakes must then be released and the mount is returned to its firing position by the translating mechanism or by a locomotive.
- 316. TRUCKS.—The trucks are four in number, of locomotive type, and contain 6 axles each with 6.5 by 12-inch journals and 33-inch steel wheels. The axles of each truck are equalized throughout so

that the load is distributed as perfectly as possible. They are equipped with semielliptical springs of sufficient capacity to stand both the transporting and the firing load. The mount is supported on these trucks in pairs by means of structural steel span bolsters. The center bearings of these bolsters are of the roller type.

317. Ammunition Supply System.—It is not certain whether the standard railway artillery ammunition car could have been used with this mount. If not, a car of similar design but of heavier construction would have been provided. The loading mechanism is of a design similar to that provided on the 14-inch mounts, models 1918 and 1919. The loading position of the gun is minus 3.3 degrees, and the loaded tray acquires sufficient velocity on the inclined track to cause the projectile to slide into the powder chamber. The projectile is rammed by hand.





17.—GERMAN 170-MILLIMETER GUN, MODEL 1915, ON RAILWAY MOUNT. (30)

- 318. This mount is a combination arranged for use as a railway mount firing from the wheels with small traverse or as an emplacement mount firing from a platform with all-round traverse. It is made up of a heavy type of mobile gun carriage set on a special drop frame flat car. The gun carriage is quite similar in design to the German field carriage mounting 15-centimeter 40-caliber guns and may be operated from the same type of platform. The mount is shown on plates 365 to 371. The car trucks of the mount examined bear the date 1917.
- 319. Gun.—The gun is a modern Navy piece, model 1915, of 40 calibers length. It is rifled with 52 grooves twisting to the right at uniform pitch of 1 centimeter in 10 centimeters. It is provided with the ordinary type of Krupp sliding wedge breechblock and uses semifixed ammunition.
- 320. RECOIL MECHANISM.—The recoil mechanism is of the hydrospring type and comprises one hydraulic brake cylinder attached to the cradle in the center at the bottom and two spring recuperator cylinders attached to the cradle on either side of the brake cylinder, plates 366 to 368. The length of recoil is 15 inches. Two round rods screwed into the recoil lug on either side of the brake piston rod extend to the rear and carry the yoke which is attached to the two spring piston rods.
- 321. ELEVATING MECHANISM.—The elevating mechanism comprises a rack bolted to the left side of the cradle and a pinion with a worm wheel, worm and bovel gears leading to a handwheel. Another handwheel, or rather a crank of 12-inch radius for high speed elevating, is connected to the first through a sprocket and chain. Sudden shocks of fire appear to be taken care of by Belleville washers on the worm shaft, which allow it a slight motion in an axial direction. This entire mechanism is disposed along the left side of the carriage and can be traced out in plate 366. A total elevation of 45 degrees is indicated on the elevation scale, although a publication at hand states that 47.5 degrees is possible. The first, or adjusting handwheel, gives a ratio of 0.4 degree per turn of handwheel, while the second at the end of the chain, for rapid movement, gives 1.25 degrees per turn. No antifriction trunnions are provided and the operation of the second handwheel even at slow speed is hard work for two men.
- 322. Traversing Mechanism.—As noted above, traverse is obtained by moving the field carriage upon the railway car. The carriage is kept in place by means of an angle-iron circle fastened to the flat car floor and around which the wheels of the mount can roll,

plate 236. At the center of this circle is a large pin, fastened to the car, from which swiveled tension rods extend back to the trail of the carriage. The gun carriage wheels bear against the circle of angles and prevent sidewise movement, while the rods prevent lengthwise movement, but the carriage is free to roll on its own wheels about the pivot. The two large wheels of the carriage are about 6 feet in diameter with 19.5 inch face, of which the center 7.75 inches is raised 2 inches higher than the remainder. These wheels are made, both rim and spokes, of structural material, generally of channel section.

323. The rear end of the trail of the carriage body rests on the car floor and against a circular rail fastened thereto, plate 368. On the outside of this rail there is a series of pins, forming a rack, into which a star wheel fastened to the trail meshes. This star wheel is operated through a worm, horizontal shaft, and bevel gear, from a handwheel located near the trunnions on the right-hand flask of the trail. The weight of the trail during traversing is carried upon two spring-supported rollers, which give under the shock of fire and allow the trail to rest directly on the car floor. Twenty-six degrees total traverse is allowed and the gun is moved 0.167 degree per turn of handwheel.

324. Gun Carriage.—The gun carriage is very much like that provided for the British and American 6-inch mobile guns and, as noted before, is quite similar to the German carriages mounting 15-centimeter guns. It comprises a cradle of naval design, plate 366, and a built-up structural steel body, plates 366 and 368. The cradle is carried on the body by means of two cast-steel trunnion bearings without any friction-reducing devices. The cradle is identical in design with those used on German ships and in their coast defense. There is a possibility that this is one of the guns removed from their second navy late in 1917. The body consists of two built-up structural flasks of channel sections with flanges 7 inches wide and a depth of web tapering, as shown on plate 366, from 38 inches in front to 13.5 inches at the extreme rear. The axle on which the wheels described under Traversing Mechanism are mounted is bolted to the bottom of the flasks.

325. RAILWAY CAR BODY.—The railway car is a drop frame flat car of special and very strong construction. The side sills are built-up plate girders of very heavy and varying sections, plates 365 and 366. The entire body is decked with about 0.625-inch steel plate. Except for the very strong construction, there is nothing of special note about the car body.

326. Anchorage.—For firing at angles up to 13 degrees on each side of the center line of the track, cast-steel wedges are placed on the ties under corresponding wedges on the side sills and the mount

is moved by a locomotive until it is wedged up on these. See plate 366 for wedges under the side sills.

327. For wider traverse and other special service a field platform and foundation mounted on a special wagon on road wheels are carried on a flat car, plate 369.

328. The field platform foundation consists of four box girders of light steel, each about 20 by 35 inches and perhaps 10 feet long. At one end of each, two 1-inch steel plates are attached to the top and bottom and extend a foot or so beyond the end, plate 368. A large hole is formed in these to receive the pivot pin. A rigid equal-legged cross, which when buried in the ground constitutes the anchorage or foundation for the field platform, is formed by placing the girders radially, so that these holes match, inserting the pin, and putting in place between the girders some special I-beam spacers, plate 371.

329. The field platform, plate 370, consists of a forward member containing a hole for the pivot pin above mentioned and having formed at its sides guides for the carriage wheels similar to that formed by the circle of angles on the car. This is joined by radial structural members to a large steel plate on which the trail is intended to rest and which is equipped with a circular arc, inside of which the end of the trail rotates, and a chain into which the teeth of the star wheel can engage for traversing. This platform slips down on top of the foundation above described, and it can be pulled around into any desired direction for firing the gun. The gun is rolled onto this platform and the tiebars secured between the trail and the center pintle just as on the railway car. It can be rotated through a small angle, perhaps 10 degrees, upon the platform in any position, and for wider traverse the platform can be moved around any desired amount.

330. Trucks.—The trucks are of structural construction, two axles each, with semielliptic springs and no equalizers. The wheels are nearly a meter in diameter and have very light spokes. Each wheel has two brake shoes.

331. AMMUNITION SUPPLY SYSTEM.—The shells of this gun are sufficiently small so that they can be handled by two men with a tray. The tray employed is provided with eyes, which fasten to hooks on the breech of the gun. It is hooked in position and the projectile rammed from it.

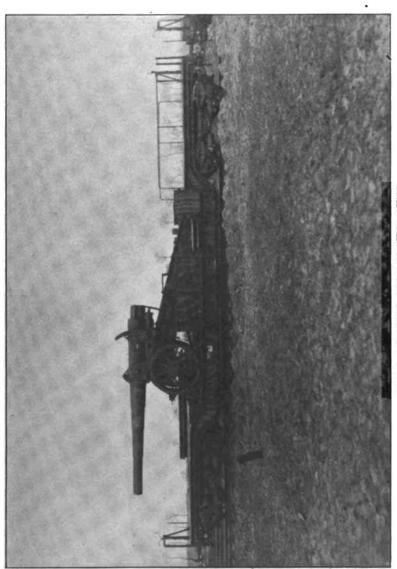
332. MAINTENANCE.—The sturdy construction of the car body as well as of the gun carriage itself, including the cradle and recoil mechanism, indicates that comparatively no difficulty would be experienced in maintaining this mount even under the hardest service and most difficult conditions. The semipermanent emplace-

ment is likewise of such sturdy construction that it is not probable that it would be damaged except with most careless handling.

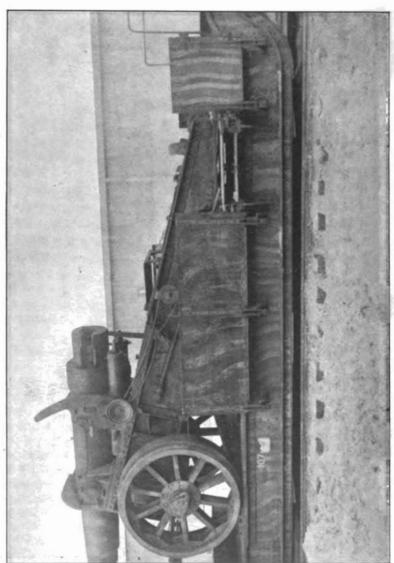
333. DIFFICULTIES INVOLVED IN SERVICE.—The construction of this mount indicates that when serving as a railway mount it might be placed for firing in 10 or 15 minutes. The indications from the construction of the trucks are that the whole mount can be rendered sufficiently stable so that the personnel could remain on the car at all times and serve the gun with maximum speed, probably one shot per minute. From the standpoint of efficiency of service this improvisation certainly seems to fill the bill.

334. Merris.—The merits of this improvisation are its sturdy and simple construction, resulting in a minimum of maintenance, its exceedingly simple method of emplacement for firing from the rails, and the excellent and simple scheme of attaching the ammunition tray to the breech of the gun.

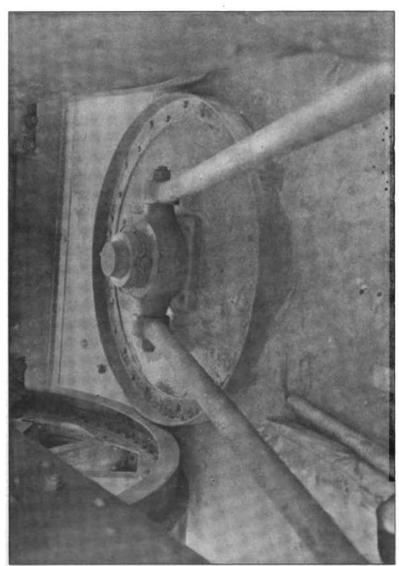
335. Demerits.—If one considers this mount simply from the standpoint of an improvisation it could not be said to have any demerits. Under "Trucks," it was mentioned that the wheels are of exceedingly light construction, but the fact that the car body rests on four wedges when the gun is fired and that when placing the car on these wedges the mount is likely raised considerably from the trucks would indicate that there would be no likelihood of breaking the wheels through shock of fire. From the standpoint of the Germans it would appear unfortunate that this mount had no greater traverse than 26 degrees in any one position on the track. It must be remembered, however, that it was an improvisation, built much more quickly than any type of all-round fire mount could have been made, and that probably the limited extent of traverse has been justified after all.



170 MM. 40-CALIBER GERMAN GUN MOUNT.



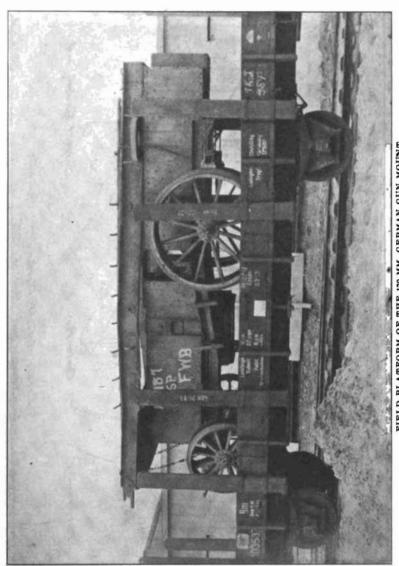
CARRIAGE FOR THR 170 MM. GERMAN GUN (RECOIL AND ELEVATING MECHANISM).



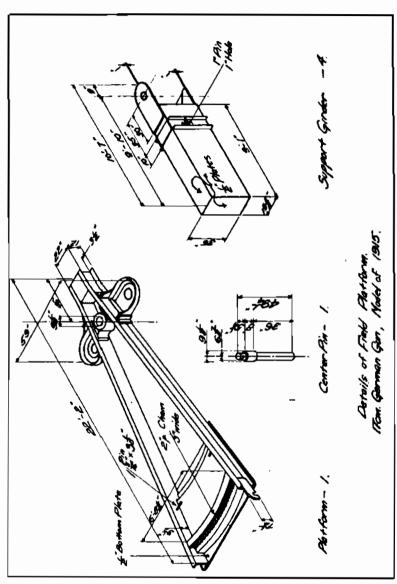
CENTER PIVOT AND TENSION RODS OF THE 170 MM. GERMAN GUN MOUNT.

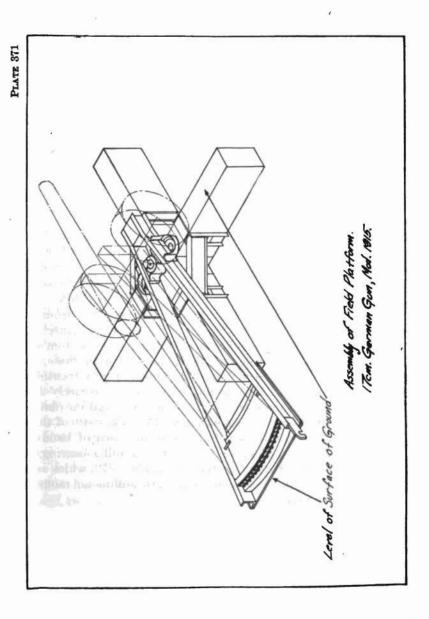


TRAVERSING GEAR OF THE 170 MM. GERMAN GUN MOUNT.



FIELD PLATFORM OF THE 170 MM. GERMAN GUN MOUNT.





18.—GERMAN 210-MILLIMETER GUN ON RAILWAY MOUNT.(31)

- 336. This mount is of the cradle recoil type, plate 372, firing either from the wheels with limited traverse or from a structural steel or reinforced concrete ground platform with all-round fire. It is similar in general type to the German 240 and 280 millimeter mounts, and all of them can be operated on the same ground platform.
- 337. Gun.—The gun is a modern naval piece, model 1913, of 31 feet total length, probably 45 calibers. The powder chamber is only a very little larger than the bore and semifixed ammunition is used. The tube is rifled with 64 grooves twisting to the right at a uniform pitch of 1 centimeter in 10 centimeters. The breechblock is of the ordinary Krupp sliding-wedge type and is fitted with a mechanical firing mechanism.
- 338. Recoil Mechanism.—The recoil mechanism is of the hydrospring type and is composed of two hydraulic recoil cylinders mounted on the top and bottom of the cradle in the center and four spring recuperator cylinders mounted two on the top and two on the bottom of the cradle and on either side of the recoil cylinders, plates 373 and 374. Each recoil cylinder is attached to the cradle by a heavy pin, about which it can swivel in a vertical plane. The forward ends of the springs are connected to the recoil band by a stirrup and two tension rods each. The length of recoil is about 24 inches.
- 339. ELEVATING MECHANISM.—Elevation is provided from 0 degree, the loading angle, to 45 degrees. The elevating mechanism comprises two racks with inside teeth bolted to the bottom of the cradle, two pinions on a common shaft meshing with these, worm wheel, worm, bevel gears, and a special two-speed gear transmission leading to a handwheel. The double-speed gear is entirely similar to that on the 240-millimeter mount, shown in detail on plate 381. The worm and wheel can be seen on plate 375. The ratio of the gear for slow motion is 0.125 degree of elevation per turn of handwheel; for fast motion it is 1.50 degrees per turn. A roller-bearing, antifriction device is provided on the trunnions, plate 372, which is similar in every way to that provided on the 280-millimeter mount and shown in detail on plate 388.
- 340. Traversing Mechanism.—Two traversing mechanisms are provided on this mount. The one is for the purpose of rotating the car body about the pintle of the front truck in firing from the track. It affords a total traverse of 2.25 degrees, or 1.12 degrees on each side of the center line. The other is for the purpose of rotating the mount around a center pivot which is fastened to a ground platform. This mechanism affords 360 degrees. The first mechanism is entirely similar to that employed with the 280-millimeter mount and shown on plates 370 and 391. It comprises a gear case bolted to the side

of the mount, a traversing beam housing bolted into the side girders over the center of the rear truck, and a traversing beam, which is likewise the upper center plate of the rear truck, sliding in guides in the housing. The traversing beam is moved with respect to the housing by a screw, plate 390, which in turn is driven by the handwheel through the gears in the case on the side of the mount. Since the beam is fixed with respect to the truck, any motion of the screw forces the housing and the rear of the mount to the right or left. An indicator is provided in the top of the gear case to show the extent of the traverse, and there is a lock for securing the mount in traveling.

341. The second mechanism comprises a center pivot and two rear support rollers, plate 376. The center pivot comprises a base, 70 inches in diameter, which bolts to the ground platform by twenty 2.5-inch bolts. This base contains a pintle about which the mount rotates and supports a ball bearing with sixteen 5-inch balls on which the swiveled racer carrying the mount rests. This pivot is identical in design with that of the 280-millimeter mount, plate 394. The racer is carried by means of its trunnions in steel bearings holted to the bottoms of the side girders. Thus the car body can rock in a vertical plane as well as rotate in a horizontal plane about the base. The rear end of the mount is supported on a track in the foundation by two rollers, 24 inches in diameter by 4 inches on the face, the housings of which are bolted to the side girders just forward of the rear truck. These are set on a radius of 14 feet 9 inches from the center pivot. One of these rollers is provided with gearing, plate 376. through which it may be driven by one two-man handle. four turns of the handle give one revolution of the roller. equivalent to about 1 degree of traverse per turn of the handle.

342. Gun Carriage.—The gun carriage and car body are one in this mount and will be jointly discussed in the next paragraph.

343. Railway Car Body.—The gun is carried in a cylindrical cast-steel cradle, about 9 feet long, which is supported in cast-steel bearings on the side girders of the car body by means of trunnions about 10 inches in diameter by 7 inches long. The railway car body consists of two single web plate girders, built up of about 0.625-inch plate, and 5 by 5 inch angles with cover plates. The depth of these girders is about 52 inches at the center, 28 inches over the front trucks, and 34 inches over the rear trucks. Structural steel transoms are employed throughout and the bracing against skew consists of a decking of about 0.625-inch plate over the two trucks and against the underside of the girder. As shown on plate 372, a number of folding platforms are provided along the sides of the mount, and a cab of 0.5-inch armor plate is provided around the breech of the gun to protect the personnel. Special I beams are supported under the

front and rear ends of the girder for use in jacking the mount off the trucks and letting it down on the foundation. The girder rests on these beams through roller bearings; adjusting screws are provided to facilitate exact adjustment of the bolt holes in the pivot flange with those in the foundation.

- 344. Anchorage. This mount must be operated on a curved track to secure wide traverse when it is fired from the wheels. Special wedges made in identical halves are bolted to the rails behind each wheel by one bolt each. These wedges are about 12 inches long by 6 inches high at the rear and are curved to fit the circumference of the wheel. The ground platform employed to secure all-round fire is identical in design with that shown on plates 397, 55, and 56. The mount is run into place on the platform and the small section of track over the center, as shown in the upper view, plate 397. is removed in order that the pivot base may be lowered on to the structural base by means of the lowering screw, plate 394. It is bolted fast by 21 bolts. Four special jacks of a design shown on plate 398, and attached to the jacking beams located under the front and rear of the mount and described in the preceding paragraph, are then let down and the mount is raised by means of them sufficiently to permit the trucks to be removed as well as the two sections of track connecting the center with the outside. The entire mount is then lowered until the rear rests on the circular track by means of the rollers and the forward end rests on the 16 steel balls in the central pivot.
- 345. TRUCKS.—The trucks are of structural steel construction throughout with four axles each, outside journals, semi-elliptical springs and equalizers between outside axles only, plate 372. A capstan headed screw is provided over each journal bearing and is so arranged that it can be screwed down on to the spring clip and relieve the springs of undue strains when the mount is fired from the wheels. Hand brakes only are provided.
- 346. Ammunition Supply System.—An overhead trolley runs on an I-beam track secured along the top of the cab. An extension beam is so hinged to the fixed beam that it can swing in a vertical plane, can be lowered for traveling or raised and braced in place to allow picking up a shell from a car or from the track some distance behind the mount. The extensible trolley arrangement of the 240-millimeter mount, plate 378, is identical in design. The shot tray is provided with two two-man handles, a yoke above with an eye, and four wheels below, so that it can be carried by the trolley hoist, by hand, or rolled on the floor. It can be hooked in place on the breech as with the 17-centimeter mount, plate 373.
- 347. MAINTENANCE.—There are no apparent difficulties in the maintenance of this design of railway mount, which, as mentioned

before, has been used for 24-centimeter guns and howitzers and 28-centimeter guns. All parts are very simple in design and substantially constructed. The elevating, traversing, and loading mechanisms had all seen considerable service and no apparent difficulties had developed. The trucks had likewise given no difficulty. The speed transmission introduced in the elevating mechanism of this and the 24-centimeter mount is very sturdy in construction and apparently did not give any trouble.

348. DIFFICULTIES INVOLVED IN SERVICE.—But one difficulty is apparent in the service of this mount. This difficulty results from the necessity for using a heavy platform, usually of steel, which likely requires from three to six days for placing. Without this traversing mechanism it is, of course, necessary to operate the carriage on a curved track, making the necessary small adjustments in azimuth by the traversing mechanism on the rear truck. The use of this steel platform necessitates the providing of a knockdown Gantry crane, and seven cars are required to carry the crane and platform.

349. Merits.—The double speed transmission on the elevating mechanism is simple in design and very effective. The design of the traversing mechanism is good. The mount requires either a structural steel or reenforced concrete platform, both of which require some time for installation, but in comparison with other mounts now in existence, this design must be considered good. This is the first mount on which so simple and effective a type of anti-friction device has been used and it deserves consideration for our own work of design. The traversing mechanism installed over the rear truck is simple in design and excellent for service in firing from the track. The scheme of attaching the loading tray is simple and excellent and warrants consideration. It may be well to mention that although the ground platform of this requires some time for its installation, it is neverthheless easy to conceal after it is installed, since the approach tracks may be removed and the mount completely covered.

350. Demerits.—The one apparently bad feature which has been mentioned likewise under the head of Merits, is the firing platform. At the beginning of this section it was mentioned that criticism would be made of the firing platform on a basis of the ideal apparently attainable. The steel platform, however, required seven cars for its transportation and can not be installed in less than from three to five days. The concrete platform can probably be installed in the same length of time and of course, with fewer facilities. It seems possible to design a mount in which the same general features may be embodied but which will not require such elaborate accessory equipment in the shape of a platform as is used here.

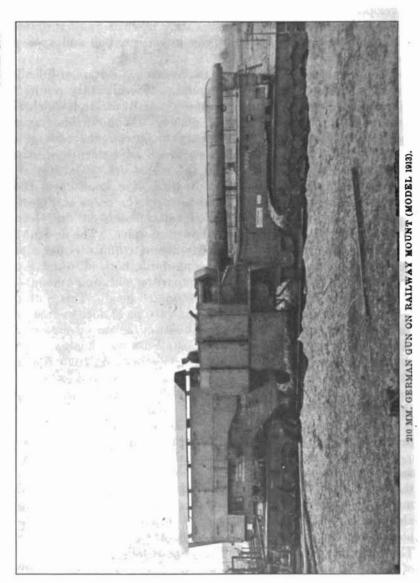
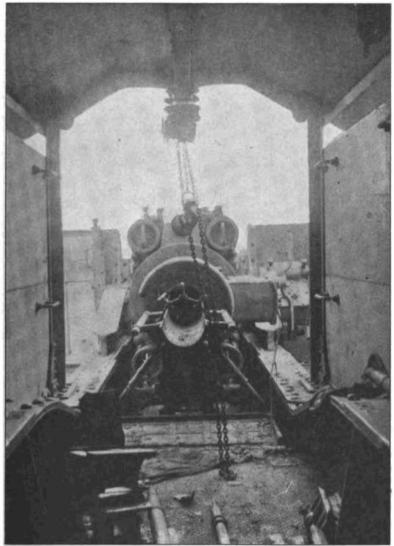
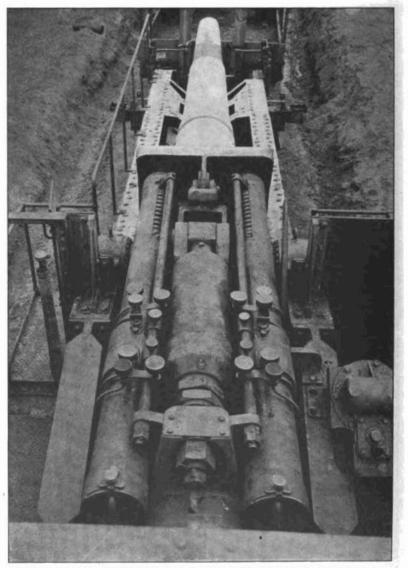


PLATE 373



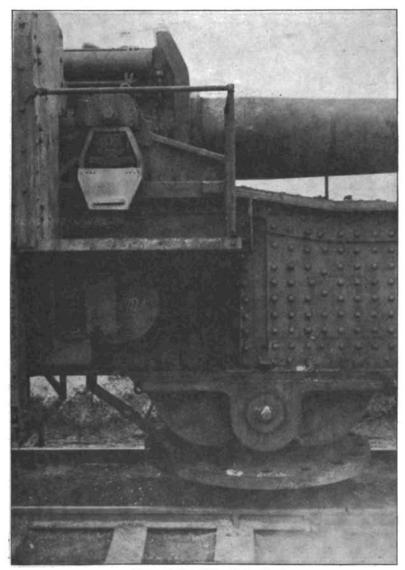
BREECH MECHANISM AND LOADING APPARATUS OF THE 210-MM. GERMAN MOUNT. 181768—21——31

PLATE 374

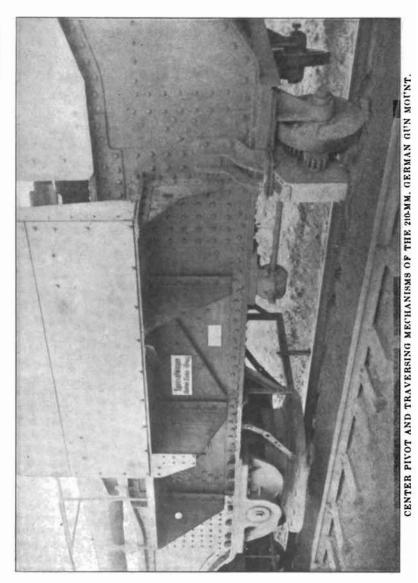


CRADLE, RECOIL CYLINDER, AND SPRING RECUPERATORS OF THE 210-MM. GERMAN GUN MOUNT.

PLATE 375



CENTER PIVOT, ELEVATING WORM, AND ANTI-FRICTION BEARING OF THE 210-MM. GERMAN GUN MOUNT.



19.—GERMAN 240-MILLIMETER HOWITZER ON RAILWAY MOUNT.(32)

- 351. This mount is of the cradle recoil type, firing either from the wheels with limited traverse or from a structural steel or reenforced concrete platform with all round fire. It is of the same general type as the 210-millimeter mount just described and only the differences between the two mounts will be described in detail. The mount examined bears the date "Essen 1918." It is illustrated on plates 377 to 383. Apparently, the mount was designed for a 240-millimeter gun, since the counterweight provided on the top of the cradle gives evidence of being a recent improvisation placed there to compensate for the difference in weight forward of the trunnions, between the gun and howitzer now mounted on it.
- 352. Gun.—The howitzer is a naval piece of 30 calibers over-all length and uses semi-fixed ammunition. The tube is rifled with 52 grooves twisting to the right at a uniform pitch of 1 centimeter in 10 centimeters. The breech block is of the Krupp sliding wedge type and is provided with a high-pitch screw for closing and a low-pitch screw for locking. The breech block is fitted with a mechanical firing mechanism.
- 353. RECOIL MECHANISM.—The recoil mechanism is of the hydropneumatic type and comprises two hydraulic recoil cylinders set into the cradle in the upper corners, and a pneumatic recuperator attached to the cradle in the center at the bottom. The pistons of the recoil cylinders are attached to the recoil band as shown on plate 379 and the forward end of the recuperator piston is connected with the bottom of the recoil hand by means of a cross head and two tension rods, plate 380. The length of recoil is about 1 meter. feature of this mechanism is the recuperator. The piston is a hollow plunger of uniform diameter facing the air directly and the packing which holds the air in, consists of four U-shaped leathers only. When the recuperator was disassembled, it had been standing for months without recharging but it still contained a very high pressure of air-The indicator was broken and it is not known exactly what the The recoil band of this howitzer is made in halves pressure was. and is bolted on, as shown in plates 379 and 380.
- 354. ELEVATING MECHANISM.—This mechanism is similar in general design to that on the 210-millimeter mount. The differences are that the main racks, plate 380, have outside instead of inside teeth and are of much wider face. An antifriction device of the rolling wedge type, plate 382, is employed. The double-speed transmission on the elevating gear, plate 381, is identical in design with that used on the 210-millimeter mount.
- 355. Traversing Mechanism.—Two systems of a design almost identical with those used on the 210-millimeter mount are provided:

The noticeable differences are that the truck traversing mechanism gives 2 degrees on each side of the center or 4 degrees total as against 2 degrees on the 210-millimeter mount, and the rear traversing rollers are housed in and geared together.

356. Gun Carriage.—The gun carriage is incorporated with the car body and is described in the next paragraph.

- 357. RAILWAY CAR BODY.—The gun is carried in a cradle of curious boxlike design, 45 inches by 52 inches by 105 inches, built up of castings and planed plates, plate 377. This cradle is suspended by means of its trunnions in cast-steel bearings mounted on the side girders of the car. As mentioned before, apparently the mount was originally designed for a 24-centimeter gun. Counterweights mounted above and below the gun and forward of the trunnions, plate 377, have apparently been added recently to compensate for the difference in the muzzle weight of the gun and howitzer. This cradle carries the recoil cylinders in its upper corners and the recuperator cylinders in the center at the bottom. The car body is similar in general design to that of the 210-millimeter mount, but differs considerably in its details. The car body is made up of two single web structural steel side girders connected by a number of structural steel transoms. Jacking beams are incorporated in the car body at the forward and rear ends, plates 377 and 383. These side girders are 39 inches deep over the front and rear trucks as against 28 inches for the 21-centimeter. This mount is likewise more liberally supplied with armor than the 21centimeter mount.
- 358. Anchorage. —See "Anchorage" under the 210-millimeter mount.
- 359. TRUCKS.—See "Trucks" under the 210-millimeter mount. They are identical.
- 360. Ammunition Supply System.—This is practically identical with that of the 210-millimeter mount, with the exception that the tray is not supplied with wheels and apparently is not used in carrying the shell. The shell is carried forward by means of the tongs, plate 392, and placed on the tray which is hooked to the breech of the gun.
- 361. Maintenance.—See "Maintenance" for the 210-millimeter mount. Some additional maintenance probably results from the use of a pneumatic recuperator.
- 362. DIFFICULTIES INVOLVED IN THE SERVICE.—See the same for the 210-millimeter mount.
- 363. MERITS.—See "Merits" for the 210-millimeter mount. The one exception is in the case of the antifriction device of the rolling wedge type, which does not appear to be so admirable a design as the roller bearing.

364. Demerits.—See "Demerits" for the 210-millimeter mount. Additional criticisms may probably be made on the construction of the cradle. On further study it might develop that there are some advantages in the use of this quite clumsy looking cradle, but none are apparent now. It is possible that this cradle is an improvisation and was so constructed as to avoid the making and machining of a large casting.

365. Although it possibly has no place here, it may be well to mention that, in these three mounts, the 210-millimeter, the 240millimeter, and the 280-millimeter, there are a great many differences in the design of details that do not seem to have any logical explanation. On the 240-millimeter mount the traversing rollers are housed and geared together, the elevating rack meshes on the outside, and antifriction device is of the rolling-wedge type, and the rear truck traverse is 4 degrees. On the 210-millimeter mount the traversing rollers are neither housed nor geared together, the elevating rack meshes on the inside, the antifriction device is of the roller type, and the rear truck traverse is 2.25 degrees. On the 280-millimeter mount the traversing rollers are housed and geared together, the elevating rack is straight, the antifriction device is of the roller type, and the rear truck traverse is 2 degrees. Apparently the three mounts can be operated on the same platform. Just why these minor variations in design were made is not at all evident.

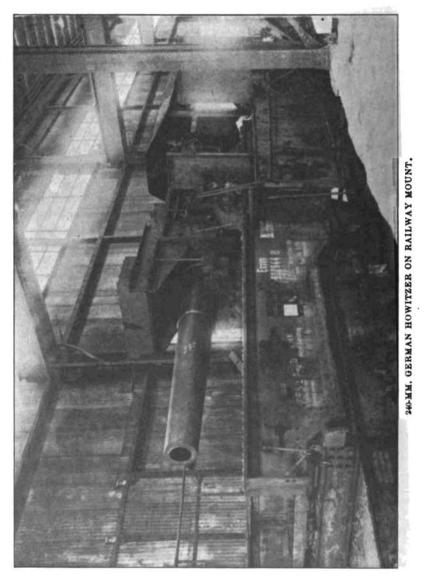
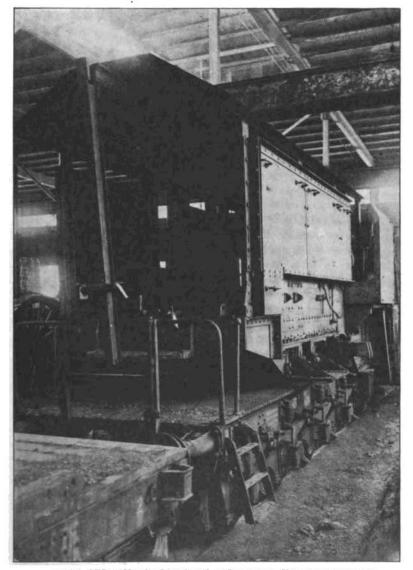
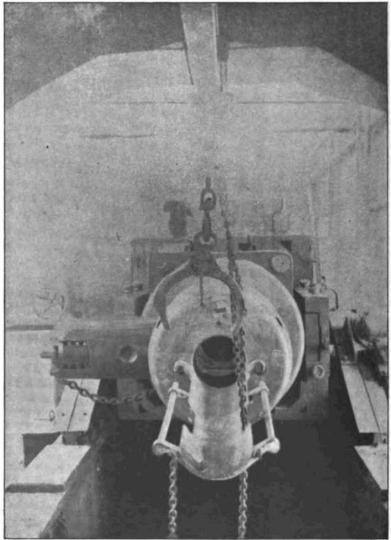


PLATE 378



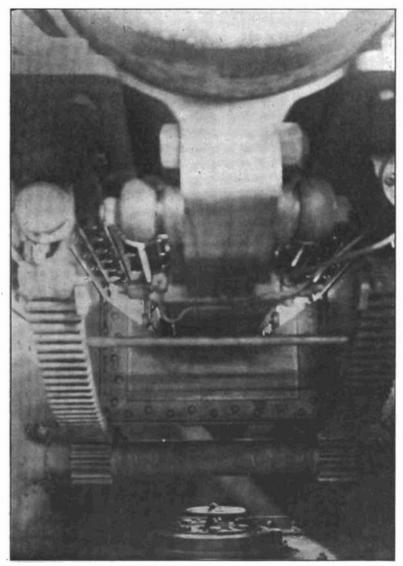
240-MM. GERMAN HOWITZER ON RAILWAY MOUNT (REAR VIEW).

PLATE 379



BREECH, CRADLE, AND LOADING TRAY OF THE 240-MM. GERMAN HOWITZER.

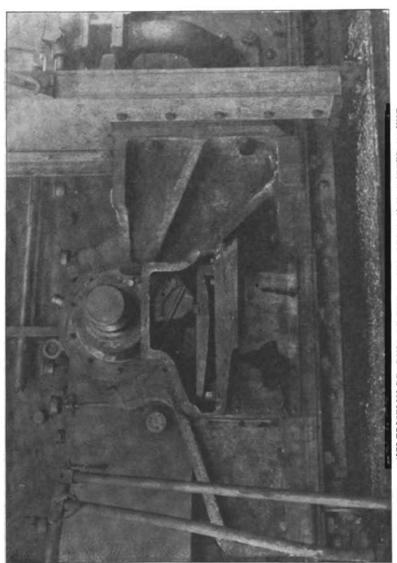
PLATE 380



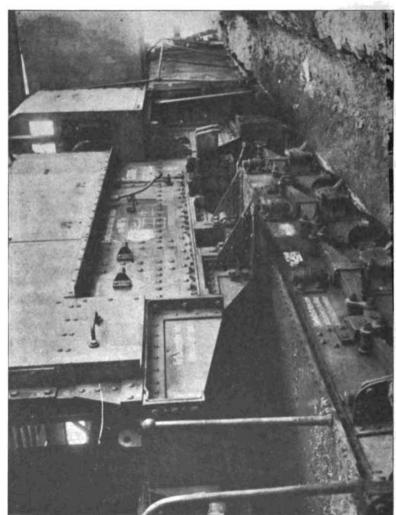
ELEVATING RACK AND RECUPERATOR OF THE 240-MM. GERMAN HOWITZER.



ELEVATING MECHANISM, DOUBLE-SPEED TRANSMISSION GEAR OF THE 240-MM, GERMAN HOWITZER MOUNT.



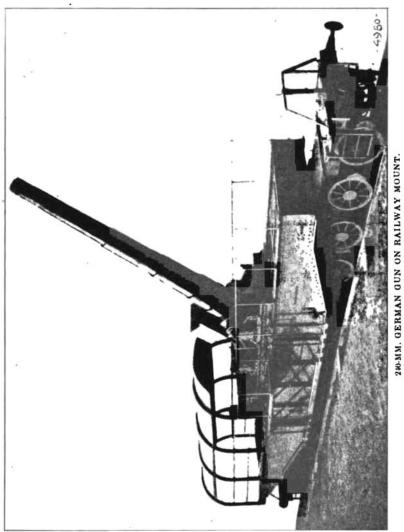
ANTI-FRICTION BEARING OF THE 240MM. GERMAN HOWITZER MOUNT.



TRUCK TRAVERSING MECHANISM AND JACKING BEAM OF THE MOMM. GERMAN HOWITZER MOUNT.

20.—GERMAN 240-MILLIMETER GUN ON RAILWAY MOUNT. (33)

366. On plate 384 a 240-millimeter gun is shown on a type of railway mount resembling more the 38-centimeter mount than the design used with the 21 and 24 centimeter mounts already described in detail. The writer has not had an opportunity to examine a mount of this type and to the best of his knowledge none of them were captured. No attempt will be made to describe it in detail, Attention is called to certain features easily seen on this plate. mount is carried on two four-axle trucks, the axles having inside iournals. This is the first German mount observed on which inside journals have been used. On the horizontal portion of the lower cords of the side girders a number of plates which appear to be key plates can be seen, and it is assumed that this mount was operated on a turntable type of emplacement somewhat similar in design to that used with the 38-centimeter railway mount. It is probable that the key plates mentioned engaged with similar plates on the racer of the emplacement. It is probable that hydraulic jacks were placed under the four corners of the car body after it was in position over the emplacement to raise the mount for the purpose of removing the trucks.



21.—GERMAN 280-MILLIMETER GUN ON RAILWAY MOUNT. (34)

367. This mount is of the cradle recoil car traverse type, firing either from the wheels with limited traverse or from a structural steel or reinforced concrete ground platform with all round fire. is similar in type to the 210-millimeter gun and 240-millimeter howitzer mounts already described and operates from the same ground Three batteries of these mounts operated from concrete platforms were included in the German defenses on the coast of (See Appendix III for description of these.) The mount examined and illustrated herein was captured by the British Fourth Army before Amiens, on August 8, 1918, in the great offensive being waged by the Allies at that time. It was exhibited for a time in a railway yard in Paris and later was taken to England. To the best of our knowledge this was the only mount carrying a gun of this caliber that was captured. The Belgian Army captured several 17centimeter mounts and one 38-centimeter mount, and the Americans have two 17-centimeter one 21-centimeter, and one 24-centimeter mount. These mounts are illustrated on plates 385 to 399, 36, 55 and 56.

368. Gun.—The gun on the mount examined is a 40-caliber naval piece of model 1914 of 42 calibers total length. The tube is rifled with 80 grooves having a uniform twist to the right of 1 centimeter in 10 centimeters. The breechblock is of the ordinary Krupp sliding wedge type and is fitted with a mechanical firing mechanism. As with all other large guns having this type of breech, this gun uses semifixed ammunition.

369. RECOIL MECHANISM.—The recoil mechanism is of the hydropneumatic type and comprises one pneumatic recuperator cylinder mounted at the bottom of the cradle in the center and two hydraulic cylinders likewise mounted on the bottom of the cradle and on either side of the recuperator cylinder, plate 36.

370. ELEVATING MECHANISM.—The elevating mechanism comprises two straight racks, plate 387, engaging with two pinions inclosed in floating housings and attached to one shaft. This shaft is connected by means of a worm, wheel, and shaft and on the right side of the gun with elevating handwheel shown near the elevation quadrant. This is the only railway mount so far observed in any of the armies in which the attempt has been made to use this straight rack, which is much more easily machined than any of the usual curved elevating racks. On the under side of the floating housings two rollers are carried on which the back of the rack rides and which hold the rack in perfect mesh with the pinions. These two racks are attached by means of heavy pins to the rear of a cradle. The cradle trunnions are provided with the same roller type of anti-

friction device used on the 21-centimeter mount already described. The mechanism used on this mount is shown on plate 388. An elevation arc, plate 403, is attached to the cradle on the right side.

371. Traversing Mechanism.—See "Traversing Mechanism" for the 21-centimeter railway mount. The design of the car traversing mechanism over the rear truck is shown on plates 390 and 391, and the mechanism used in giving the mount all round traverse is shown on plates 392 to 395. The traverse rollers on the 21-centimeter mount are separate and exposed, while on this mount, plate 396, they are housed in and geared together.

372. Gun Carriage.—The gun carriage is incorporated with the

car body and is described in the next paragraph.

- 373. RAILWAY CAR BODY.—The gun is carried in a cradle of the design shown on plate 36. The cradle is provided with a heavy counterweight just above the trunnions to raise the center of gravity of the tipping parts sufficiently to permit of easy elevating and depressing. This cradle is suspended by means of its trunnions in cast-steel bearings mounted on the side girders of the car body. Each of the trunnions is provided with an antifriction device of the design shown on plate 388. The car body is built up of two single web structural-steel side girders connected by a series of structuralsteel transoms and deck plates and the car platform is covered with light armor, plate 385. Both the traversing roller housings and center pivot trunnion bearings are bolted to the bottom of the side girders and serve to stiffen it. Jacking beams, which, in the case of the mount examined, had the jacks attached, plate 385, are carried under the forward and rear ends of the car body. The car traversing mechanism, a part of which forms the upper center plate over the rear truck, can be seen on plate 391.
- 374. Anchorage.—See "Anchorage" for the 21-centimeter mount. The emplacement shown on plate 397 was used with batteries installed along the Belgian coast. This battery is only about 1 mile north of Ostend. The designs of the concrete and structural-steel platforms and the emplacing jacks are shown on plates 55, 56 and 398.
- 375. TRUCKS.—The two trucks on this mount, plate 385, are practically identical. The frame is of structural steel and each carries five axles with outside journals. The brakes are operated by hand only, and the end and center wheels are provided with two brake shoes each. Above each spring clip there is a capstan head screw, identical in design with those used on the 21 and 24 centimeter mounts, which is run down hard on the clip to relieve the springs of undue strains in firing from the track.

376. Ammunition Supply System.—The ammunition car captured with this mount is a wood box car of apparently standard design,

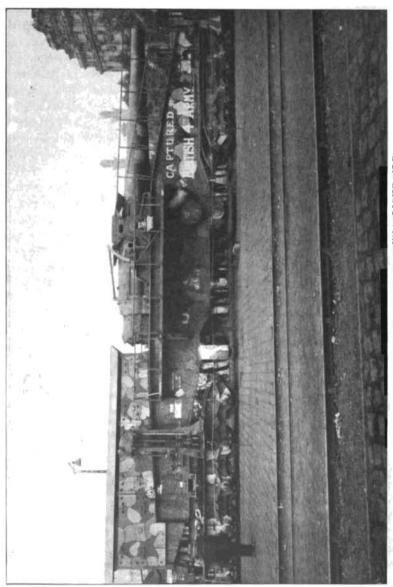
fitted with racks to carry 25 projectiles, plate 397. These projectiles are carried to the forward end of the car by means of an overhead trolley and are lifted through the roof of the car by means of a chain hoist on the end of the extension of the trolley track in the cab of the mount. It is carried forward by this second trolley, and placed on a tray attached to the breech of the gun, similar to those used with the 21 and 24 centimeter mounts. The projectile is rammed into the gun from this tray by hand. All of the projectiles in the car had an ogive of 10 calibers radius and all were fitted with false caps. The caps were placed on the projectiles as they were used. In the end of the cap there is a tapped hole through which a stick of wood is passed until it rests against the fuse. Considerable pressure is brought on this piece of wood when the small plug is screwed into the end of the cap. All of the projectiles captured were provided with time fuses of the 90-second clockwork variety.

377. MAINTENANCE.—There are no apparent difficulties in the maintenance of this railway mount, all parts of which are very simple and substantially constructed. The elevating, traversing, and loading mechanisms had all seen considerable service, and yet no apparent difficulties had developed. The trucks had likewise apparently given no difficulty. It is not known just what difficulty may have been experienced with the recoil mechanism, but probably comparatively little.

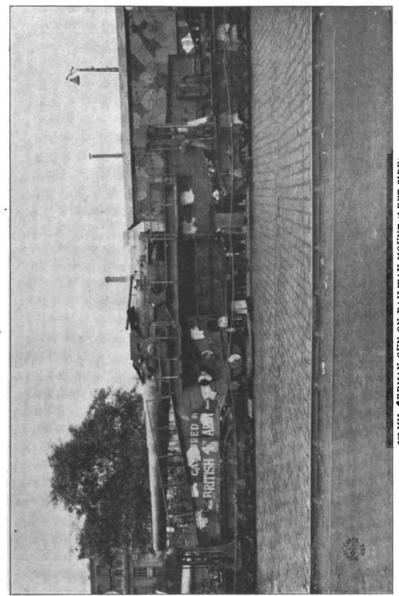
378. DIFFICULTIES INVOLVED IN SERVICE.—See same for the 21 and 24 centimeter mounts.

379. MERITS.—See same for the 21 and 24 centimeter mounts.

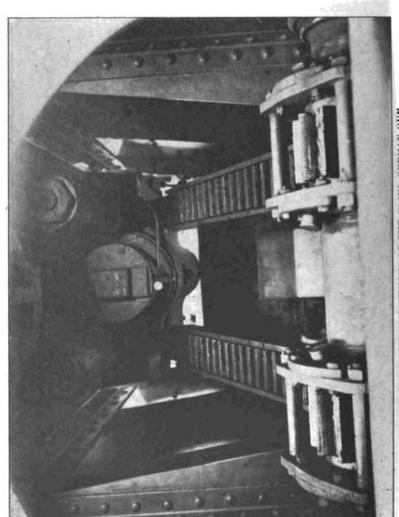
380. Demerits.—See same for the 21 and 24 centimeter mounts.



280-MM. GERMAN GUN ON RAILWAY MOUNT (RIGHT SIDE).

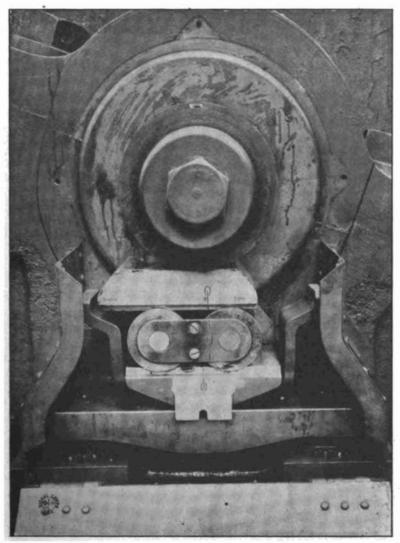


280-MM. GERMAN GUN ON RAILWAY MOUNT (LEFT SIDE).



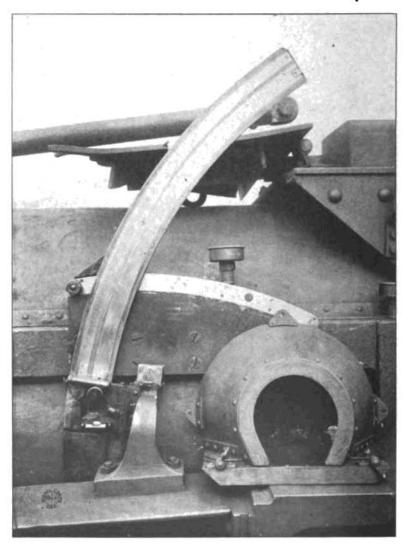
ELEVATING RACKS AND PINIONS OF THE 28C-MM. GERMAN GUN.

PLATE 388



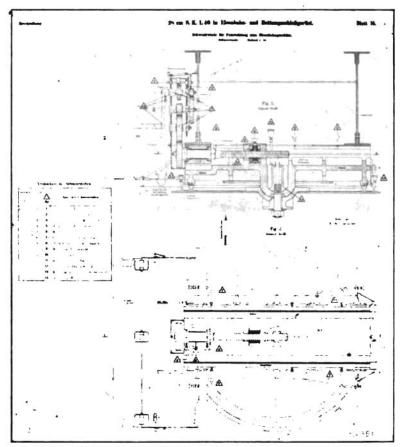
ANTI-FRICTION BEARING OF THE 280-MM. GERMAN GUN MOUNT.

PLATE 389



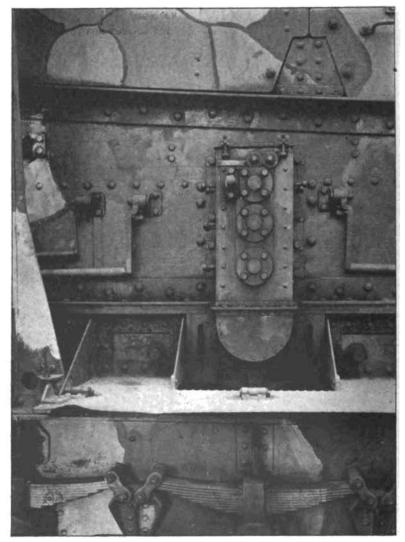
ELEVATING ARC OF THE 280-MM. GERMAN GUN MOUNT.

PLATE 390

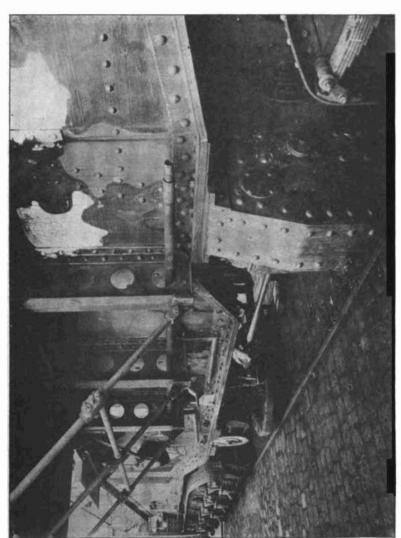


CAR TRAVERSING MECHANISM OF THE 280-MM. GERMAN GUN MOUNT.

PLATE 391



CAR TRAVERSING MECHANISM OF THE 280-MM. GERMAN GUN MOUNT (GEAR CASE ON LEFT SIDE OF MOUNT).



CENTER PIVOT AND TRAVERSING MECHANISM OF THE 240-MM, GERMAN GUN MOUNT.

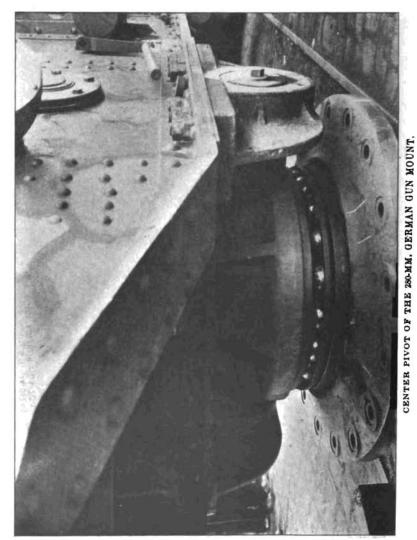
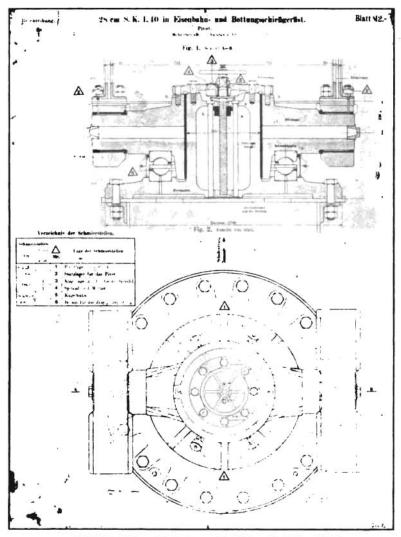
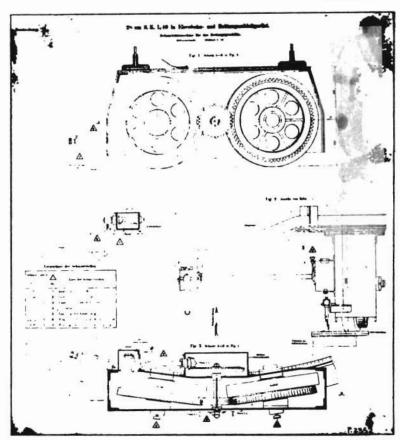


PLATE 394



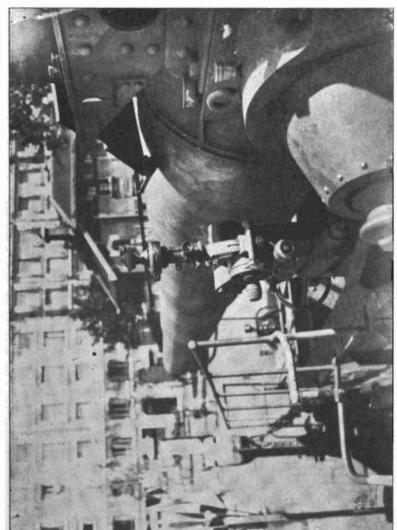
CENTER PIVOT OF THE 280-MM. GERMAN GUN MOUNT.

PLATE 395

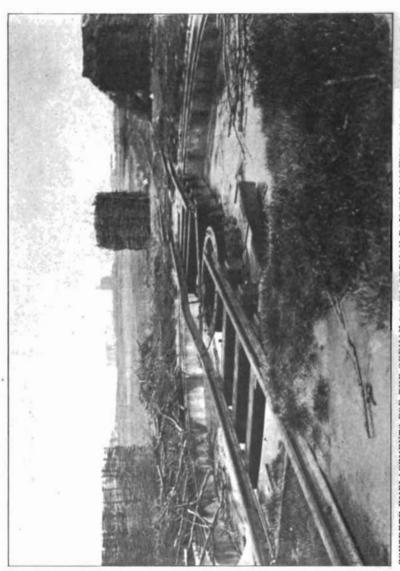


TRAVERSING MECHANISM OF THE 280-MM. GERMAN GUN MOUNT.



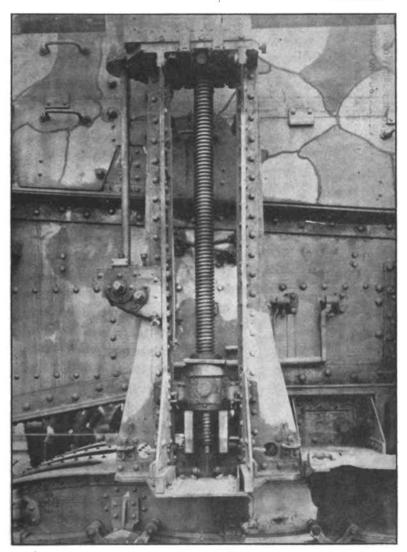


PANORAMIC SIGHT OF THE 280-MM. GERMAN GUN MOUNT.



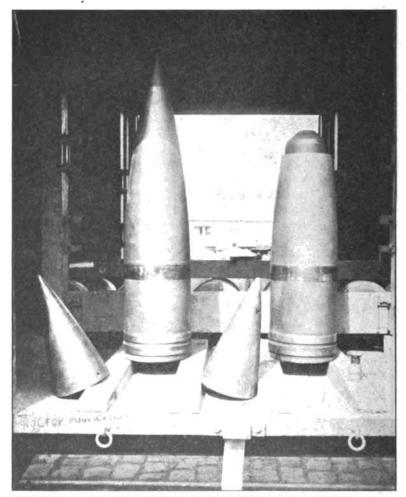
CONCRETE EMPLACEMENTS POR THE OERMAN 20-MM, GERMAN RAILWAY MOUNTS ON COAST OF BELGIUM.

PLATE 398



EMPLACING JACK OF THE 280-MM. GERMAN GUN MOUNT. 181768—21——33

PLATE 399



PROJECTILES AND AMMUNITION CAR FOR THE 280-MM. GERMAN GUN MOUNT.

22.—GERMAN 380-MILLIMETER GUN ON RAILWAY MOUNT. (35)

381. This mount, plates 400 and 401, is of the cradle recoil type. firing from the wheels with limited traverse to an elevation of about 18 degrees, or from a structural-steel turntable type of ground platform with all round fire. The mount examined was captured by the Belgians and is in serviceable condition. Emplacements on which it could have been operated have been found in only two places, the one in the Forest of St. Gobain, west of Laon, and the other in the Bois de Chatelet, about 5 miles north of Chateau Thierry. All evidence available to-day indicates that while it was being operated from the emplacement in the Forest of St. Gobain it was serving as a mount for the long-range guns, all of which were made from worn-out 38centimeter, 45-caliber naval guns. The mount bore the date of February, 1918, at which time it was probably completed by the firm of Krupp, and the evidence available to date indicates that it was the only mount of this design that they had. Gen. Arnoulde, Chief of Artillery of the Belgian Army, informed the writer that the mount had been found on a special track in the Bois de Leugenboom near the permanently emplaced 38-centimeter gun in that same woods, about 10 miles south of Ostend. There was no evidence that it had ever been operated from this position.

382. Gun.—The gun found on the carriage inspected was of the 1916 model and was number 33L. The total weight is 77,552 kilograms. The total length of the gun is 17.13 meters and the distance from the face of the breech block to the muzzle is 16.13 meters, making the gun about 42 calibers long. This is very significant, considering the fact that the gun is supposed to have a range of 55 kilometers (50,095 yards). The breech is of the standard Krupp sliding wedge type, the wedge being operated by one handle through a series of spur gears, to one screw.

383. Apparently the gun, plates 400 and 402, is built up of five main sections; the tube is reinforced by two hoops which are further reinforced by one jacket extending from the breech forward about two-thirds of the length, and a breech section attached to the last named jacket by the recoil lug. In the case observed, the tube has evidently lengthened to the extent of about 0.562 inches. The evidence of this is the extension of the tube beyond its original position with reference to the end of the forward hoop a distance of about 0.187 inches and the parting of the forward hoop from the hoop to the rear to the extent of 0.375 inches. This same condition was observed on several other guns of this design. The number of grooves is 100. The width of the grooves is approximately 0.219 inches, and the width of the lands 0.236 inches. The lands show slight signs of wear on the driving side and copper was visible both on

the lands and in the grooves at the muzzle of the gun, although not to such an extent as probably to have much effect. The diameter of the powder chamber is 42.5 centimeters. The recoil lug to which the two pistons of the hydraulic cylinders and the one piston of the recuperator cylinder are attached likewise serves to prevent rotation of the gun. It is forked at the bottom and bears on two sides of the recuperator cylinder which serves as a guide, plates 403 and 404. In this connection, it is significant that with every heavy German gun observed, rotation of the gun was prevented in this same manner, the breech lug having an extension which either bore on two sides of a recuperator cylinder or between two recuperator cylinders. It is certain that there were no cases of a spline on the gun sliding in a way in a cradle. In traveling, the gun is locked in battery by the very simple device shown on plate 402.

384. This gun is identical in design with the guns of the Battery Deutschland and the Battery Pommern, at Leugenboom, described in Appendix III. The guns of these batteries are accredited with a maximum range of 55 kilometers. In the report which was examined in Gen. Arnoulde's office, the range was given as 42 kilometers. There is no question but that the Battery Pommern fired on the city of Dunkirk, requiring a range of 45 kilometers. Whether the Battery Deutschland, which is 2 kilometers northeast of Ostend, likewise fired on Dunkirk is a question. The basis for the statement in the Bulletin de Reseignements de l'Artillerie of January-February. 1918, crediting these guns with a range of 55 kilometers is not known. Whether the provision for an elevation of 55 degrees has any real connection with the unusual range of a gun 42 calibers in length and credited with a muzzle velocity of 800 meters per second, is not known definitely. It seems certain, however, that the specification given the designers for a maximum elevation of 55 degrees resulted in the type of elevating mechanism described later.

385. RECOIL MECHANISM.—The recoil mechanism is composed of two recoil cylinders and one spring pneumatic recuperator cylinder, all located on the bottom of the cradle, plates 403 and 404. Each of the recoil cylinders is a separate cylinder carried in brackets cast on the cradle and each is provided with a buffer approximately 32 centimeters long. The filling plugs are on the ends of the buffers. The maximum length of recoil is 1.3 meters. This distance is, of course, approximate, and was arrived at after careful examination of all of the apparatus. In a report examined in the office of Lieut. Gen. Arnoulde at Brussels, the length of recoil was given as 1.15 meters. On inquiry, it was found that this was likewise an estimate. Two rods screwed to the recoil lug and extending to the rear, plate 403, carry a cross head to which the piston of the recuperator cylinder is

attached. The recuperator cylinder, plates 405 and 406, is likewise a separate cylinder carried in brackets cast on the cradle, and at the rear on both sides it is planed to serve as a guide for the recoil lug, to prevent rotation of the gun.

386. ELEVATING MECHANISM.—The elevating mechanism of this mount is unique in several respects. Provision is made for elevating the gun from 0 degrees, the loading angle, to 55 degrees. It is composed of two straight racks, plate 407, driven through pinions, a wormwheel, worm, a double speed transmission, sprockets and chains, by four two-man handles, plates 408 and 409. The straight racks slide in ways which are parallel to the inclined lower face of the forward end of the side girders. It was necessary to put them in this position to secure sufficient movement to elevate the gun to 55 degrees. At the lower end, they are connected with each other by a heavy shaft, plate 407, to which are attached the two connecting rods running up to the bottom of the cradle. It will be observed, plate 409, that provision is made for two handles on each side of the car, each for two men. A double speed transmission, similar in design to those used on the 21 and 24 centimeter mounts is incorporated in this mechanism. The ratio on the low gear is 4.125 turns of the handle for one degree of movement of the gun. One man can operate the elevating mechanism with some difficulty at low gear. It seems probable that eight men could operate the high gear without serious difficulty. The gun and cradle were identical with five others observed in the coast defenses of Belgium. On all of the other guns, however, the elevating mechanism included double telescoping screws. It is probable that this gun when used on a ship or in the coast defenses was likewise so elevated, and that it was impossible to accommodate this mechanism on a railway mount and secure the elevation desired. It is likely that under the specification of such an extreme elevation no other type of mechanism could have been adapted to this cradle and mount without serious difficulty. Judging from the diagram, plate 404, which was made up from measurements of the gun and cradle and the estimated length of recoil of 1.30 meters, it seems probable that the gun can be fired from the track, the mount operating as a rolling mount, to an elevation of 18 degrees, 30 minutes. If the length of recoil is 1.15 meters, as given in Gen. Arnoulde's report, it is probable that an elevation of as much as 20 degrees can be secured. The gun can be fired above 18 degrees only from a special emplacement.

387. Traversing Mechanism.—This mount is provided with a car traversing mechanism installed on the front span bolster, giving a maximum traverse of 1 degree on each side of center. This mechanism, which includes the usual screw, plate 411, is operated through a

series of spur gears and chains, plate 412. There seems a good reason for providing a high and low speed elevating mechanism, but just why the designers provided both high and low speed on this traversing mechanism is not known. In comparing this design with French and American designs, it is significant that no rollers are provided between the body of the mount and the span bolster. Cast-steel shoes narrowing down to a wedge are provided on each side, plate 426. The designers evidently preferred to count on an ample supply of man power rather than provide the usual rollers. A second traversing mechanism for all-round firing is installed in the emplacement, plates 419 and 420. In this case the racer of the emplacement rests and rotates on 112 8-inch steel balls. A complete circular traversing rack made up of angles and steel pins is bolted to the structural steel base, plate 419. A pinion carried on a vertical shaft on the side of the racer which corresponds to the rear of the carriage engages with this rack, and the mechanism is driven either from two 2-man handles on shafts carrying a worm engaging with a wormwheel on top of this vertical shaft or by means of four handles carried in gear cases on either side of the mount, plate 420. Motion is communicated to the vertical shaft from these four handles through two shafts carrying two universal joints each. These latter handles are apparently the ones ordinarily used, if one may judge from the scheme of operation shown on plate 422.

388. Gun Carriage.—The gun carriage is incorporated in the car body and will be described in the next paragraph.

389. RAILWAY CAR BODY.—The cradle is a cylinder of simple design having ribs at long intervals and of a depth of only about 3 centimeters. Other cylinders observed for the same design of gun were without any ribs whatever. The walls of the cylinder have a minimum thickness of 10 centimeters and a maximum thickness of 13 centimeters over the ribs. The design of the antifriction mechanism is shown on plate 414. As shown on plate 411, a counterweight in two sections is attached to the top of the cradle. Both sections can be raised and locked together, or, if desired, the rear section raised and locked in place by the two tie-rods. The railway car body, plates 400, 413, 414, and 415, is made up of two single-web side girders connected in the front and rear by heavy structural-steel transoms and further reinforced in the front by the heavy cast-steel housings for the elevating mechanism. The trunnion bearings are of cast steel and are simply bolted to the top chord with single keys to the rear of them. These single keys have the positive backing of one top cover plate each. The face of the horizontal section of the lower chord of the side girders is planed and is provided with a key at each end, plate 416. Eight 2-inch holes are provided in each lower chord

at the front end and six at the rear. The purpose of the hooks shown on the front is not known.

390. The designers avoided the use of sharply curved angles, plate 415. There are only two slight curves on the angles of the lower chord. The working platforms provided on each side to the rear of the trunnion seat are locked in their traveling positions, as shown on plate 425.

391. Anchorage.—The gun can be fired to a maximum elevation of 18 degrees 30 minutes with the mount operating as a rolling mount. Above this elevation the trucks must be removed and the mount is operated from a fixed emplacement.

392. In August, 1918, when the German Army had retired from the salient between Soissons and Rheims, the emplacement shown on plates 417 and 418 was found in the Bois de Chatelet. All evidence indicated that this emplacement had not been used in this position. It was simply in process of erection when it was abandoned. The Germans attempted to destroy it, but succeeded only in ripping loose a few plates. At the time that this emplacement was captured, no descriptions of any kind were available of the carriage for which it was intended. The writer's failure to find any emplacement in Belgium from which the mount could be operated led to a search for emplacements in France, and an examination of the emplacement shown revealed the fact that it was the one sought.

393. The mount is run in on the emplacement in a position shown approximately on plate 417. It is then raised by four jacks, one of which can be seen in the left foreground on plate 419, and the trucks removed. The rotating section of the emplacement is then turned 90 degrees, and the carriage lowered onto the side girders. In the right center of plate 417 is shown one of the key plates, which corresponds to a similar plate on the bottom chord of the carriage girders, plate 426. The six bolt holes shown in the key plate on plate 418 correspond to the six holes in the lower chord on plate 426. On this plate only the bolt holes on the outside of the girder web are visible. From the fact that the key plates for the forward end must have eight bolt holes and those for the rear six, it is evident that the traversing mechanism is located on the part of the emplacement corresponding to the rear of the carriage.

394. It is necessary to install two auxiliary construction tracks on either side and parallel to the approach track for the service of the Gantry crane used in installing the emplacement. One of these tracks is shown on plates 417 and 418 and both are shown in both elevation and plan on plates 419 and 420. The emplacement, as well as the Gantry crane used in the work of installation, are shown on plate 421. German handbooks allow a period of three weeks for the

installation of the structural-steel emplacement. The mount is shown completely installed and in operation on plate 422. This plate is made from a cut contained in a printed publication of the Krupp Co., which manufactured the mount.

395. Camouflage.—In the case of the emplacement found in the Bois de Chatelet, sockets were placed in the center of the approach track at intervals of about 30 feet, into which trees with trunks up to about 6 inches could be placed for the purpose of concealing these tracks.

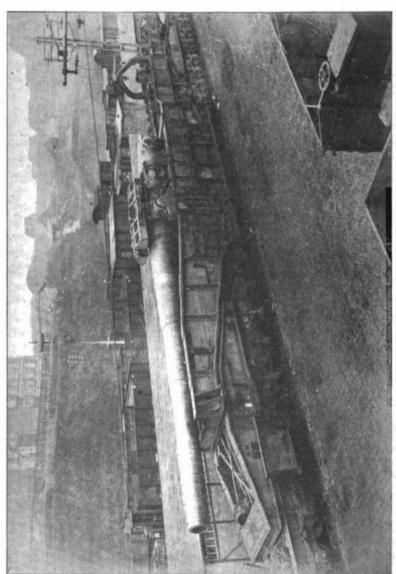
396. Trucks.—All of the trucks, as well as the span bolsters, are constructed entirely of structural steel, plate 401. The front trucks contain five axles each and the rear trucks four axles each. The journals are approximately 14 centimeters in diameter by 32 centimeters in length, and the wheels are 95 centimeters in diameter. On the front trucks, three wheels have two brake shoes each. On the rear trucks, the end wheels have two shoes each and the inner wheels one shoe each. The braking is done by hand only. A portion of the circular track on which rubbing plates attached to the span bolster on each side bear, can be seen on the front truck, plate 400. There are no rollers on any of the trucks or bolsters. The axles are equalized in pairs only, the center axles of the front trucks having no connection with the others, plate 423. The various dimensions of the trucks are given on plate 401.

397. Ammunition Supply System.—The provision made for supplying ammunition when the mount is operated on the emplacement is shown on plate 424. This narrow-gauge ammunition track can be seen likewise around the pit on plate 422. The indications are, from plate 422, that the track formed a loop around the pit in this case and that it was not a complete circle with turntable as was found in other emplacements in Belgium. A removable plate can be seen between the shot truck rails on the operating platform of the mount, plate 425. Over this plate is a light bridge, in the center of which is seen a ball on the end of the cable used in hoisting projectiles through the hole in the floor. The cable (0.5-inch) runs over a series of pulleys to a small drum in the box on the top of the left-side girder.

398. The ammunition is supplied from the storehouse over the narrow-gauge track already mentioned, the portion of the track around the pit being under the opening in the working platform. The projectile is raised by means of tongs attached to the hook under the ball and when at the top of the bridge the shot truck is run forward and the projectile placed on it. The shot truck inspected has no buffers, but four holes can be seen in the flange on the front which may have been provided for the attaching of a pad of some sort. The clear space over which the men could get up speed with the truck is about 5 meters. The gun is loaded at 0 degree ele-

vation. It is understood that the projectiles of the 38-centimeter gun of the same design at Leugenboom were rammed by 12 men. It is probable that the same number of men were used on the railway mount.

- 399. When the mount is operated as a rolling mount, the ammunition is supplied directly from the ammunition car. This necessitates the use of the extension to the car body, which extension, by the way, gives one the impression of having been an afterthought. This extension is pinned to the rear of the car body and is likewise connected by means of the two tie rods shown on plate 426. These tie rods do not seem absolutely necessary since the weight of the extension is carried by the rear truck. When the shot truck is at the end of the extension, the projectile can be placed upon it from the trolley that extends a short distance from the end of the ammunition car. When operated as an emplacement mount the extension of the car body was removed.
- 400. Maintenance.—There seems to be no evidence that this mount involved any difficult problems of maintenance. The design is simple throughout and quite sturdy. It is not known how much difficulty they may have had in maintaining the desired air pressure in their recuperator cylinder. It will be observed on plate 413 that a small pump is provided on the left side of the mount, which presumably was provided for charging the recuperator. A gauge at the rear of the recuperator cylinder gave evidence of the existence of a floating piston. The gauge on the top of the cradle, plate 402, is capable of registering a pressure of 250 kilograms per square centimeter. If the pressure maintained in the recuperator was even half the pressure which the gauge was capable of registering, it is possible that they may have had some difficulty in maintaining their recuperator.
- 401. DIFFICULTIES INVOLVED IN SERVICE.—The mount is operated above 18 degrees 30 minutes from an emplacement of the type shown on plates 417 and 418. Any such contrivance as this is considered a decided nuisance and would not be tolerated in our own designs; neither would it be tolerated by any of our allies. It is significant that in German handbooks the time allowed for installing gun emplacements is usually from three to five times as great as that permitted in the American Army. It is probable that the full three weeks allowed was required for the installation of this emplacement. No other difficulties are apparent in the service of this mount
- 402. Merits.—The simple design of cradle, generally simple design of the mount throughout, convenient ammunition supply system and high elevation, may be classed as merits.
- 403. Demerit.—The necessity for the use of an emplacement of this type for the operation of the mount at high angles is a decided demerit.



390MM. GERMAN GUN ON RAILWAY MOUNT.

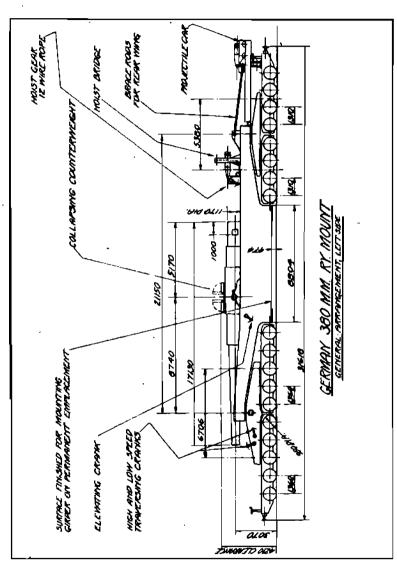
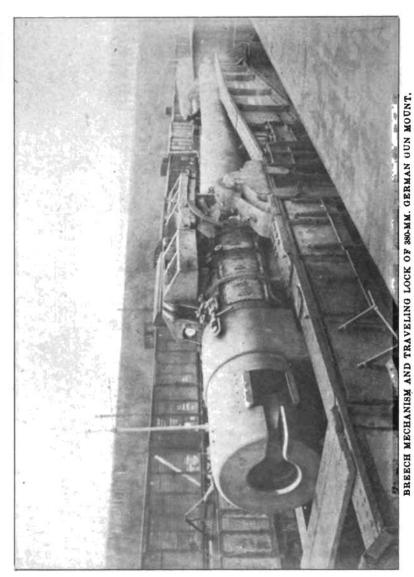
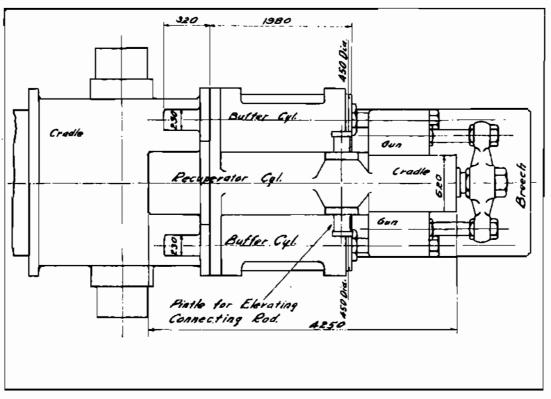
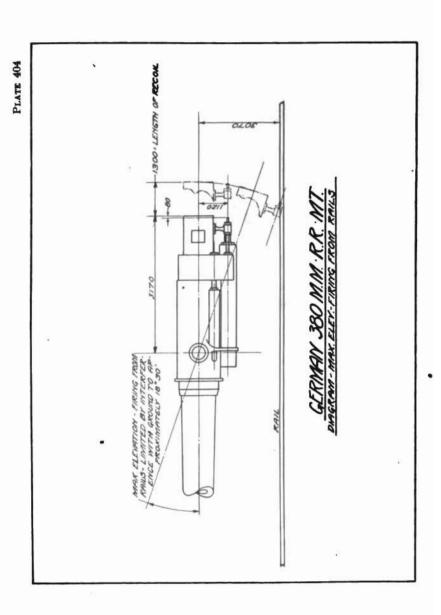


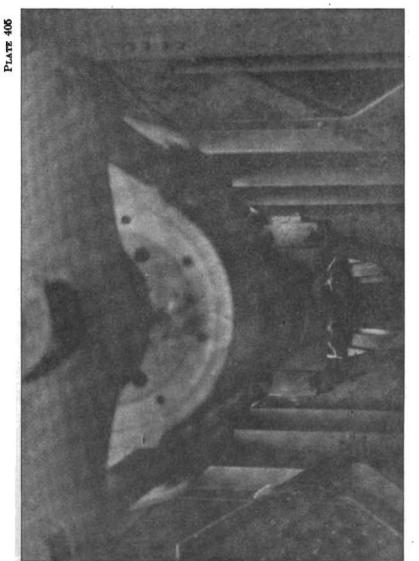
PLATE 401





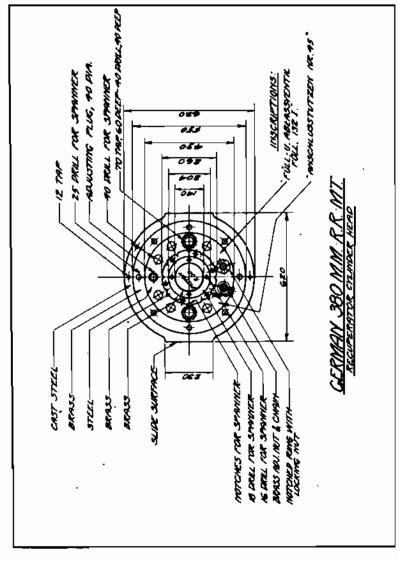
GERMAN 380-MM. RAILWAY MOUNT. RECOIL AND RECUPERATOR MECHANISM-BOTTOM PLAN.

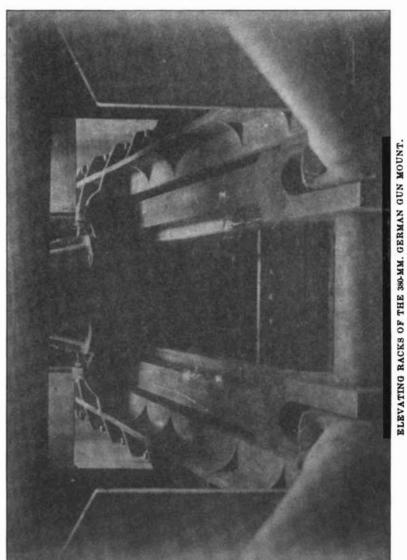




RECUPERATOR CYLINDER OF THE 380-MM. GERMAN GUN MOUNT.







181768—21——34

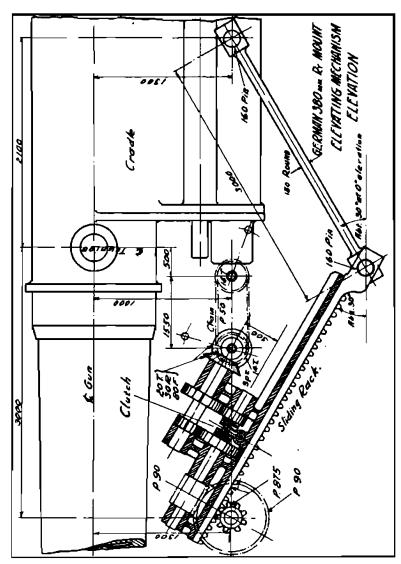
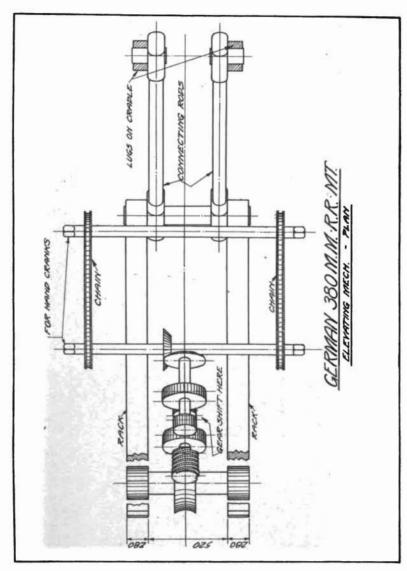
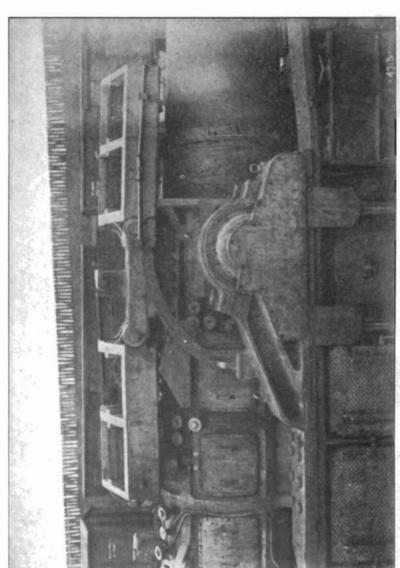
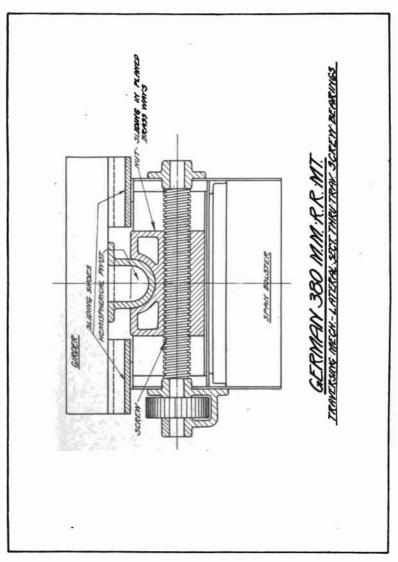


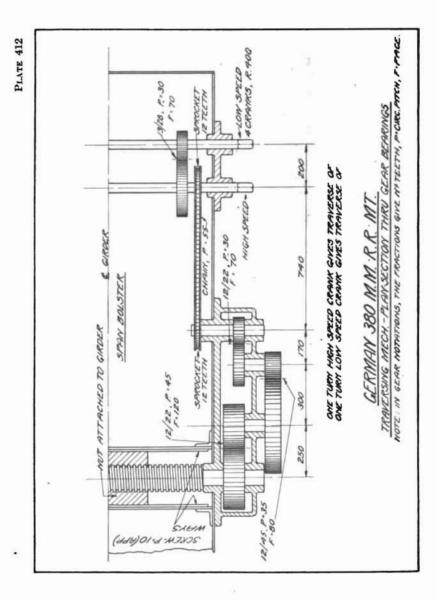
PLATE 408

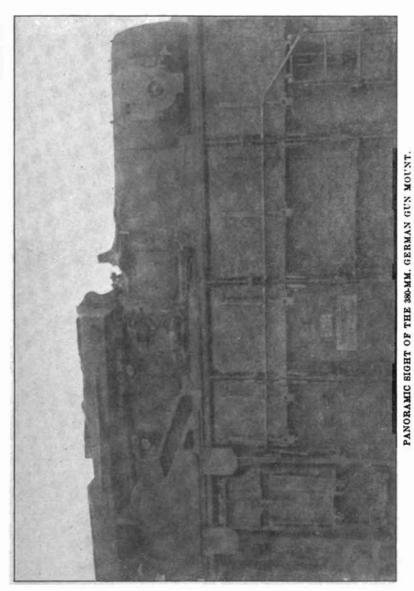


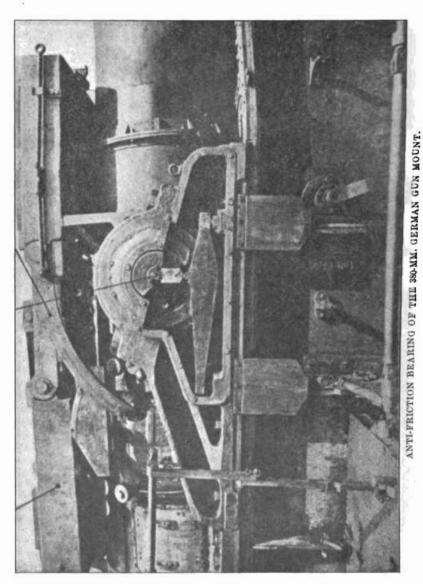


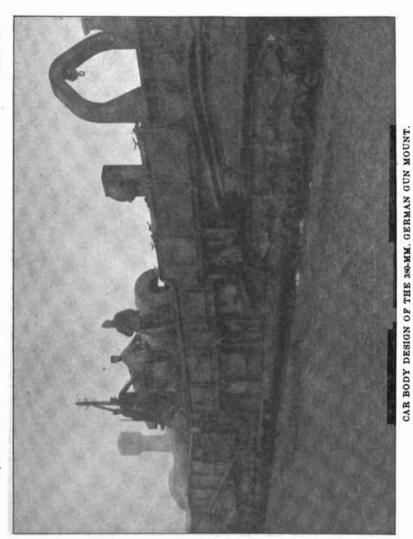
COUNTERWEIGHT AND ELEVATION ARC OF THE 30-MM. GERMAN GUN MOUNT.

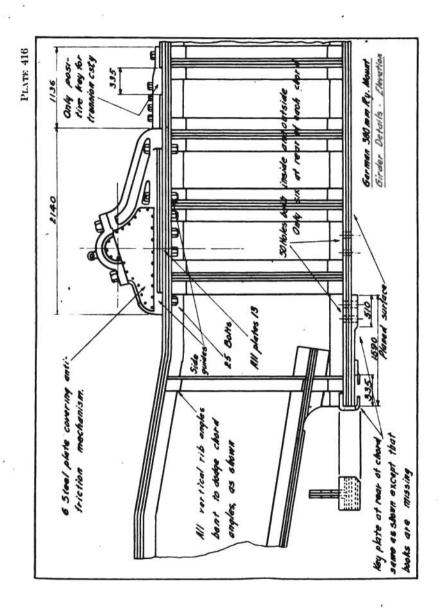


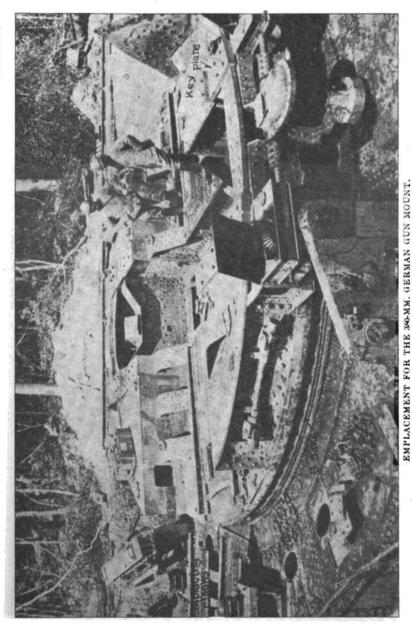


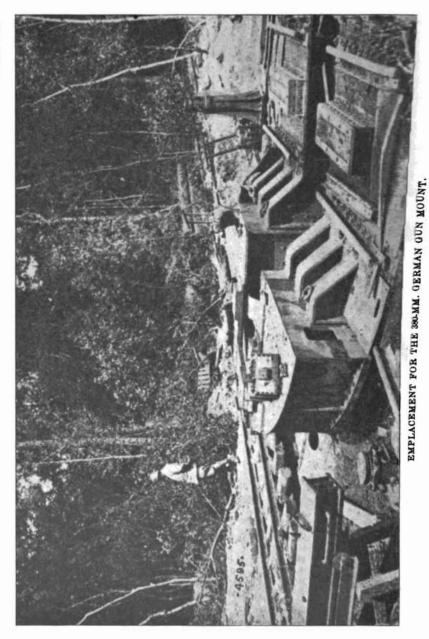


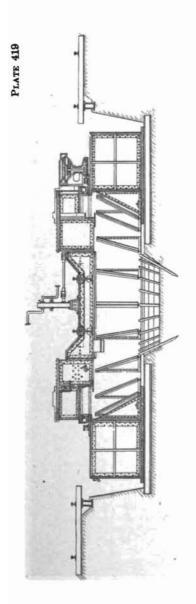


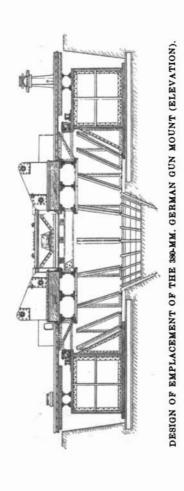


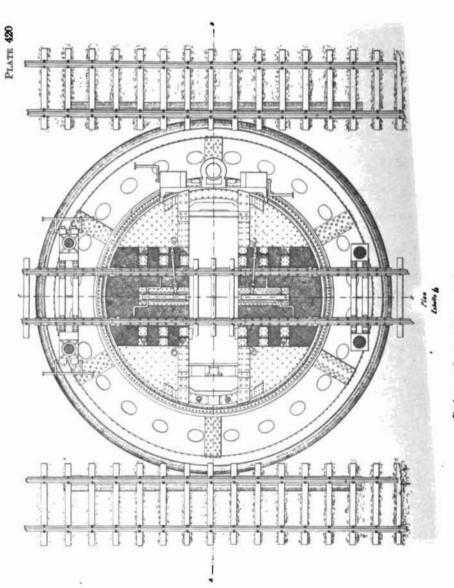






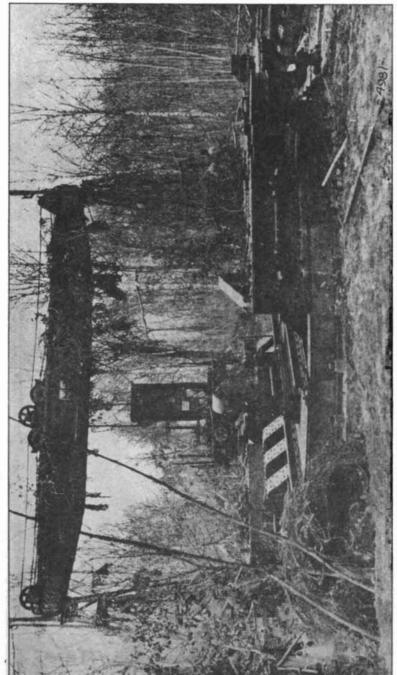




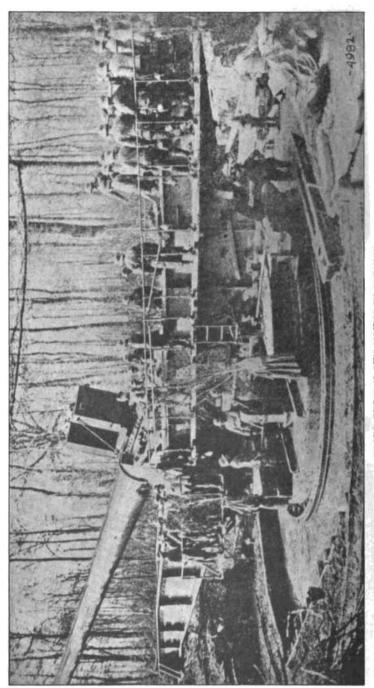


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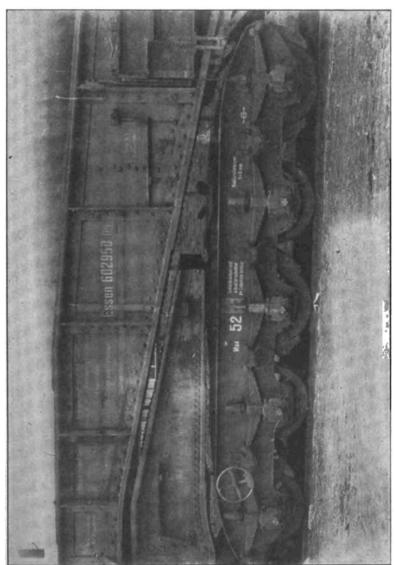
DESIGN OF EMPLACEMENT FOR THE 380-MM, GERMAN GUN.



GANTRY CRANE USED IN INSTALLING EMPLACEMENT FOR 39-MM. GERMAN GUN MOUNT.



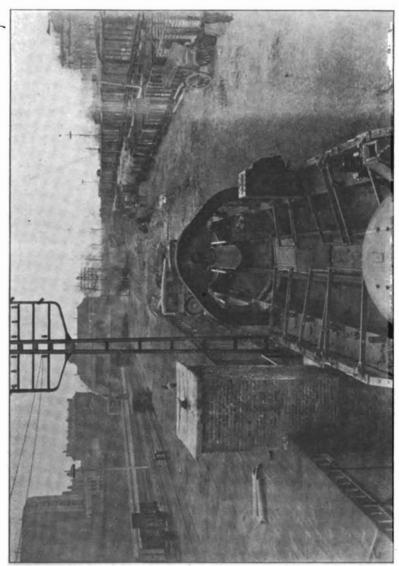
3SO-MM. GERMAN GUN MOUNT IN SERVICE,



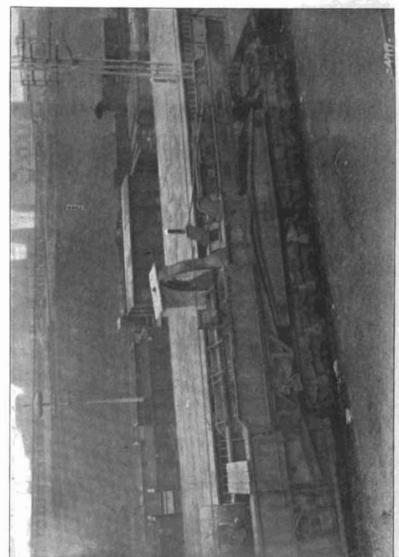
FRONT TRUCK OF 380-MM. GERMAN GUN MOUNT.

181768—21——35

PLATE 424 TRANERSING GEAR



OPERATING PLATFORM, SHOT TRUCK, AND AMMUNITION HOIST OF THE 380-MM. GERMAN GUN MOUNT.



CAR BODY EXTENSION AND REAR TRUCK DESIGN OF THE 380-MM. GERMAN GUN MOUNT.

SECTION 4.

PRACTICAL QUALIFICATIONS OF RAILWAY ARTILLERY FOR LAND WARFARE AND COAST DEFENSES.

404. To arrive at a proper conclusion with reference to the qualifications desirable in railway artillery, the relative merits of various details of design, as brought out in sections 1 and 3, will be considered first. Next, the various services required of the pieces will be given as discussed in section 2, and the general characteristics necessary in a mount to satisfy each service will be determined. Finally, on the basis of the above discussions, the best combination of design details to satisfy the requirements of each mount will be recommended.

RELATIVE MERITS OF DESIGN DETAILS.

405. Design details will be considered under the same headings used in describing them in section 3. In addition, attention will be given to special requirements for coast defense.

406. Gun.—Practically all of the guns used on railway mounts are of old or obsolete design. None of the novelties of design brought out by the war were developed to a point of actual utilization on railway mounts. A few of these new ideas are briefly described below, however, as they may develop to some importance in relation to railway artillery.

407. Autofrettage is a system of gun-tube construction in which the distribution of initial stresses (which is ordinarily obtained by the shrinkage of concentric rings, one upon the other) is attained in a single homogeneous tube, or better, in one tube and one jacket, through the application of internal hydraulic pressure. This system has not yet been applied to the manufacture of anything larger than field guns. It has been used, however, in the making of the French long-range gun. The 33-meter tube of 21 centimeter bore, used in converting a 34-centimeter, 45-caliber naval gun into a long-range gun, was placed in the gun cold and expanded by hydraulic pressure. The hoop placed over the projecting portion of the tube was likewise put on cold and the tube expanded into it by hydraulic pressure.

408. "Artillery C" is a term used by the French to designate an experimental system of M. Charbonnier, in which copper rotating

bands are replaced by machined rifling on the shell. The rifling in the gun is made to correspond, and the shell is made longer and heavier than normal. Experiments have been made in 75 and 155 millimeter field guns along this line, in which shells up to 9.5 calibers in length and weighing 60 per cent more than the regulation shell, were fired and attained ranges up to 35 per cent in excess of the range for the standard shell.

409. The turbo-cannon of Lieut. Delemerr-Mayo, of the French Army, is a gun without rifling, in which the rotational velocity is given the projectile by the impact of the powder gases on special vanes. Such tests as were made indicated rotation of the projectile, but no further conclusions were possible.

- 410. Muzzle brakes, or gas deflectors, for reducing recoil have been experimented on by Lieut. Bory and Capt. Galliot, as well as in the American Ordnance Department. The best results so far attained in experiments are a reduction of 40-60 per cent in recoil energy on the 75-millimeter field gun and a reduction of 83 per cent on a 3-inch seacoast gun. Measurements taken of the atmospheric pressures in the case of the seacoast gun indicate that the gun crew is not in any danger from the outwardly deflected gas stream.
- 411. RECOIL MECHANISM.—The various recoil systems were discussed very fully in section 1, and the following points were brought out:
 - (a) Cradle recoil with air recuperator is the highest development of recoil systems.
 - (b) Top carriage recoil is obsolete, being particularly unsuited to high-angle fire.
 - (c) Sliding recoil is unsuited to small guns because the time of firing can not be reduced below a minimum which is too great for the efficient service of such guns. Without the use of a cradle, it is unsuited also for the very largest guns, on account of excessive trunnion forces. It is very satisfactory for medium and large calibers.
 - (d) Rolling recoil is similar to sliding recoil in regard to the points mentioned above. A rolling mount requires less track preparation than any other type. In all known types of rolling mounts cradles have been used, making them more complicated than the sliding mounts.
- 412. Mounts with rolling or sliding recoil must be pushed back into battery after firing. This is accomplished on the lighter of the sliding type mounts by the use of a hand translating mechanism, consisting of a crank, a train of gears, and some chains leading to one or more of the axles. In the mounts constructed to date one translating mechanism is provided on one or two of each four to six

axles, and the ratio of gearing is from 100 to 132 turns of the handle to one revolution of the wheel. The mount can be moved at the rate of from 3 to 5 feet per minute. With the mounts having rolling recoil, the length of recoil is considerably greater and a gasoline-driven winch, mounted on the front truck or span bolster and taking up a cable fastened to the track ahead, is preferred for returning the mount to its firing position. For this sort of movement, experience has shown that the rolling friction is much greater than is ordinarily assumed for railway work. The tractive effort on a level track with the American 16-inch howitzer ran up to 50 pounds per ton. On the heaviest sliding mounts electrical translating mechanism is provided. This is very convenient, of course, but requires a power plant and complicates the design and accessory equipment. Manpower is always available and is reliable. Electrical equipment has the bad habit of failing when it is needed most.

- 413. ELEVATING MECHANISM.—Elevating mechanisms are so diverse in type, and the speed of operation of the piece is so largely dependent on them that a somewhat lengthy consideration is felt to be justified. First the requirements of the mechanism will be discussed, and then their practical embodiment will be described.
- 414. The requirements of an elevating mechanism are that it shall:
 - (a) Afford proper extent of elevation.
 - (b) Give proper ratio of handwheel to gun movement.
 - (c) Be sufficiently strong to withstand shocks of fire.
 - (d) Be efficient enough to allow operation at the required speed with the power available.
 - (e) Be simple in construction and easily maintained.
- 415. In regard to extent of elevation, (a) above, ideas have been modified considerably by the experience of the European War. howitzers, a maximum elevation of 65 degrees is required to give the desired plunging fire. For guns there may be objectives at long ranges of such size that the high dispersion incident to fire at maximum range is not disadvantageous. Therefore the mount should always allow sufficient elevation for the gun to attain this maximum range. For medium caliber guns at medium velocities, this approximates the theoretical 45 degrees. For large guns and high muzzle velocities, however, the decreased air resistance at high altitudes so far increases the range that the maximum appears to be attained at from 50 to 55 degrees. The long range 210-millimeter German gun which operated at a muzzle velocity of 1,500-1,600 meters per second, was fired at an angle of at least 55 degrees. The French 220-millimeter gun will be mounted with provision for an elevation of 55 degrees.

- 416. The ratio of handwheel to gun movement, (b) above, will be expressed as the gun movement in degrees over the corresponding handwheel movement in turns, 2/1 meaning 2 degrees of gun movement per revolution of handwheel. This ratio should be such that the necessary fine adjustment for laying can be had, on the one hand, and that the gun may be depressed and elevated rapidly for loading. On some of the older mounts, the ideal for both requirements is sought by the use of a slow elevating gear and a quick loading mechanism together, as on the 190, 200, and 240 millimeter French howitzers. Railway artillery, however, is not called upon for extreme speed in firing, and late designs of mounts show that a satisfactory compromise can be found in a single mechanism. an indication of the requirements for accurate laying, it is found that the adjustment of elevation to a precision corresponding to one quarter of the probable error in range, requires setting to within from 1 to 2.5 minutes, depending upon the accuracy of the particular gun considered. Such a setting could easily be made with a handwheel ratio of 1/1 to 2/1. The smaller handwheels can be spun at from 60 to 90 revolutions per minute, which would give a speed of operation to 45 degrees elevation, of from 15 to 45 seconds. is amply fast enough for railway artillery. Practice shows a variation of this value per turn of handwheel between about 0.33/1 and 1.80/1. The ratio for the heaviest guns approximate a value of 0.5/1, but as one of them which has an efficient elevating gear, has a value of 1/1, it is thought the lower value is adopted for the sake of mechanical advantage, rather than because it is inherently desirable. The conclusion from the above is that a ratio of 1/1 (1 degree movement of gun per revolution of handwheel) is amply fine enough and that the value may be run up to 2/1 with the less accurate and smaller guns.
- 417. In reference to strength (c) above, the chief forces to be withstood are two. The first is a turning moment due to the powder pressure. In American ordnance design, the center of gravity of the recoiling parts is usually put a short distance below the center line of the gun, so that, as long as the projectile is in the bore, there is a couple due to the powder pressure against the breech, which tends to elevate the gun. The elevating mechanism must be made strong enough to stand this without movement, so that the accuracy of fire will not be reduced. The second force is the moment due to the breech preponderance of the gun when in full recoil. If the elevating mechanism is so constructed that it can not be moved by this couple, then it must be made strong enough to withstand this moment as well, which is usually considerably larger than the one first mentioned. On most heavy mounts (tipping parts weighing over 25,000 kilo-

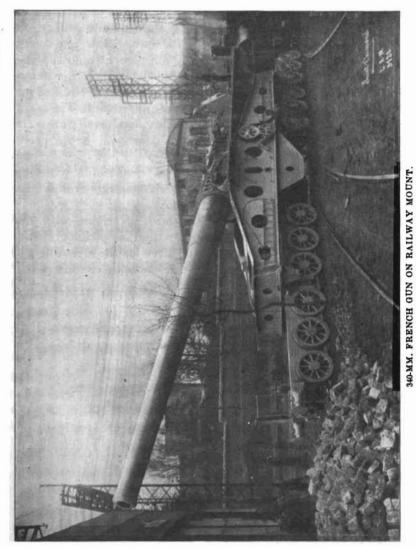
grams) the elevating mechanism is arranged so that it can slip slightly under the action of this couple, the slip-friction device being inserted ahead of any worm or screw which, of course, are irreversible. The movement takes place only after the projectile has left the bore and does not affect the accuracy of fire. Even in these cases, the gearing seems to be made strong enough to stand this moment, with a safety factor of perhaps two. On the sliding mounts, with fixed trunnions, neither of the above stresses occur, but if the center of gravity of the gun is not exactly coincident with the axis of the trunnions, a turning moment develops as the mount recoils. A turning moment is developed in a similar way with a rolling mount where the trunnions are very likely to be behind the center of gravity, as on the British 14-inch mount.

418. Under the above analysis the turning moment to be resisted is calculated or assumed. With the heavier guns the moment becomes more and more difficult to provide for. Ordinarily, one tooth of a pinion must take it. Next, a second pinion with another rack may be added. After these, plain worms, Hindley worms, and screws, give possibilities of progressively increasing strength within the practicable limits of the mechanism.

419. The efficiency (d) above, required of the gear, depends upon the work to be done in elevating the gun and the power available. The work is, in general, that of overcoming the friction of the trunnions in their bearings. With the small guns of light weight and supported by trunnions of small radius this is comparatively insignificant, but with heavy guns and large diameter trunnions, particularly with the sliding mounts, where particularly large trunnions are required, this friction may be considerable. When the work of overcoming this becomes too large, recourse is had to various antifriction devices, which support the gun during elevation but give under the shock of fire and allow the main trunnions to take that shock. These devices operate either by reducing the coefficient of friction, as with the roller bearings, or by reducing the relative movement, i. e., using a very small radius auxiliary trunnion (St. Chamond type). Some devices combine these two ideas, and the arrangement on the 280-millimeter German mount, plate 388, is perhaps the best which has been seen. In practice these devices seem to be adopted almost universally for mounts with tipping weights exceeding 25,000 kilograms. The second factor concerned, as noted above, is the power available. This is preferably hand power and may be approximated as varying from one-tenth horsepower, for a man spinning a handwheel for a short time, to perhaps 1 horsepower for four men working at top speed on long radius cranks. Some French mounts have 71 horsepower electric motors for elevating and the British 14inch has a 20-30 horsepower gasoline engine. For the sake of simplicity of construction, operation, and maintenance, it is highly desirable that hand power be used where possible, and it is believed that, if efficient gear trains and good antifriction devices are employed, this is possible even with the heaviest gun; and even where power elevating is used, the hand mechanism should always be provided as an auxiliary.

420. The required efficiency of the gear train can be approximated from the preceding considerations. Manifestly, it is a function of the number and character of the mechanical elements in the train. These are, usually, spur gears, bevel gears, chains, worms, and screws, with efficiencies falling off in about the order named. Low pitched worms and screws are very inefficient. It is, of course, necessary to make careful calculations on the efficiencies of each individual elevating mechanism but these will always be found to involve two constants which must be assumed, the coefficient of friction in the trunnion bearings and the efficiency of the gear train. The relation of the former divided by the latter is taken as an indication of the efficiency of the mechanism. As an indication of values, data has been taken from proof tests of a number of seacoast carriages, and the efficiency of the mechanisms has been computed. It is found to vary from 0.372 to 2.67 with an average of about 1.14. The gear trains of all these mounts included a worm or a screw and from one to four pairs of bevel or spur gears. Assuming 0.15 for the coefficient of friction. this would indicate a gear train efficiency of from 40 down to about 6 per cent. By contrast, the American 16-inch howitzer with a train of three pairs of spur gears, gives a value of approximately 0.15; that is, a gear train efficiency of about 60 per cent, with a coefficient of friction of about 0.10. This indicates clearly the superiority of spur gears from the standpoint of efficiency. Since the gun of this mount, the tipping parts of which are at least half as heavy as those of the largest gun to be considered, can be elevated in 25 seconds by one man with one hand, it is felt that spur gears give a sufficiently efficient train so that even the largest gun could be operated through them by hand power. The best example of this construction is the St. Chamond 340-millimeter gun mount, plate 427, with a gear ratio of approximately 1/1 and on which the elevating gear is apparently entirely satisfactory.

421. In the matter of simplicity, (e) above, manufacture is probably simplest on chains and spur gears, and becomes progressively more difficult on bevels, screws, worms, and Hindley worms. As to maintenance, the difficulties involved are confined largely to the necessity for close adjustment. Within limits, practically all that is required of the chain drive is that the two sprockets be in approximately the



same plane. With spur gears, the distance between shaft centers must also be fairly closely maintained. With bevel gears the shaft center lines and planes of the gears must both be exactly maintained. With worms, the shaft distances and the plane of the worm shaft must similarly be kept just right, and with Hindley worms, the position of the worm along its shaft must be exact as well. With the screw, screw and nut must be coaxial, but if they mesh at all, this condition is assured. This indicates that screws, chains, and spur gears are the easiest mechanisms to keep in adjustment, and that bevels, worms, and Hindley worms are more difficult in the order named.

422. The way in which these five requirements are realized may be understood by a study of the various mounts described in section 3, Volumes I and II. The following summary, extracted from section 3, is given, covering some of the points discussed in the preceding paragraphs:

Use of slip-friction device: Almost invariable with mounts whose tipping parts weigh over 25,000 kilograms. Exceptions have screw elevating gear.

Use of antifriction device: Almost invariable with mounts whose tipping parts weigh more than 25,000 kilograms. The single exception has a power drive for the elevating gear.

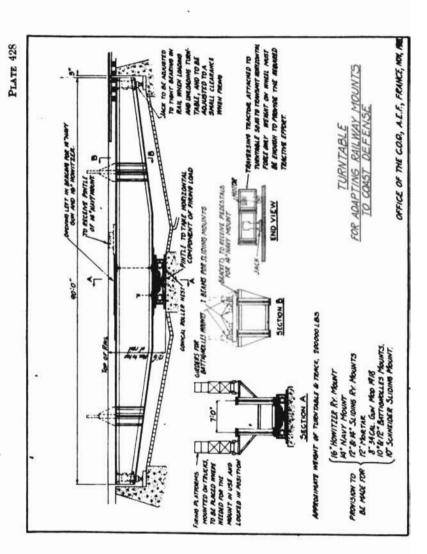
Mechanism at the gun: Forty-one examples classify as follows:

Curved rack and pinion	29
Straight rack and pinion	
Worm and wheel	3
Screw and nut	8
Gear train, exclusive of above:	41
Spur gears only	5
Bevel gears only	6
Spurs and bevels	2
Worm and bevel	17
Chains employed	4
General type of entire mechanism:	
Rack and spur gears	5 19

The only types of mechanism which occur with almost or identically the same arrangement of components, on a number of mounts, are the rack with spur-gear train, which is found only in American and French designs, and the rack, pinion, worm, wormwheel, and bevel combination, which is very popular and occurs in American, French, British, and German designs. The chief objection to this latter type of gear is low efficiency, which has necessitated a low ratio of gun to handwheel movement—from 0.33/1 to 0.67/1.

- 423. The conclusions with regard to elevating mechanism are:
 - (a) Extent of elevation: To 45-55 degrees for guns; 65 degrees for howitzers.
 - (b) Ratio of handwheel to gun movement: One to 2 degrees of gun movement per turn of handwheel.
 - (c) Strength: Usually safeguarded by a slip-friction device.

 In exceptional cases great strength may be obtained by the use of a screw.
 - (d) Efficiency: Spur gears most efficient. Screws and worms may reduce efficiency to very low values.
 - (e) Simplicity: Spur gears, chains, and screws are simplest mechanisms. Bevels and worms to be avoided when possible.
- 424. Traversing Mechanism.—Traversing mechanisms are discussed in a general way in section 1. A detailed discussion of the mechanical features of the different schemes follows.
 - 425. Nontraversing mounts must be pointed in azimuth by some extraneous means, as a curved epi or a turntable. These mounts are usually of the rolling or sliding recoil type and have some sort of translating device to bring them back again into firing position. See description of recoil mechanisms above. This same mechanism can be used, of course, to move the gun along the epi for training in azimuth. In the case of a turntable a special rotating mechanism, usually motor driven, is, of course, provided in the turntable itself, plate 428.
 - 426. Railway car traverse, as explained in section 1, allows usually only a very limited movement on the trucks, perhaps 4 degrees. Car traverse in connection with an emplacement is best worked out through the use of a center-plate arrangement built into or attached to the car body; it usually includes roller or ball bearings on which a part or all of the weight of the car body is supported. All round fire mounts of the car traversing type, as at present developed (American 14-inch model E, German 380, 280, 240, and 210 millimeter mounts), require elaborate foundations. Car traverse may be superior to top carriage traverse for a wider range of fire than can be obtained from the trucks, with guns which are not so powerful but that a rapidly built emplacement is possible, yet which are so large that top carriage weight is comparable with car body weight. So far as is indicated by present practice, however, this type of traverse is best applicable to high-powered guns requiring only limited traverse in the mount and firing usually from an epi.
 - 427. Top carriage traverse, as noted before, is suited to a maximum traverse of from 10 to 360 degrees. The top carriage consists usually of cast-steel side frames carrying the trunnion bearings in which the



gun cradle swings, and transoms connecting the side frames. It will be more fully discussed later. The components of the traversing gear should be strong enough to resist the forces tending to rotate the carriage when the piece is fired at high elevations. The ratio of the gearing should be such as to allow of fine adjustment—that is, to one mil. Efficiency is not of as much importance here as in the elevating gear, except, perhaps, for coast defense work. As previously pointed out, this type of traverse finds its best application in mounting the less powerful pieces for all round fire, where carriage weight is small in proportion to car body weight.

- 428. A discussion of the relative advantages of these systems of traverse is narrowed down by the following considerations:
 - (a) Top carriage traverse is so simple for howitzers and the smaller guns (8 inches or less) that the other types do not merit consideration.
 - (b) Nontraversing carriages have so little advantage in simplicity over the car traversing type that they need not be considered.

429. The question becomes, therefore, one as to the type of traverse to be adopted for heavy guns—specifically between epi curve-car traverse combination and an emplacement top carriage traverse com-The chief objection to the former is the ease with which the battery may be located by aerial photography; in other words. the difficulty of effective camouflage. The answer to this objection lies chiefly in two considerations; first, that the type of target fired on from an epi is usually such that the gun is placed, delivers the required number of shots, and is then returned from the epi to the base, so that, even though the enemy may know where all the epis are, he is by no means sure just where the gun is, and it may quite easily deliver its fire and retreat before he can be sure of its location and start counter-battery fire. The second consideration is that camouflage has proved ineffective against the various means of detection which have been developed—aerial photography, sound ranging, flash ranging, earth vibration ranging, etc. The Allies found, after the conclusion of the war, that the vast majority of the German batteries had been exactly at the points where these various agents had indicated them to be. In the special cases known where careful and effective camouflaging was worth while, for instance for fire of destruction against the bridges east of Metz, the mounts were in position for a long period, but, on the other hand, they were firing at practically a single target, and needed no epi curve, car traverse being ample for the service. With top carriage traverse, on the other hand, ordinarily either no more traverse is realized than with the other type or a special foundation has to be installed, which, with heavy guns, is a very difficult and time-consuming job.

- 430. The general conclusions with regard to traversing mechanisms are that two types should be considered for services as follows:
- (A) For heaviest cannon (14-inch 50-caliber guns and 16-inch 25-caliber howitzers): Top carriage or car traverse as wide as stability will allow, using outriggers to take most of the horizontal component of the force of recoil. These same mounts should be so designed as to be capable of operation as rolling mounts if desired and be equipped with traversing rollers and a base ring of the 14-inch model E type for service in coast defense.
- (B) For medium-powered cannon (10-inch 50-caliber and 12-inch 25-caliber howitzers): Car traverse with wide angle of fire, plates 59 and 60.
- 431. Gun Carriage.—Most of the components of the gun carriage have already been discussed, but there remain to be mentioned some facts regarding the types and construction of the main frame and the types and construction of pintle and traversing rollers.
- 432. The main frame of the carriage consists normally of two side members which support the trunnion bearings, and connecting transoms and perhaps a racer. In American and early French practice these parts are uniformly steel castings. Later French and English practice, however, is to build these parts up out of structural shapes and plates.
- 433. Such practice appears entirely satisfactory, providing provision is made (by additional clearances, etc.) so that the greater flexibility of the structural, as compared with the cast frames, can not cause trouble.
- 434. Pintle and roller arrangements are of two types. The first, or front pintle type, has a large vertical pin under the front of the carriage, around which the carriage swings. Rollers, usually spring supported, are provided under the rear end of the carriage, and these travel on a special track on the base, or railway car. This type is exemplified, for instance, in the Batismolles mounts and the American 16-inch howitzer. The advantages of such a top carriage are comparatively small forces on the traversing rollers, due to the relatively long lever arm at which they act and great simplicity of construction, facilitating both original manufacture and field maintenance. disadvantage is that the work involved in traversing is large in proportion to the distance between the pintle and rollers, and because of the large radius of the roller path the type can be used on railway mounts for limited traverse only. The second, or center pintle type, is provided with cylindrical pintle (either a pin or a large radius surface) and a complete circle of conical traversing rollers or balls, both concentric with the carriage. The rollers circulate between conical paths on the base ring and racer, and constitute a roller bearing; the balls, varying in diameter from 4 to 8 inches, circulate between two

grooved paths of circular cross section on the base ring and racer. Both rollers and balls take the entire shock of fire directly. The radius of the roller or ball path is made as small as possible to reduce the work of traversing. The advantages of this type are that a minimum traversing force is required and that the apparatus is sufficiently compact to allow all-round fire in the limits of railway clearance. The disadvantages are the heavy loads which must be carried by the traversing rollers, or balls, and the comparative complexity and exactness required in fabrication, especially in the case of the rollers.

435. The conclusion from the above is that the center pintle type would be most usually employed on railway mounts for medium howitzers and light guns, and for heavy guns and howitzers in connection with some type of separate base ring. The other type will be employed for heavy howitzers and medium and light guns when a greater carriage traverse (10 degrees) than can be secured in car traverse (4 degrees) is desired.

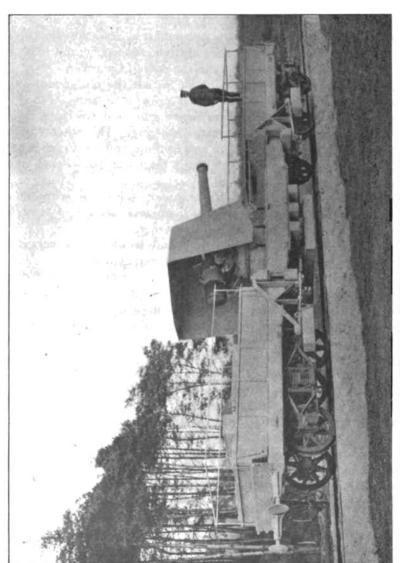
436. RAILWAY CAR BODY.—Railway car bodies are, with the exception of certain improvised French mounts, always of structural steel and are of two types, flat car and girder.

437. The car bodies of the first type may be merely flat cars of the ordinary freight pattern with the carriage mounted on top of them, as in the case of the 155-millimeter howitzer, plate 429, the 240-millimeter gun, plate 237, or the 194-millimeter gun, plate 431. This type is simple, sturdy, and satisfactory for these mounts.

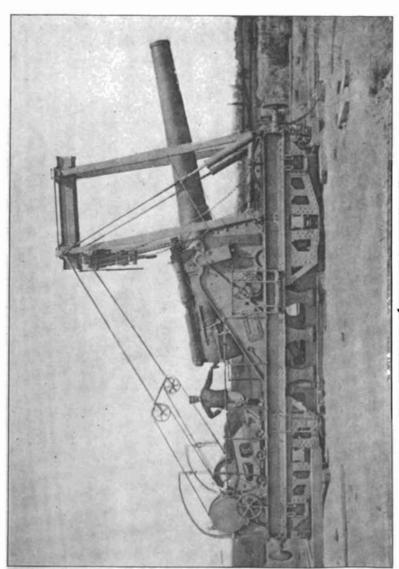
438. In most cases, however, the height of the gun carriage is such that headroom demands a drop frame type of flat car body. This type is illustrated by the 200-millimeter howitzer, plate 10, the British 12-inch howitzer, plate 432, and the American 8-inch gun, plate 88. Experience has shown two defects with this type of flat car body, one the difficulty of making it stiff enough to prevent undue deflection under the load of the gun, thus perhaps causing deflection of the gun carriage base ring and cramping or jamming of the traversing mechanism; and the other is the same as that experienced with commercial drop frame flat cars, viz, their inability to stand under the severe buffing strains to which they are subjected in coupling, and being hauled over the road, with heavy trains.

439. The girder type of car body is employed when the weights become too great to be carried on the ordinary flat type. Practically all of the larger caliber mounts furnish examples of this type. This can, of course, be made as strong and as stiff as occasion demands. Only one point needs to be mentioned, and that is the necessity for rigid cross bracing between the two side girders. The lack of such sufficient bracing results in racking or weaving of the side girders relative to each other and the binding of the gun trunnions in their supports breakage of trunnion caps, and the like. There must be actual contact

PLATE 429

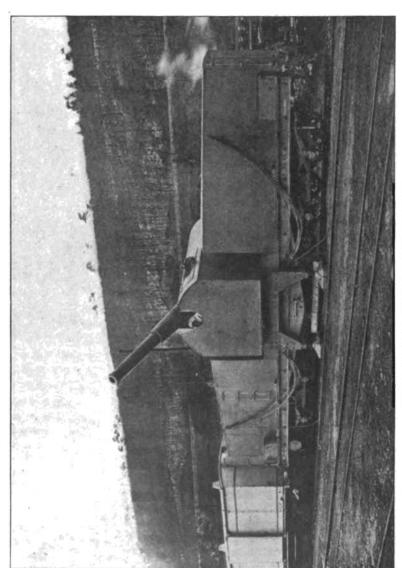


155-MM. HOWITZE'R (FRENCH) ON RAILWAY MOUNT.



240-MM. FRENCH HOWTTZER ON RAILWAY MOUNT.

PLATE 431



194-MM. FRENCH GUN ON RAILWAY MOUNT.

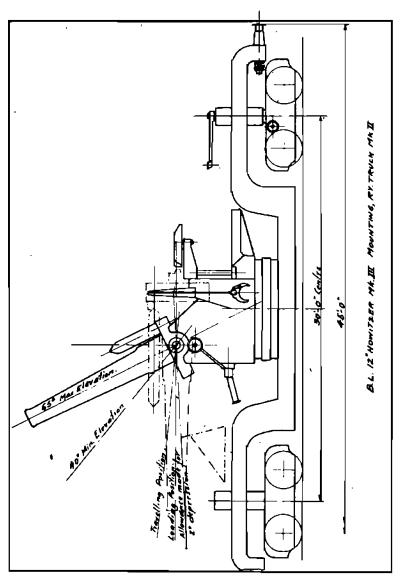


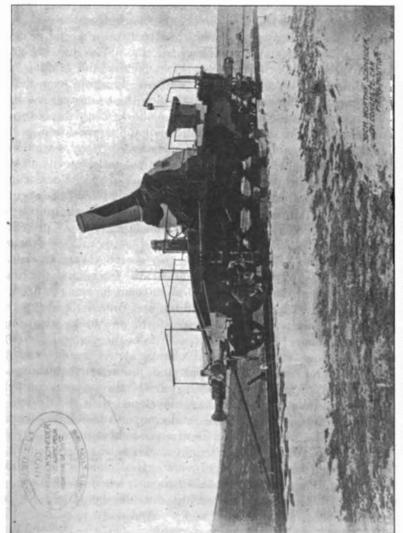
PLATE 482

between the webs of the transoms and the webs of the side girders to produce the desired rigidity. The rivets can not be depended upon.

- 440. An experimental car body of reinforced concrete, plate 433, for a 30-centimeter mortar has been made in France. In spite of the fact that it was successful, this type of construction is not thought to merit consideration where steel is available.
- 441. Anchorage.—The discussion under section 1 brought out most of the points regarding the existing types of anchorage. They may be summarized as follows:
 - (a) Mounts requiring no preparation: Must be of the rolling recoil type, can have but very limited traverse, and are in general best suited to the very heavy guns.
 - (b) Mounts requiring a track platform: Sliding type, suited for heavy guns with limited fire. Strut type, suitable for light and medium guns with 60 to 360 degrees traverse.
 - (c) Mounts requiring a ground platform: Suited for medium guns with all-round fire, and for heaviest guns with limited fire. (All-round fire for heavy guns in exceptional cases.)

Something remains to be said regarding mechanical details and relative desirability of the different designs under the various types.

- 442. The first type is, of course, ideal from the standpoint of anchorage. The chief objection, however, is that in all types heretofore constructed it has been necessary to include a recoil system to reduce the maximum pressure on the trucks, and a counterbalancing system to compensate for the extreme muzzle preponderance resulting from mounting the trunnions close to the breech to secure great elevation. Further, the length of recoil along the track (30 to 50 feet) is too great. Improvements now being experimented with on sliding mounts, and detailed in paragraph below, suggest that some means might be adopted to transmit the force directly to the rail instead of through the truck springs. If the car girder were sufficiently strong to distribute the pressure along the track for the length of the mount, pressure on the ties would be nearly as low as on the sleepers of the present sliding mounts, and the pressure on the ground would be halved. If this arrangement did not require too great a weight of girder or too great a complication of jacks it would seem to constitute a most excellent system for guns requiring only very limited traverse.
- 443. The sliding type of track platform mount requires an epi built with special, long, closely spaced ties, and laid with I-beams in addition to the regular rails. The mount is distinctly at a disadvantage, as compared with the rolling type of mount, in that standard track can ordinarily not be utilized and, indeed, no standard



300-MM. FRENCH MORTAR ON REINFORCED CONCRETE RAILWAY MOUNT.

track materials, except rails, can be used to advantage in the special construction required. A modification of the sliding type mount is now being experimented with, in which the I-beams, or bearing stringers, are fastened to the mount and slide along the top of the ties instead of having them fastened to the top of the ties and allowing the mount to slide over them. This involves the use of dressed ties of extra length in laying the epi, but on the other hand. it avoids the use of a large amount of structural material in making the epi and saves time in its construction. The proving ground tests show that this construction is satisfactory and it offers a distinct improvement over the previous types. It would seem that this scheme might be developed by lengthening the beams carried by the mount, so that enough ties to take the shock would be covered on standard track. With such a modification and the addition, perhaps. of a set of cutters on the mount for surfacing the ties, it would seem that this type might be adapted to operate as satisfactorily on standard track as the former type operates on a spur of special construction. This would have the same advantage as the modified type suggested above, but would, like it, be limited to heavy guns requiring only limited traverse. The sliding type of anchorage, as at present developed, however, still possesses considerable advantages over other types of platform. While it requires the construction of an elaborate epi, this can be built while the mount is still far behind the lines in safety, and when it is finished the mount can be run up, fired, and gotten out again in an absolute minimum of time.

444. The other types of track platform anchorage also employ stringers of beams laid over the ties, to take the vertical component of fire, but they employ guys, rail clamps, struts, spades, and floats to take the horizontal component and prevent overturning. difficulty is experienced with taking care of the vertical component of fire, but serious limitations have developed with the devices employed to take care of the horizontal component and the overturning tendency. This limitation is of course most marked in an allround fire carriage operating at right angles to the track, and it will be discussed from that point of view. Rail clamps alone sufficed on the early 155-millimeter howitzer mount, when used on standard gauge track. Horizontal floats, just outside the rails, with jacks attached to the side of the car and screwed down on them, sufficed for the 164.7 and 194 millimeter guns. On the 200 millimeter howitzer it was necessary to place these horizontal floats further out and mount the jacks on the end of swinging arms. This same scheme was tried and found inadequate for the American 6-inch seacoast gun. With the addition of a vertical spade to the float it was tried

on the British 9.2-inch mount and cables attached to deadmen had to be used as a supplement. The next step is the use of struts, with floats arranged at their ends perpendicular to them and bearing against a prepared and properly sloped surface on the ground. This is employed on the American 8-inch gun and 12-inch mortar mounts and the St. Chamond 240-millimeter mount. These seem to mark almost the upper limit of the possibilities of track platform anchorage for all round fire. It is felt that the American 8-inch scheme is a better design than the St. Chamond. It is more effective and can be put in place in one third of the time.

445. Ground platforms, requiring removal of the track and the placng of special work under it, are of two distinct types—the steel or concrete emplacement type and the wooden float and strut type. The former is exemplified in the Batignolles platform, plate 54, for limited traverse carriages, and in the 280-millimeter German platform of steel or concrete, plates 55 and 66, and American 14-inch model E, steel platform, plate 239, for all-round fire. Under this head come also the turntable emplacements used with the German 380-millimeter, plates 417 to 422, and suggested for United States coast defenses, plate 428. The latter type noted above, i. e., wooden float and strut, is merely an extension of the track platform and strut type of mount. It is illustrated by the St. Chamond mounts, plates 51 and 52, and the American Navy 14-inch mount M. I, plate 23. This type allows only of limited traverse. Relative speed and simplicity of installation give a decided advantage to the Batignolles type of ground platform for limited traverse carriages, but the manufacture is, of course, relatively costly and elaborate.

446. A general study of the various types of platforms shows that the permissible load figured on is approximately two tons per square foot, or 20,000 kilograms per square meter. General Peigne's early researches led him to recommend a pressure just half this, i. e., 10,000 kilograms per square meter, and it is undoubtedly true that for horizontal thrusts near the surface of the ground, as in the track platform and strut type of mount, the use of a figure less than 20,000 kilograms is advisable. For vertical stresses or in case of floats deeply buried, the figure is probably perfectly good.

447. TRUCKS.—The trucks used for railway mounts do not differ from those required for other types of heavy railroad work and no detailed discussion of merit need be entered into. It may be said, in brief, that the outside type of journal should be used if at all possible, for the sake of simplicity, and that both hand and air brakes should be provided. It should also be added that a number of peculiarities which will be noticed on French trucks—such as lack of

equalizers, mounting the centerpin off center of trucks, etc., are improvisations, and are not to be considered desirable for this type of service.

448. Axle loads, during the present war, have been limited by French railways to 17 metric tons. The American Navy 14-inch mount, which exceeded this by about 35 per cent, gave a great deal of trouble, especially from the overheating and scoring of journals and hearing brasses. Mounts with rolling recoil take the firing load directly through the trucks, and this force must be reckoned with in the design. This force is about 35 long tons on English mounts and 27 long tons on the American 16-inch howitzer.

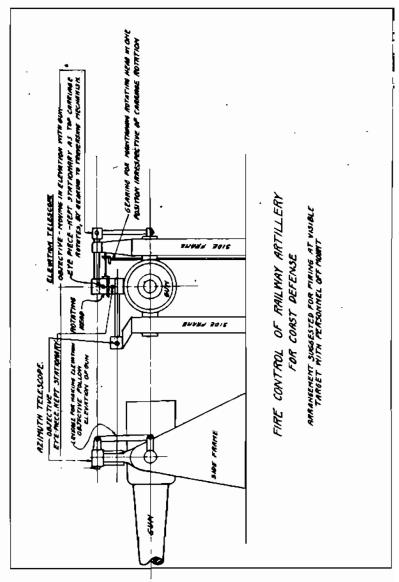
- 449. Ammunition Supply System.—The ammunition supply system consists of two essential parts, as a rule, a hoisting and translating mechanism for bringing the shell near the gun and a tray or truck for guiding it into the breech. The hoisting and translating mechanism is usually a Triplex block suspended either from a jib crane or an overhead trolley. The jib crane appears to be the favorite for small calibers, and for large calibers where the gun has a fair amount of traverse. The overhead trolley, however, is used in most of the heavy mounts where there is very little traverse, and where the shells can be taken directly out of the ammunition car, or off the transbordeur.
- 450. The guiding mechanism is a tray onto which the shell is lowered, and which extends into the breech of the gun. On some mounts, as the American 8-inch gun, this is very small and is carried by a second jib crane. Usually, however, a part of it constitutes the top of a stationary shell stand, while another portion can be pushed into the breech when the latter is opened. The shell is then slid along it into the gun, plate 161. Another type consists of a tray provided with wheels, which rolls along a track and part way into the breech of the gun. The tray then brings up against a buffer. while the shell continues to move of its own inertia and comes up to a full or partial seating against the forcing cone. Here the same line of demarkation occurs as in the lifting mechanisms—the plain tray appears to be the favorite for all light shells, and for heavy mounts with considerable traverse. In many cases a negative loading angle is given to assist in moving the shell into the gun. The rolling tray or shot truck is more used with the heavier calibers and mounts having small traverse, plate 162.
- 451. It is felt that the above indicates the best use of the various arrangements discussed, i. e., the crane and tray arrangement for practically all small guus and the overhead or trolley cranes and shot truck arrangement for heavier caliber guns having very small traverse.
- 452. Special Arrangements for Coast Defense. -- As noted at the end of section 2, the use of railway mounts for coast defense calls

for special characteristics not demanded in land service, viz., provision for operating the sighting, elevating, and traversing mechanisms up to the moment the piece is fired, so that a moving target can be followed and also for operating them simultaneously for the entire battery for volley firing. It is proposed here to discuss the merits of the several possible arrangements for accomplishing this end.

453. The difficulty encountered in the evident solution of leaving men on the mount to carry on these operations is that, in rolling and sliding mounts, and quite probably in all mounts with any but the heaviest anchorage, the shock of fire is so great that this has never been felt to be safe.

- 454. For the purposes of this discussion, mounts may be divided into three classes:
 - (a) Heavy mounts with top carriage traverse and operating fixed to the anchorage.
 - (b) Light mounts with top carriage traverse and operating fixed to the anchorage.
 - (c) Sliding and rolling mounts traversing by movement along curved epis.
- 455. With heavy mounts fixed to an anchorage, it is felt that the evident solution mentioned above, of leaving the personnel on the mount, is feasible. This same condition may be realized with heavy guns with small traverse, by mounting them on a turntable, plate 428, which would be electrically operated. The latter arrangement has the disadvantage that turntables must be provided wherever firing is to take place, and the former would seem to be feasible only when an elaborate anchorage is employed. With either of these arrangements, however, the guns can be controlled and fired just as if they were installed in a fort in the ordinary way.
- 456. With light mounts fixed to an anchorage, the vibration of the structure from the shock of fire would probably be too great to permit the personnel to remain upon it. Three arrangements suggest themselves as possible solutions for this case.
 - (a) Remote control of elevating and traversing mechanism either mechanical or electrical, and observation of azimuth circle and elevation indicator through telescopes. In this case the azimuth circle should be rotatable, so that correction of zero could be made after each shot. For the case where the target is observed directly prism telescopes would have to be employed and arranged as shown in the sketch, plate 434, so that their eyepieces, rotatable around the center of carriage rotation, would be so connected with the traversing mechanism as always to point in the same direction.



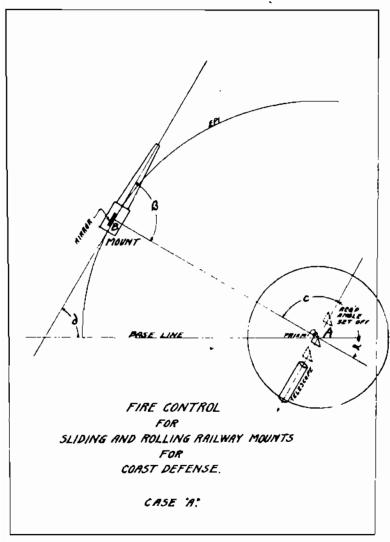


- (b) Provision of a simple recoil mechanism on all seats occupied by personnel during firing. The shock and vibration in these mounts is very sudden but not of great amplitude, so that this cushioning mechanism would be very simple. It would, of course, be essential that all optical instruments be arranged so that the eyepicce recoiled away from the observer.
- (c) Provision of concrete foundations to which the car can be firmly fixed. This is the Luellen idea and would, of course, be equivalent to a gun mounted on a permanent emplacement.
- 457. The first scheme (a) above is quite feasible but somewhat complicated, the third has the disadvantage that fire can only take place at prearranged points, and the second seems best if it can be worked out satisfactorily.
- 458. With sliding or rolling mounts operating on curved epis, two alternatives are possible:
 - (A) The pointer may be located on the ground, with remote control arrangements for elevation and traverse.
 - (B) The pointer may be located on the mount and his seat provided with a long recoil mechanism, such that the shock of fire will not injure him.

In either case somewhat elaborate apparatus for laying the piece is required. The aiming point may be located at the center of the epi or at some other point. In order to show what may be done, the following four cases will be discussed.

- (a) Pointer on ground, reference point at center of epi.
- (b) Pointer on ground, reference point anywhere.
 - (c) Pointer on mount, reference point at center of epi.
 - (d) Pointer on mount, reference point anywhere.
- 459. Case (A) is illustrated in plate 435A. A mirror is so fixed on the mount that its plane is always parallel to the vertical plane through the center line of the gun. (If the mirror is tilted up to raise the line of sight, so that it moves in a cone instead of a plane, the following reasoning still holds. This may be necessary with a group of mounts controlled from a tower.) At the center of the epi the pointer is located on a platform rotatable about that center. He looks through a telescope A, whose angle δ with the baseline can be varied by rotating the platform and can be read on an azimuth circle. His line of sight is turned at right angles by means of the prism P, which can be moved back and forth for a distance of perhaps 10 inches each side of the center along the line of sight of the telescope. The operation of training then is as follows: The telescope and rotatable platform are set, either by an assistant from telephone instructions or automatically through mechanical

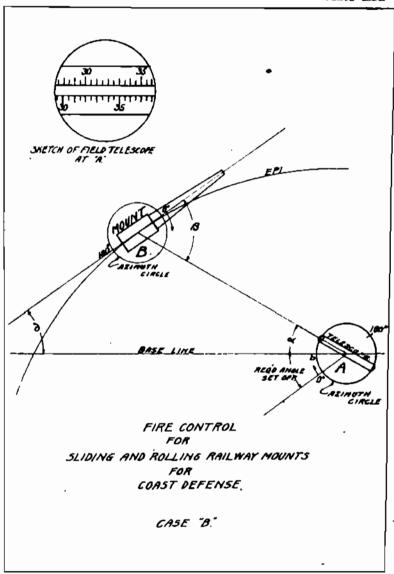
PLATE 435A



or electrical synchronizing from a central observation point, so that the angle α equals the required deflection of the gun from the base line. The pointer sets his prism directly over the center of the platform (in mid-position), and by operating the controllers of the electric translating motors on the mount he brings it up until he sees the reflection of the prism (or a pointer arranged on it) in the mirror of the mount and registering with the vertical cross hair of his telescope. This would mean that both angles B and C are right angles, and therefore that angle δ equals angle α the required deflection.

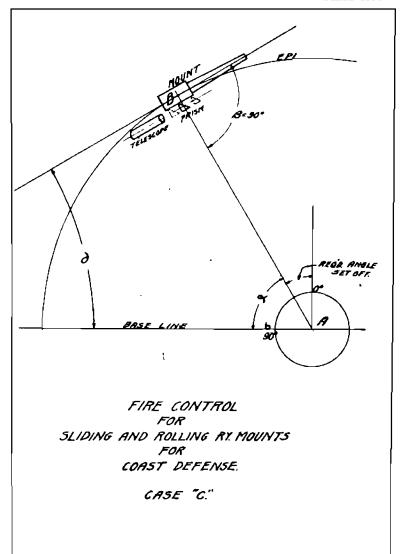
- 460. Due to the irregularities of the track and the following of the mount upon it, the line AB may not always pass exactly through the center point. In such cases the prism may be slid back and forth until this line passes through it.
- 461. This scheme may be greatly simplified if the observer of the targets is placed in a tower just above A, and arrangements are made so that his telescope and the telescope and platform shown here rotate together. The services of the man setting the azimuth circle at A would then be unnecessary. In actual practice, however, it will likely be found more desirable to place the observer's tower on high ground at some distance from the center of the epi, which will be in low positions not visible from the sea.
- 462. Case (B) is illustrated on plate 435B. A horizontal azimuth circle and a rod marking its vertical center line are mounted on the gun, so that the rod and the zero of the circle are both in the vertical plane through the axis of the gun. At any point whatever, as A, the pointer is located on a rotable platform with a telescope. Attached to this telescope, and so arranged that it occupies half of the field of view of the latter, is an independently rotable azimuth circle, which can be read against the cross hair through the telescope, and also against the base line at b. The operation of training is then as follows: The circle Λ is rotated either by an assistant from telephoned instructions, from the observation tower, or automatically through mechanical or electrical sychronizing, from a central observation point. The pointer keeps his telescope trained on the central rod of the azimuth circle on the mount. He then traverses the mount. through remote electrical control, until the reading of the azimuth circle on the mount against the telescope cross hair is the same as the reading of the azimuth circle at A against the same cross hair. Each of these circles occupies half of the field of the telescope, so that his task is simple to bring like graduations opposite. Now, if the circle at A is always kept with the required angle reading at b, then the reading on the circle by the telescope will be required angle $+ \alpha$. If B is made equal to this, then by constructing δ will equal the required angle.

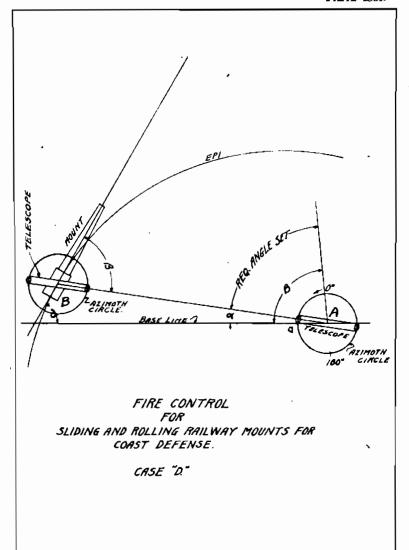
PLATE 435B



- 463. Case (C) is illustrated on plate 435C. A telescope with a movable prism, similar to that described under case (A), is mounted on the mount so that it is always parallel to the vertical plane through the gun center line. At A, the center of the epi, a rod and azimuth circle are mounted. The 90-degree graduation of the azimuth circle is placed at b on the base line with the graduations decreasing in a clockwise direction. The operation of training is then as follows: The pointer is given the required angle by telephone, or an index on the azimuth circle is moved to it, by an assistant or by automatic mechanical or electrical synchronizing arrangements from a central observation point. The pointer, looking through his telescope, moves his prism to bring the central rod of the azimuth circle on the vertical cross hair. He then traverses the mount until his cross hair intersects the desired graduation or the index on the azimuth circle. The required angle, as set off, is that between AC and AB. This is evidently equal to angle 5 by geometry.
- 464. Case (D) is illustrated on plate 435D. On the mount are located an azimuth circle and rod, similar to that described for case (B), and a telescope, rotable about the vertical axis of this circle. At any point, A, there is located another telescope and azimuth circle. similar to that used at A_i in case (B), except that it reads the graduation on its own azimuth circle corresponding to the intersection with base line, as a b, rather than that corresponding with intersection with telescope line of sight, as in the previous case. This azimuth circle is rotable independently of the telescope and its graduations rise in a counterclockwise direction: The operation is then as follows: An index is set on the graduation of the azimuth circle A at the graduation corresponding to the desired deflection from the base line. This may be done automatically as before, or the deflection may be telephoned to the pointer instead. The assistant at the A telescope trains this instrument on the rod on the mount and gets the reading on the azimuth circle B. He then turns the azimuth circle A until this same reading appears at a. The pointer at B trains his telescope on the azimuth circle A and translates his mount till his cross hair intersects the index or the required angular graduation on azimuth circle A. From the geometrical construction it is seen that δ equals $B-\alpha$ or the required angle of deflection.
- 465. Of these various schemes, it is felt that (C) is probably the best and (D) the most complicated in operation. (C) would allow mounting a battery of guns on concentric epis and training them from a single point, which might be in the base of a high observation tower, and which would lend itself admirably to the arrangement for mechanical synchronizing of indices, as suggested. This would be accomplished by having these indices rotated by the same vertical

PLATE 485C





shaft which carried the observation telescope through which the target was being followed. Plate 436 gives a rough sketch of such a scheme.

466. Discussion.—The various design details just discussed are so closely interrelated that it is seldom possible to realize an advantage in respect to one of them without a corresponding sacrifice in respect to another. The following tabulation is given of examples drawn from practice to illustrate this interrelation:

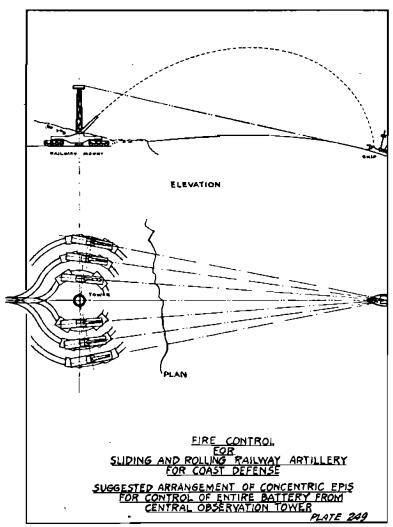
Point gained.	Point sacrificed.	Example.					
Cradle recoil (easy anchorage;	Simplicity and rapidity of manu-	St. Chamond and Batignolles					
rapid fire).	facture: small maintenance.	mounts.					
Eliding recoil (simple construction, little maintenance).	Rapid construction of emplace- ment; rapid fire. (Small runs.)	Schneider mounts.					
Rolling recoil (no anchorage)	Same as cradle recoil; rapid fire; minimum number axles.	Armstrong 12 and 14 inch and 14 and 16 inch American mounts.					
High elevation (long range)	Balanced gun; gun without counterweight or counterbal-	Armstrong 14-inch, American 12 and 14 inch.					
Rapid elevation (rapid fire)	Simple trunnions; easy operation. Compactness of gear; self-locking gear.	St. Chamond 400-millimeter. St. Chamond 400-millimeter.					
Nontraversing (simple construc-	Rapid construction of emplace, ment; accuracy of laying.	Sebneider mounts.					
Car traversing (accuracy of laying).		Armstrong 14-Inch; German 280- millimeter.					
Top-carriage traverse (accuracy of laying; ability to shift targets).	Simple construction	American 8-inch mount.					
No anchorage (rapid emplace-	Rapid fire; simple construction	American 16-inch.					
Track platform (fairly rapid em- placement; all round fire; rapid, fire).	Utmost rapidity of emplacement; simple construction of mount.	American 8-inch.					
Ground platform (wide traverse on heavy guns; rapid fire).	Rapidity of emplacement; simple construction of mount.	St. Chamond 400-millimeter.					

467. For every class of service, therefore, those characteristics must be chosen which possess the maximum number of points advantageous for the particular service and the minimum number of points which are disadvantageous.

SERVICE REQUIRED OF RAILWAY ARTILLERY.

- 468. Guns.—In a broad way, the service required of railway artillery may be defined in terms of caliber and range. Referring to plate 58 and the discussion of it at the end of section 2, it appears that the field here discussed lies between calibers of 200 and 500 millimeters and ranges of 10 to 50 kilometers. A single type of gun, of the largest caliber and longest range required would, of course, cover the entire field, but this would manifestly be uneconomical. The subdivisions which should be made in range and in caliber will be considered in the next section.
- 469. Subdivision by Range.—As noted above, the range to be covered by railway guns extends from 10 to 50 kilometers. The distances at which the guns will be located behind the lines will vary

PLATE 436



greatly; approximates from practice are given in the table below. The question to be investigated is how many different caliber lengths of guns should be provided for each caliber. The theoretical points covering this will first be brought out and they will then be compared with experience.

470. The ideal aimed at in this subdivision is, of course, to hit each of the individual targets which may be presented at any point in the field above, with a minimum average cost per shot. At a given caliber the cost of charge does not vary greatly with the range. The cost of gun wear varies enormously and it is this factor alone which will be considered.

Characteristics of heavy and railway artillery.

	Type of carriage.	Trav- erse desired.	Aver- age dist- ance behind front lines.	Maxi- mum range.	Effective range behind enemy lines.	Walght projec- tile.	Weight explo- sive charge.	rounds
BOWITZER. 8-inch British Mk. 8. 9.2-inch Mk. 2 240-um. 12-inch, 20-cal 16-inch, 18-cal.	do R. R.	360 360	#sn. 4 4 4 10 10	<i>Km</i> . 10 12 15 20 20	#m. 6 8 11 10 10	Lbs. 200 290 856 700 1,600	1.bs. 29 34 49 109 235	6,500 8,700 2,800 1,000 550
00N. 155 G. P. F. 194 G. P. F. 10-inch, 50-cal 14-inch, 50-cal	R. R	360 380 60 5	5 5 10 10	17 25 35 45	12 20 25 35	95 176 510 1, 200	22 32 65 181	4,500 2,900 620 360

471. Consideration of a large number of actual cases shows that the cost per shot for gun wear varies with the maximum range at which the gun can shoot. These cases as well as theoretical calculations show that the variation in cost per shot is directly as about the cube of the range. On the basis of the above it can be shown that two guns, one having 100 per cent and the other from 70 to 80 per cent of the maximum required range, constitute probably the most advantageous subdivision to cover the above field. A study of the caliber length of the entire existing line of the United States Army cannon indicates a decided grouping around average caliber lengths of 12, 32, and 50. This corresponds approximately to ranges of 100, 75, and 45 per cent. This may be taken as a rough check on the above, because the variation in range covered by these guns is greater than that in question here.

472. SUBDIVISION BY CALIBERS.—As noted before, calibers of pieces are determined by resistance of targets; but there are targets

of two kinds as regards resistance, and these require separate consideration. They are:

- (a) Targets which require only a certain amount of explosive to destroy them; i. e., which may be demolished by a few large or many small shells.
- (b) Targets requiring at least a given caliber shell on which a larger caliber represents a waste and a smaller is ineffective.
- 473. A detailed investigation of the ranges, weights, and rounds life of existing guns indicates that for targets of type (a) the cost in gun wear of placing a given weight of projectiles is nearly independent of caliber for ranges above 20 kilometers. (Details of these calculations are given in Appendix II; in such cases hence, subdivision of calibers is of relatively small importance.) For ranges of 20 kilometers or less it becomes progressively more economical to use the smallest possible caliber, sending over the required larger number of shells to accomplish the demolition.
- 474. For targets of type (b) the above investigation indicates that the cost per shot in gun wear varies as about the caliber cubed, and the laws governing the most advantageous subdivision would be similar to those deduced in the case of range.
- 475. In land warfare it may be said that the targets of type (a) occur at ranges (over 20 kilometers total or more than 10 kilometers behind the lines) and under circumstances for which guns are employed (interdiction, long-range destruction of buildings, railroad yards, store yards, etc.); while targets of type (b) (fortified works, troop shelters, etc.) are generally fairly close and often demand a plunging fire, thus requiring Howitzers. Hence it may be concluded that:
 - (a) Great subdivision as to calibers is not called for theoretically for guns. Here such subdivision would probably be decided wholly on the basis of other considerations, such as strength of given types of mounts, relative range, etc.
 - (b) Howitzers, however, should be well subdivided, probably with three sizes between the limits given. A subdivision of 400 millimeters or 16 inches, 305 millimeters or 12 inches, 240 millimeters or 9.2 inches, checks well with theoretical requirements. The latter Howitzer will probably be mounted upon a caterpillar and need not be considered here.
- 476. In coast defense, targets are practically all of class (b), paragraph 472. Of necessity, plunging fire will be conducted at shorter

ranges than direct fire; those targets requiring the largest calibers, however, will generally also be at the greatest ranges.

477. SUBDIVISION BASED ON REQUIREMENTS OF SERVICE.—In the spring of 1918 the allied armies were planning a great offensive for the year following and elaborate consideration was given to heavy artillery requirements. The following condensed tabulation is based on the report of the allied conference on this subject.

FOR DESTRUCTION.

Callber required.	Range required.	Traverse required.	Time for preparation.					
520 millimeters	18	(Limited	Do.					
FOR COUNTERBATTERY WORK.								
240 millimeters.	22 22	All rounddo.	Minlmum. Do.					
FOR INTERDICTION.								

•	-	-		4				-		 _,	_	_	
240 millimeters				36 j	Al) ro	ນກ d ວ	• • • • • • • • • • • • • • • • • • •	• •	 	 	Mi	ulmu Do.	.m.

The railway guns in other armies also give some information along this line. Some of these are as follows:

Caliber.	Caliber length, maxl-mum,	Range.	Traverse.	Time for preparation.
232 millimeters. 305 millimeters. 232 millimeters. 305 millimeters. 305 millimeters.	45 40	Km. 16.7 13.1 24.7 23.1 31.0	Deg. 360 360 20 20 4	Fairly small. Do. No preparation. Do. Do.

The German railway mounts were:

Caliber.	Caliber length, maximum.	Range.	Traverse.	Time for preparation.
170 millimeters		#m, 26.0 20.4 23.1 27.7 26.2 (17*) 55.0 (50°)	Deg. 26 95 40 40 Epi. 360	10 minutes. 2-4 days. 10 minutes. 3-6 days. No preparation. 3 weeks.

A. 30-caliber howitzer is also mounted on this same carriage.

It will be noted that this list includes no mortars or howitzers. The German mortars and howitzers, even up to the largest calibers (420 millimeters), were generally arranged for wheel transportation. The one exception is the 420-millimeter mortar mentioned in the historical introduction. As, however, it has not been possible to obtain really authoritative information on this piece, it is not included above.

478. A further point can be brought out regarding maximum caliber. Only two 520-millimeter howitzers were made, neither of which was ever used on the front. The Germans, it is understood, experimented with a 540-millimeter howitzer, but it was not satisfactory. Both of these facts point to about 400 millimeters or 16 inches as the practical maximum caliber.

479. For coast defense, general conditions will not be outlined, but some idea of the calibers and ranges desired can be gained from the following table showing calibers of mortars, howitzers, and guns now in or contemplated for the coast defenses.

CANNON.

MORTARS.			
Callber	Caliber length, max- izaum for each caliber.	Muzzle velocity.	Approximate range at maximum elevation allowed by carriage.
10 inches	10	1,150 1,500	km. 9,9 14.0
HOWITZERS.	-		
12 inches	20 18	1,960 1,900	20. 0 20. 6
guns.	•		
2 24 inches. 3 01 inches. 4.00 inches. 4.02 inches. 5.00 inches. 5.00 inches. 6.00 inches. 1.00 inches. 1.10 inches. 1.21 inches. 1.31 inches. 1.41 inches. 1.52 inches. 1.53 inches. 1.54 inches. 1.55 inches. 1.55 inches.	50 55 40 48. 92 50 38. 6 50 40 50 42. 70 50 42. 867	2,400 7,600 2,300 9,600 2,600 2,700 3,350 2,250 3,200 2,700 2,750	7, 0 8, 0 8, 1 10, 3 9, 6 10, 8 16, 5 29, 2 11, 2 22, 0 38, 0

Judging from the above, it would seem that almost anything suitable for land warfare would also find a useful place in the coast-defense armament.

480. Conclusions as to Guns.—The conclusion as to the caliber and length of guns which should be adopted for a railway artillery program should be based upon the foregoing considerations and also upon a comparison with the pieces of heavy mobile artillery which cover the field immediately below.

481. In making this last comparison, account must be taken of the fact that mobile artillery, especially the pieces mounted on caterpillars, can be taken much nearer the front line than railway artillery; to bring this out, a tabulation of characteristics for some heavy wheeled, caterpillar-mounted and railroad guns, is given on page 602. On the basis of this data, another curve similar to plate 58 has been drawn, but this time with abscissæ representing the distance of the target from the front lines. On this, the field covered by each of the guns, also trench artillery and bombing planes, is indicated, plate 437-

482. In view of all of the foregoing, the following is felt to be a

logical selection of guns for a railway artillery program:

12-inch 20 to 25 caliber howitzer for destruction and counterbattery work.

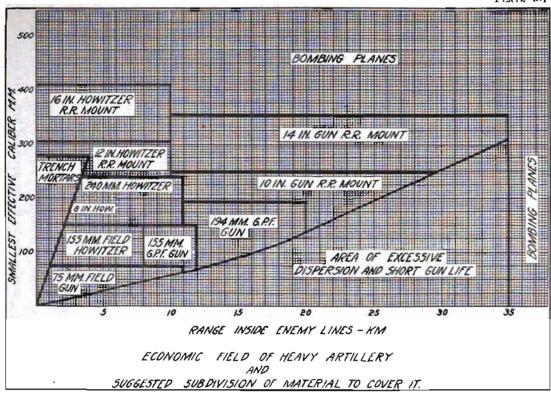
16-inch 18 to 25 caliber Howitzer for destruction.

10-inch 50-caliber gun for destruction and interdiction.

14-inch 50-caliber gun for distant destruction.

The fields of these guns have been plotted on the curve, plate 437. It will be noted that the subdivision, in general, follows the requirements of the theory before outlined, except for guns of intermediate range between the 14-inch 50-caliber and the 16-inch howitzer, and the 10-inch 50-caliber gun and the 12-inch howitzer. In these cases, it is felt that most targets, existing at ranges of more than 10 kilometers from the lines, will be of the type which can perfectly well be handled by a sufficient number of smaller shells (10-inch instead of 14-inch and 194-millimeter instead of 10-inch), so that occasions for using the 10-inch and 14-inch guns at short ranges ought to be rare. It is telt that these guns are also well suited to coast defense.

483. Mounts.—In section 2 it was brought out that types of mounts (considered on the basis of traverse and anchorage) were assigned according to the number of different targets to be fired upon (amount of traverse required) and the time available for the preparation of emplacement. Other characteristics, as extent of elevation, are determined by the type and size of gun to be mounted. A consideration of the report of the allied conference and of general



practice in the French and British armies shows these requirements to be as follows (these points have already been partially brought out in section 2):

(a) For heavy destruction at short range:

Traverse: It is seldom that more than one target need be covered at a time and limited traverse, 10-12 degrees, appears to be satisfactory.

Time for emplacements: These guns often must work close to the front line. It is highly important that they advance, deliver their fire, and retire as quickly as possible. Time for emplacement should therefore be as small as is practicable.

(b) For destruction at long range:

Traverse: As above, but 2 degrees is sufficient.

Time for emplacement: Abundant leisure is usually available for construction of emplacement of this class.

(c) For counter-battery work:

Traverse: 360 degrees if possible: 60 degrees as a minimum.

Time for emplacement: These pieces must be even more mobile than those for destruction at short range. Time for emplacement should be the minimum consistent with the above traverse (one or two hours).

(d) For interdiction:

Traverse: Practice in the armies indicates that limited fire with a fair amount of traverse (60 degrees) is sufficient for railway mounts. This is further justified by the probability that smaller mobile guns on caterpillar mounts will cover the field for which all round fire railway mounts would be required.

Time for emplacement: This should be the minimum consistent with obtaining the traverse required.

(e) For seacoast defense:

Traverse: Field of fire 60-180° perpendicular to track. Must be possible to sight, traverse, and elevate the mount up to the moment of fire. It must be possible to do this for a battery simultaneously. This will probably involve much auxiliary equipment.

Time for emplacement: Should be fairly short.

CONCLUSIONS AS TO MOUNTS.

484. Appropriate mounts for each of the guns decided upon, both for land service and coast defense, will next be considered, and the various characteristics which the services demand of it, will be tabulated.

485. Twelve-Inch, 25-Caliner Howitzer.—A mount of the general design of either (a) the 12-inch howitzer mount No. 8, or (b) the 10-inch, is recommended. The desirable characteristics for the services of counter-battery work and destruction, which this design should possess, gun mount plates 59, 60, and 438 to 448 are, for each of the design details:

Recoil: Cradle, with pneumatic recuperator.

Spur gearing with anti-friction device on the trunnions.

Elevation:

Ratio about 2 degrees elevation of gun per turn of handwheel.

Elevation to 65 degrees.

Traverse: Top carriage, center pintle type, with all round fire. Railway car: Drop frame flat car type, but strongly reenforced.

Anchorage: Track platform and struts, like American 8-inch. Ammunition supply: Crane and tray.

For seacoast defense, recoil mechanism or shock absorbers for seats of personnel should be added.

486. SIXTEEN-INCH, 25-CALIBER HOWITZER.—This mount is for fire of destruction only. It is felt that a combination of the top carriage of the 16-inch howitzer, model 1918, MI, the struts of the 12-inch howitzer, the base ring and steel sliding shoes of the 14-inch model E, and certain rolling recoil features fulfills the requirements in respect to time for emplacement, wide angle of fire, and adaptability for coast defense. The following detailed characteristics should be included:

Recoil: Cradle, with pneumatic recuperator.

Spur gearing with anti-friction device on the trunnions.

Elevation:

Ratio, 1.5 degrees elevation per turn of handwheel. Elevation to 65 degrees.

Traverse: Top carriage traverse, limited fire, 8 to 10 degrees. (Electrical translating motors for counter-recoil and training on an epi).

Railway car: Girder type.

Anchorage: (a) Rolling, (b) strut, (c) base ring.

Ammunition supply: Crane and shot truck.

Recoil mechanism or shock absorbers for seats of personnel and air brakes set by the recoil might well be added, so that the mount might be used either as an emplacement (base ring) or as a rolling recoil mount for coast defense, if the latter method were found necessary.

487. TEN-INCH, 50-CALIBER GUN.—This mount must supplement the long guns on caterpillars on interdiction and long-range destruction work. It must be capable of quick emplacement, should have a wide field of fire and should be able to deliver a number of shots in a minimum of time. A consideration of these points leads to the following recommendations on desirable characteristics:

Recoil: Cradle, with pneumatic recuperator.

Spur gearing with anti-friction device on the trunnions. Elevation:

Ratio, 1 degree elevation per turn of handwheel.

Elevation to 45 degrees.

Traverse: Car traverse:

On trucks for limited fire of 11 degrees.

On center pintle for limited fire of 60 degrees.

Railway car: Girder type.

Anchorage:

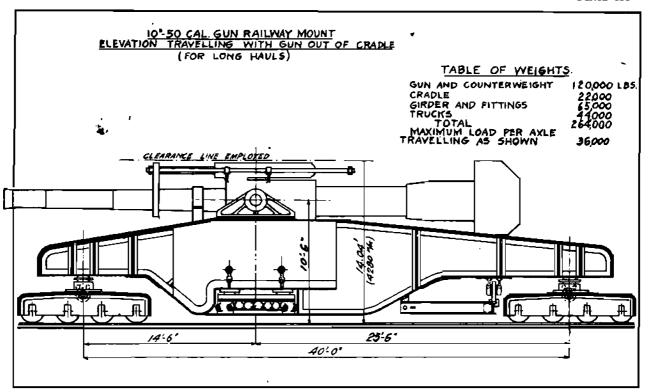
Rolling for 11 degrees fire.

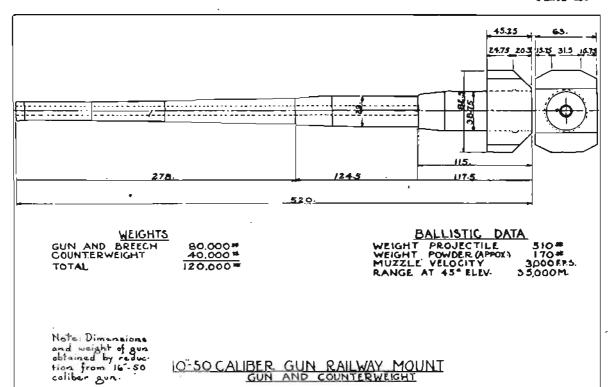
Track platform and struts for 60 degrees fire.

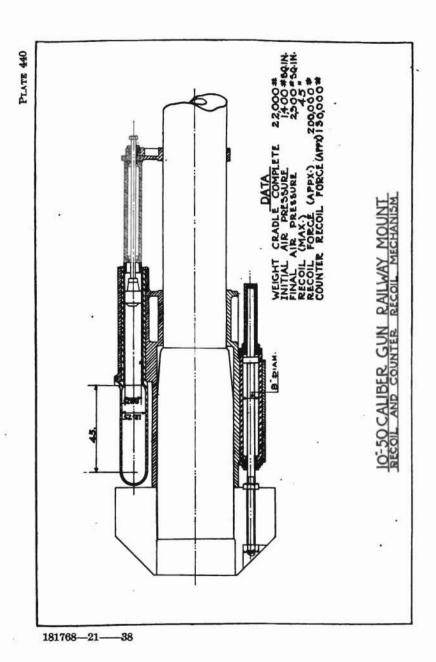
. Ammunition supply: Crane and shot truck.

Plates 59, 60, and 438 to 448 show how this design might be worked up. While details have not been investigated, enough has been done on each important feature to demonstrate that nothing is required of it beyond that required of a similar feature on an existing successful mount. It is believed that this type of mount would be well adapted to emergency coast defense.

488. FOURTEEN-INCH, 50-CALIBER GUN.—This mount will be used for the longest range destruction work. It will, in general, be employed some distance back of the lines, ample time will be available for placing it and its field of fire at any time is apt to be narrow. It is recommended that the carriage suggested for the 16-inch, 25-caliber howitzer be used likewise for this gun. An elevation of at least 50 degrees and an elevating gear ratio of 0.5 degrees per turn of the handwheel is recommended.







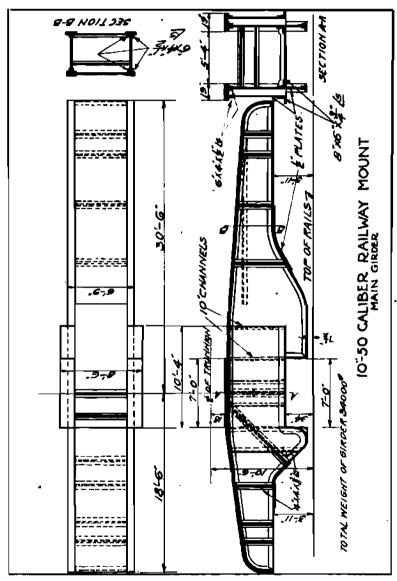
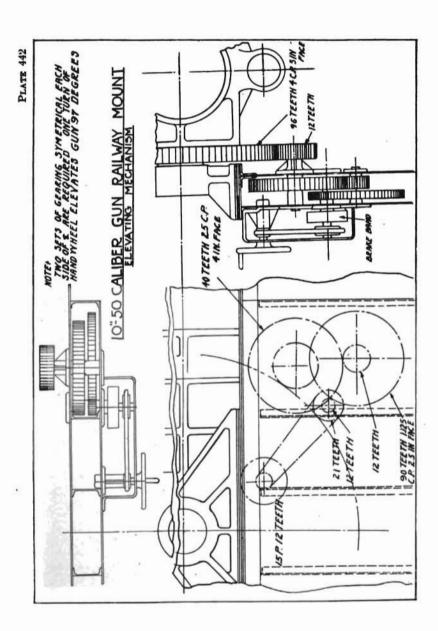


PLATE 441



I'LATE 443

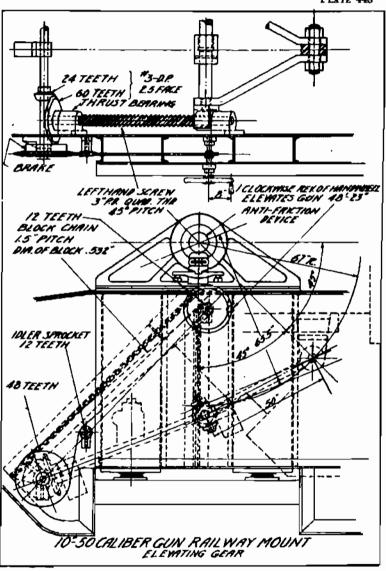
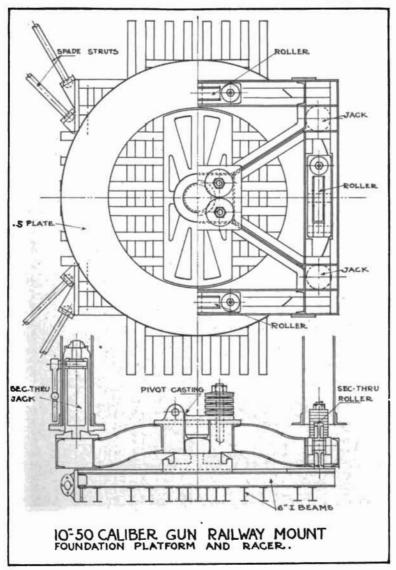
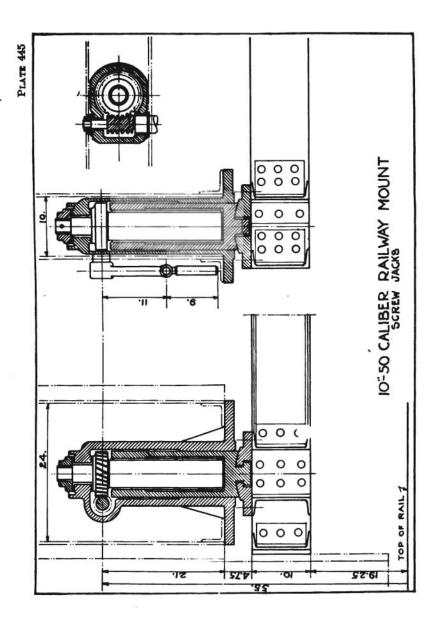
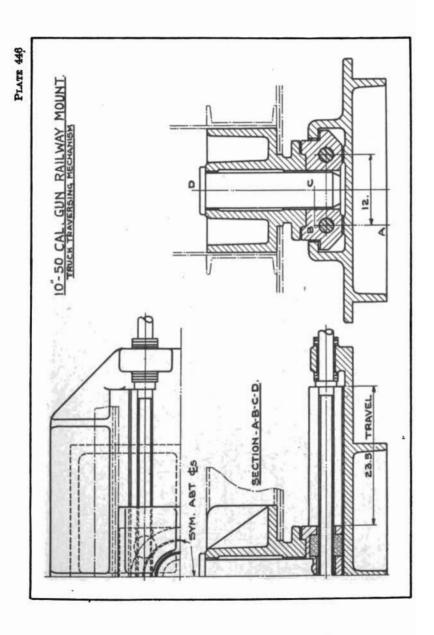
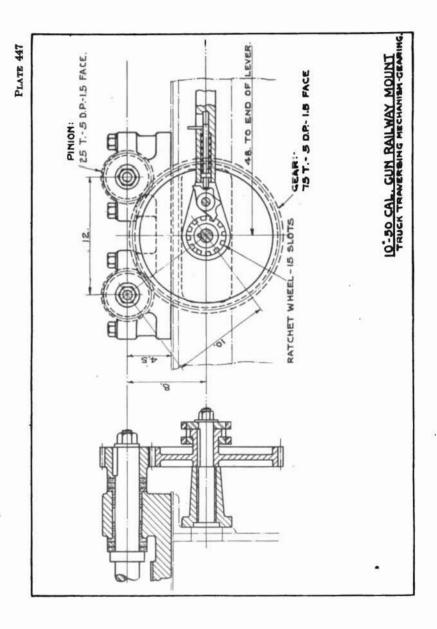


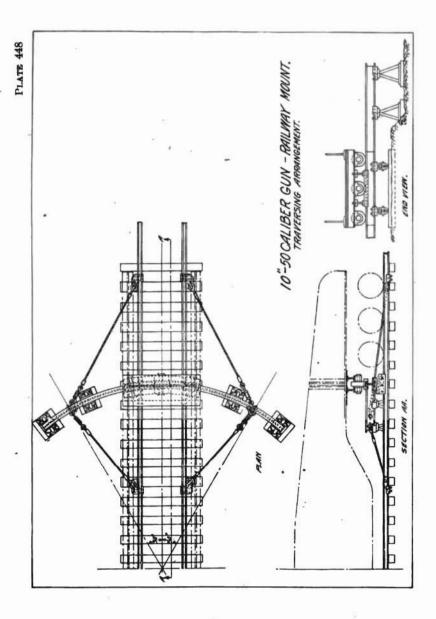
PLATE 444

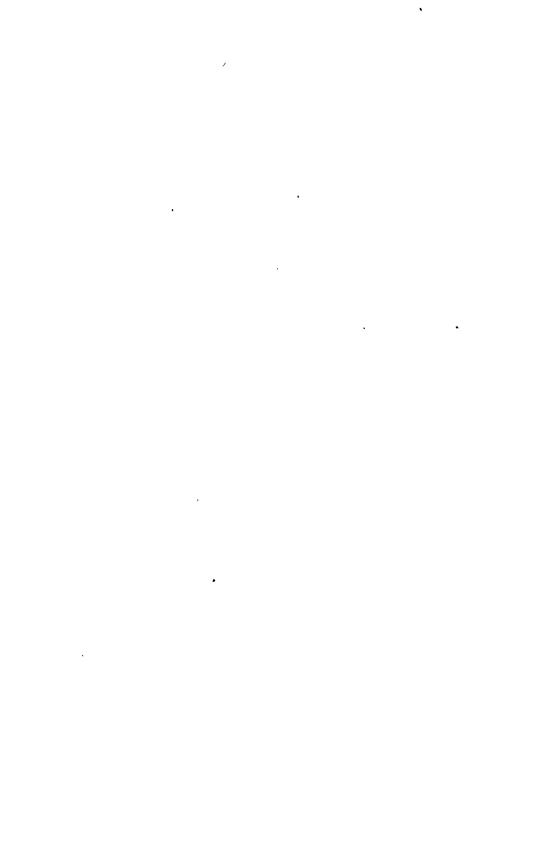












SECTION 5.

PROCEDURE IN PREPARING FOR ACTION IN LAND WARFARE.

- 489. In brief and in effect the procedure in preparing batteries or groups of railway artillery for action is as follows:
- 490. The commander of the heavy artillery receives instructions to operate on a certain group of targets in any of the sectors covered by the various armies. (This of course is based on the assumption that all the heavy artillery is available for use in any of the armies.) In the event that the heavy artillery be divided into units, a unit being allowed to each army, then the commander of the heavy artillery assigned to any given army will receive his instructions from the commander of that army.
- 491. The targets in the group assigned may be any of the great variety noted under the heading, "Scope of utility of railway artillery." The significant point is that they are always of the type that may be termed "fixed," in the sense that they can not be moved, or are not likely to be moved, in a short time. This makes it possible to prepare for an action in a thorough and accurate manner, and with comparative deliberation. As given in the instructions to the heavy-artillery commander, the targets are in terms of coordinates with reference to the adopted system of quadrillage. When given in such coordinates they may be readily located on any military map and the necessary firing positions selected and prepared.
- 492. The orders mentioned above are transmitted to the artillery officer, likely a colonel, directly in charge in the sector concerned, who, after consideration of the characteristics of the targets and the probable operating conditions, decides upon the type of artillery required, and places a request with headquarters that a certain number of groups of railway artillery of the desired caliber be ordered to report in that sector for service. The staff of this officer further carries out the work of reconnaissance, selecting the firing position, terrestrial observation posts, and parking stations for the troop trains. The orienteur officer in charge attached to the staff proceeds with the work of preparing the necessary data for laying out the epi curves, etc.
- 493. Upon receipt of orders from the railway artillery headquarters the group commanders proceed with their troop trains to the sector designated and report to the officer in charge. The troop

trains are parked in prearranged places and the personnel of the various batteries at once proceed with the work of laying all necessary telephone lines, constructing epis, dugouts, etc. When all preparations to the minutest details have been completed, the group commander orders the portion of his personnel still at the artillery camp to proceed to the front with the guns. Each gun, with its attendant ammunition cars, is provided with its own locomotive. It is desirable always to have the guns arrive during the night and placed on the firing positions so that firing may begin as soon as it is light enough for satisfactory observation. This observation may be either from terrestrial posts or from the air; if terrestrial, it is desired to have three posts. It is desired to have the observation handled by airplanes, if at all possible, inasmuch as they are able to make their observations approximately over the targets.

- 494. If necessary or desirable, the guns may remain in one position for several days, since it may take the enemy four or five days or even longer to locate them and place artillery of sufficient range to return fire. Generally it is not necessary to remain in one position very long. In one of the engagements in which the Americans, operating 320-millimeter howitzers, were engaged, one battery fired 11 shots and the other 45 shots. The targets were demolished and the battery moved out at night and returned to camp about 30 miles behind the lines. They remained in camp until needed at the front again for similar service.
- 495. The understanding that at first prevailed in the Ordnance Department that the various units of railway artillery would be kept in the field, as the term is used with reference to light artillery, proved erroneous. This artillery may occasionally be idle for months and when needed it may be for only a few days, after which it is moved back to the permanent camp. Incidentally, the shops for the maintenance of this artillery are likewise located in the permanent camp.
- 496. Construction.—As indicated in the preceding, considerable construction of various kinds is necessary in preparation for the use of railway artillery. This is described and specified very completely in the instructions for "Trackwork for Heavy Artillery," issued by the French Army. This manual is so good a treatise on the subject that it is quoted entire at the close of this section.
- 497. CAMOUFLAGE.—The subject of camouflage is too broad to be more than touched upon here, but it will be outlined by indicating first the means developed for locating batteries, and on the other hand, the steps taken to defeat these means and hide the positions. In general, camouflage is of less importance, relatively, on railway artillery than on the lighter pieces.

498. Gun positions are located by:

Ordinary observation from-

Advance posts.

Balloons.

Airplanes.

Aerial photography.

Ranging by flash of guns.

Ranging by sound of guns.

Ranging by earth vibrations from fire.

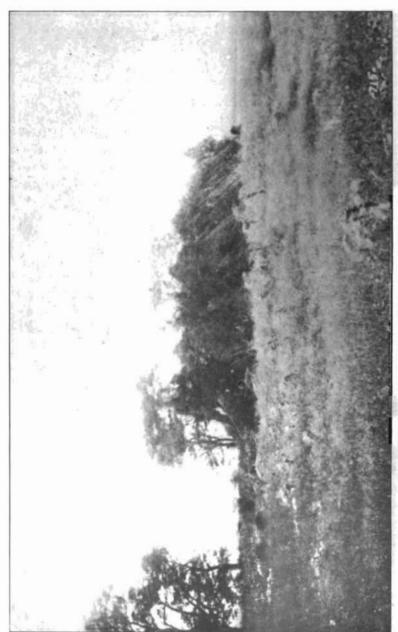
It is understood that the French have learned, through captured documents, that the Germans were, in many cases, able to obtain almost complete information as to French battery locations by these means. The French, on the other hand, found when the Germans were driven back in certain regions, that the German batteries they had previously located by these methods, were correctly located, and represented in one instance 27 out of 30 of the batteries in the region studied.

499. The chief scheme used to camouflage railway mounts and positions are, first, and most effective, the choice of a protected position, in a wood or a ravine. Next, the careful concealment of all approaching tracks and all preparations. Then the use of painted paulins, tree branches and raffia nots, plates 449 and 451, as well as the camouflage painting of the mount itself, plate 174. Perhaps one of the most effective schemes was the interchange of gun positions and, of course, as previously brought out, the removal of the railway mount before suitable counterbattery fire could be brought into play.

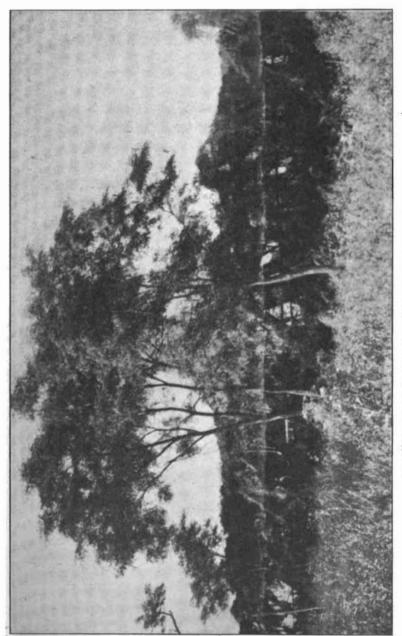
500. In view of the great accuracy of the various locating methods successful concealment for long periods is almost impossible, and more reliance is to be placed on delivering the necessary shots and then getting away rapidly.

501. The most elaborate known attempt at concealment is the emplacement installed at Pont-a-Mousson between Nancy and Metz, plates 452 to 456. The concrete roof is about 2 meters thick with several meters of earth above. The gun was fired through a hole in the roof, as can be seen from the photograph. There was never any indication that the Germans ever located this battery, though their observation planes were seen above it while the gun was firing on a bridge just west of Metz on the first two days of the St. Mihiel offensive.

502. In another instance, a railway mount was located in the bottom of a very steep and wooded valley, and fired through a tunnel dug through the hill in front of it. This position was never located by the Germans so far as is known.

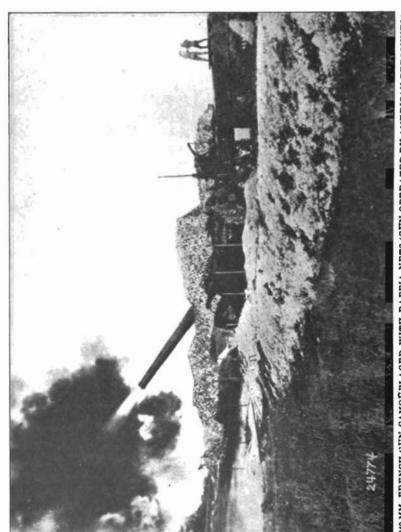


CAMOUFLAGE OF RAILWAY MOUNTS WITH TREE BRANCHES.

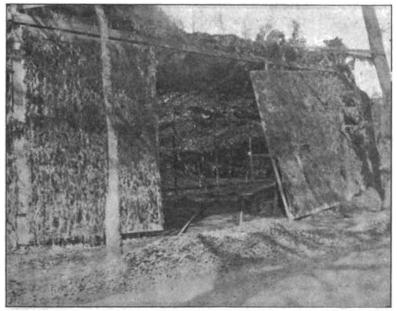


CAMOUFLAGE OF RAILWAY MOUNTS WITH TREE BRANCHES.



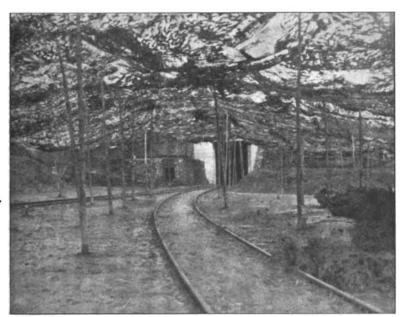


30-MM. FRENCH GUN CAMOÜFLAGED WITH RAFFIA NETS (GUN OPERATED BY AMERICAN PERSONNEL).



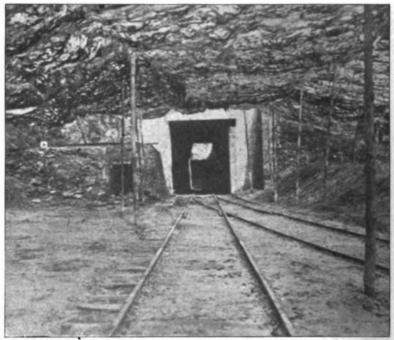
CAMOUFLAGED ENTRANCE TO EMPLACEMENT FOR 340-MM. FRENCH GUN (CONSTRUCTED BY AMERICANS).

PLATE 453

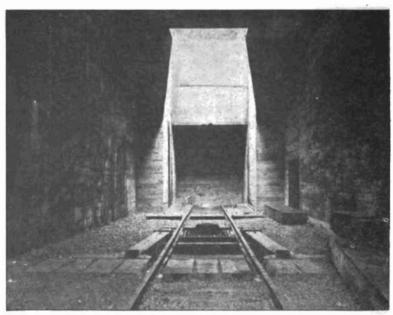


CAMOUFLAGED ENTRANCE TO EMPLACEMENT FOR 340-MM. FRENCH GUN (CONSTRUCTED BY AMERICANS).

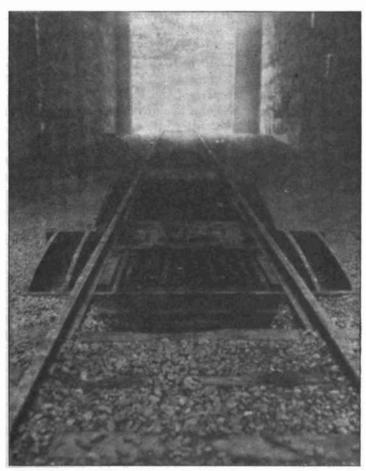
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ENTRANCE TO CONCRETE SHELTER TO 340-MM. FRENCH GUN (CONSTRUCTED BY AMERICANS).



INTERIOR OF CONCRETE EMPLACEMENT FOR 340-MM. FRENCH GUN (CONSTRUCTED BY AMERICANS).



INTERIOR OF CONCRETE EMPLACEMENT FOR 340-MM, FRENCH GUN (LOOKING TOWARD THE ENTRANCE).

TRACK WORK FOR HEAVY ARTILLERY.

503. The material which follows on "The study and locating of track," "Track construction," "Placing of firing track," etc., has been extracted almost verbatim from a translation of a French pamphlet entitled "Manual of the Course for Student Officers," (36). This manual was prepared by the French Service for the instruction of officers assigned to their Railway Artillery Camp at Mailly, France. The translation was made by Capts. C. L. Nelson and A. N. Clark, Engineers, U. S. R., and was edited by Maj. Orville Benson.

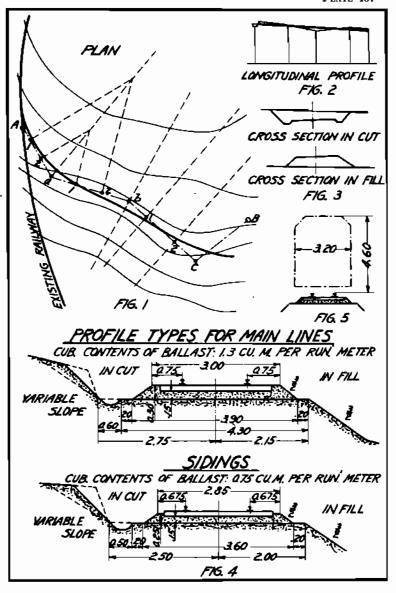
504. STUDY AND LOCATING OF TRACK.—The studies and the locating of railway tracks are made by topographic parties of certain regiments of the Corps of Engineers, or of the Standard Track Construction Batteries, who are part of the Railway Artillery Reserve.

505. The beginning and end of a line are always indicated approximately by the authority that orders the studies. After making a study on the topographic map, the chief of the party makes a reconnaissance on the ground, covering the zone of the eventual construction. This reconnaissance will reveal to him the points of necessary passage, the points favorable for the departure A, and of arrival B, the obstacles to be avoided, the parts defiladed from the view of the enemy, the camouflage which will be necessary, and permits the determination of the strip of land on which the location is possible.

506. In default of a good topographic map, it is necessary to run a grade line on the ground, to make sure that the maximum grade is not exceeded. The topographic party then proceeds to survey the aforesaid strip of land. An experienced operator runs a preliminary traverse line there, formed by a series of straight alignments, of which the extremities are indicated on the ground by stakes. These stakes and alignments are chained (Aa, ab, bc, cB) and angles A, a, b, c, figure 1, plate 457, are measured with a transit, beginning with A of the traverse. These measures allow the making of a map of the traverse which is plotted on a scale of 1/2,000 or 1/5,000. On this traverse numbered stakes are also placed at all points (1, 2) where there is a break in the slope. A level line is then run over all the points, A, 1, 2, a, b, c, B. At all these stakes a cross profile is surveyed reaching 30 to 40 meters to each side, in the same manner that the longitudinal profile was made.

507. All of the lines of the traverse and the traverse profiles (cross sections) are drawn on a plate. In this way one has the position and elevation of all of the essential points of the strip of terrain; it is easy to draw the contours on the plate. Another more rapid method is to take stadia shots directly to the essential points of the terrain from instrument stations placed successively at stations A, a, b, etc., of the traverse. On this contour map it becomes possible

PLATE 457



to study a line answering all the technical conditions imposed, which will be discussed in detail later. This line, drawn in a heavy or red line on the map, permits the plotting of the longitudinal profile, in which the distances between different points of the terrain appear as abscissæ and their elevation as ordinates, figure 2, plate 457. On this longitudinal profile one may draw the red line or profile of the track by a series of grades joining the track of departure with the objective without ever exceeding the maximum grade.

- 508. When the red line passes underneath the black line representing the terrain the track is in cut; when the red line is above the black line the track is on fill, figure 3, plate 457. The difference in elevation between each point of these two lines of the profile gives the height of the road bed above or its depth below the natural surface.
- 509. In taking account of the width of the road bed and its emplacement one may, in utilizing only the longitudinal profile, compute the volume of cut and fill necessary, and accordingly determine the number of days' work. When the project is approved the line is located on the ground; that is, it is staked out.
- 510. STAKING.—The numbered stakes of the preliminary survey are useful in laying out on the ground the line adopted, the distances from the line to these stakes being scaled from the map.
- 511. CENTER STAKES.—The stakes are placed at the points of tangency of the curve with the tangents. In the French Railway Artillery Engineers' Service, these stakes are painted white and carry the letter "T" with a number in order; intermediate red stakes, of which the numbers are of the same series as the preceding ones, are placed every 50 meters, on tangents, and every 25 meters on curves. A tack is driven in the stake at the center of the track.
- 512. ELEVATION STAKES.—These stakes are set in such a manner that the head has the elevation of the top of rail. They are placed at the side of the track, about 2½ meters from the rail. Breaks in grade are painted in yellow and marked "C. P.," with a serial number on stakes. Intermediate stakes of the same color every 50 meters are numbered in a series distinct from that of the line stakes.
- 513. Specifications of Standard Track.—Minimum radius of curves, 150 meters; tangents to be inserted between reverse curves, 25 meters; maximum grade on tangents and on curves above 150 meters radius, 20 millimeters per meter, or 2 per cent. Reverse grades should be joined by a vertical curve of 1,000 meters radius. Gauge, distance between the inside of the heads of the rails. The gauge used for artillery is slightly wider than for standard track work, e. g., tangents and curves over 150 meters radius (4 feet, 8.875 inches), 1.445 meters; curves of less than 150 meters radius (4 feet, 9.312 inches), 1.445 meters. Spacing, C to C, of ties, 0.80 meters;

width of subgrade, 4 to 5 meters. The clearance required for rolling stock is given by sketch, figure 5, plate 457. The rails ought to be at least 1 meter from any obstacle, and it is necessary to increase this distance on curves to allow for leaning and the cutting in of long cars. A detailed discussion of clearances for American railways as well as French is given in paragraphs 664 to 688.

- 514. EARTHWORK.—The study of projects ought to be conducted in such a manner as to make necessary the least possible amount of earthwork. The execution of earthwork may be done, either by the method of "borrow and deposit," in which necessary earth is taken from borrow pits along the side and excess material is thrown back over the sides of the cuts; or by the method of "transports," in which the earth is carried from the cuts to make up the fills. While the earthwork is in progress care is necessary that the grade stakes be not disturbed.
- 515. The depth to which it is necessary to go to reach the subgrade may be indicated to the excavators in a striking manner as follows:

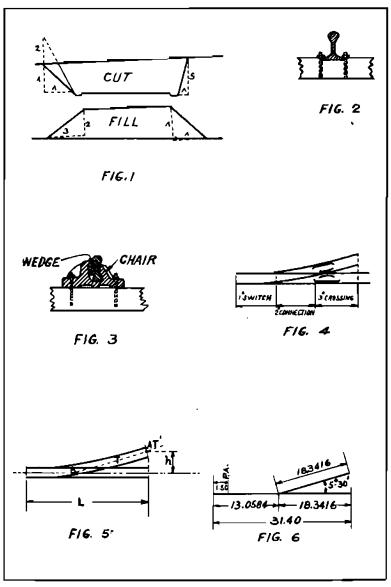
 (a) In cut, a hole, half a meter square, is made at the side of each stake with the bottom at the level at the subgrade; or, the depth to which it is necessary to descend is written on the head of the stake.

 (b) In fill, the red line of the fills is represented in profile with pickets of the proper length. In fills the height is increased 10 per cent to allow for settling. The earthwork is controlled with a set of "nivellets en bois."
- 516. Side Slopes of Cut and Fill.—In ordinary soil the slope of a cut varies between 1 to 2 in height to 1 on the base. In chalk one may adopt 5 in height to 1 on the base. The slope of fill is 2 in height to 3 on the base; sometimes this is reduced to 1 to 1 to reduce the base, figure 1, plate 478.
- 517. AMOUNT OF EARTHWORK PER EXCAVATOR PER DAY.—A man ought to dig and load into a wheelbarrow, or dig and throw with one toss of the shovel, from 2 to 4 cubic meters of earth in cut in a 10-hour day. In firm soil, e. g., chalk, or moist soil, i. e., clay, the production may fall to from 1 to 3 cubic meters. With a shovel a man can load or unload from 8 to 10 cubic meters of soil, gravel, or ballast per day.

TRACK CONSTRUCTION.

518. MATERIAL.—In France two types of track have been adopted; they are distinguished by the form of the rail and the method of attachment to the ties. These are: (1) Voie Vignole or T rail; the tie is notched to provide a seat in which the flange of the rail rests; the rail is fastened to the tie by two or three screw spikes, figure 2, plate 478. (2) Voie & Coussinets (chair track); the rail has a nearly symmetrical section and is held by a wedge in the chair, which is fastened to the tie by screw spikes, figure 3, plate 458. The rails

PLATE 458



PROFILES, RAIL SECTIONS, AND SWITCHES.

should be inclined 1 in 20 toward the axis of the track so that the bearing surface of the head of the rail and the wheel tread may be parallel; in the first type it is the seating in the tie that gives the inclination, and in the second it is the shape of the chair.

- 519. Superelevation.—To facilitate traveling on curves of short radius an inclination is given to the track by raising the outer rail. For railway artillery rolling stock, which travels at a slow speed, a difference of elevation of from 3 to 5 centimeters between the two rails is sufficient for curves of a radius of from 150 to 125 meters. To bring the two rails on tangents to the same level the difference is eased off along a length of about 12 meters beginning at the point of tangency.
- 520. Expansion and Joints.—A small space is left between the rails when they are laid to allow for the expansion of the metal. This interval, which is a function of the length of the rail, should be very large in summer and very small in winter. In France a variation of 0.6 millimeters per meter is allowed between the two extremes in temperature.
- 521. Plan of Placing or Laying Ties.—The spacing between ties may vary between 0.5 and 0.85 meters. In general the following numbers for rails of different lengths are adopted:

Length of rail.	Ties per rall.
5.50 to 6 meters	. 7
8 meters	. 10
11 meters	. 14
12 meters	16

- 522. Plan of Placing the Rails.—In standard gauge military track laying the rail joints should be exactly opposite each other. Since the lengths of the radii of the inner and outer rails on curves differ to the extent of the gauge of the track, it is necessary to supply rails of different lengths to obtain this result. For quick laying in a campaign the rails are usually supplied in equal lengths, and the following principles are then adopted:
- (1) T rails: Little attention is paid to the locating of the joints. They may fall on a tie, since this does not prevent the rails from being spliced and screwed to the ties; or, the joints may come between the ties. In this latter case the ties at the joint should be a little closer together to lessen the suspension of the rails.
- (2) Chair rails: With rails of this type it is necessary, of course, that the joints come between the ties, and the requirements, especially on curves, will be a little more severe.
- 523. In laying rails of either type the following principles are followed with reference to the relative position of opposite rails: (a) On long tangents the joints should be even. (b) On curves the joints should be staggered with an overlap of about half a rail length-

(This necessitates starting with half a rail length at the point of tangency.) (c) On crooked lines or wherever tangents are not predominant, staggered joints should be used throughout the entire length.

TRACK LAYING.

- 524. Before beginning the track laying it is necessary to check for the stakes that may have been disturbed during the excavating. These stakes will serve as guides for distributing the ties and the rails, and after the ballasting has been completed they will serve as guides for the exact placing of the track. Following are brief rules for the laying and assembling of the track components:
- (a) Ties: The ties are properly spaced by means of a gauge and are aligned approximately through the use of the rail notches as guides.
- (b) Rails: As noted in the preceding paragraphs, spaces should be left at the joints for expansion, and care should be exercised to avoid any considerable displacing of the ties.
- (c) Joining of the rails: The connecting or fish plates are placed at the rail joints and bolted tight.
- (d) Adjustment of ties: After the rails are bolted together the exact positions of the ties may be marked off on them with chalk, and the ties adjusted to this marking by hand or with bars.
- (e) Spiking or wedging: As soon as the ties are adjusted the rails may be spiked to them, using a gauge to keep the rails the proper distance from each other, if T rails are being used. If rail chairs are provided, these chairs will have been previously spiked to the ties at proper distances apart and the rails need only be wedged into them.
- (f) Firing track: For this section of a track T rails of a heavy weight and from 11 to 12 meters in length are always used. No particular attention need be paid to the locating of the joints. Particular attention must be paid, however, to the locating of the ties with respect to the holes in the structural steel sliding beams.
- 525. Turnouts.—A turnout is composed of three parts. These are (1) A switch, which is the operating section; (2) a junction, which carries two ordinary tracks; and (3) a crossing with a frog or guard rails. A crossing may be defined in two ways—that is, either by the angle between the two tracks which it cuts, for example, 5 degrees and 30 minutes, 7 degrees and 30 minutes, which are angles in use on the Est Railway, or by the tangent of the angle between the two axes.
- 526. STUDY OF TURNOUTS.—In preparing for the placing of a switch, the type having been determined, it is necessary to know the follow-

- ing: (1) The total length of the turnout, L, and (2) the position of the tangent of the turnout, TT, which is defined by the position of the point B, with intersection of the axes, with reference to one end of the switch, and by the angle between the two axes, figure 5, plate 478. Figure 6, plate 458, illustrates the standard 5-degree 30-minute, model 1909, 45-kilogram rail switches in use on the Est Railway.
- 527. Ballasting and Adjusting.—Before ballasting, grade stakes are set regularly at intervals of 25 meters as well as along or inside the track at changes in grade. The top of a stake gives the elevation of the rail (inside rail on curves). The quantities of ballast per meter of track are: (1) Through tracks, 0.60 cubic meters to 0.75 cubic meters, according to the nature of the terrain; (2) firing tracks, 1.200 cubic meters.
- 528. The straightening, adjusting and tamping is handled successively, and with repeated corrections until the desired regularity both in plan and profile is obtained. The raising of the track includes: (1) The raising and bringing to grade of points at the grade stakes, and (2) the raising and bringing to grade of all points between the grade stakes. In this second raising three little blocks of equal heights may be placed at the points first raised and the point being raised for convenience in sighting. The track having been raised by means of screw jacks or levers, the ballast is gradually filled in and tamped under the ties with tamping picks or bars. The tamping should be energetic under the rails and to a distance of from 30 to 35 centimeters on either side; under the middle of the tie it should be very gentle. The straightening is handled ordinarily by a gang of about a dozen men using large bars. The track is lined up with the line stakes by measurement and for final and fine adjustment by . sighting with the eye.
- 529. Eolmer Switch.—The installation of the standard type of switch generally requires two days with a gang of 20 trained men and necessitates the complete cutting of the main line for a distance of about 30 meters for several hours. The Eolmer is a removable switch which can be placed in a few hours at any point whatsoever of a track in service and without taking up the rails. To clear the main line for traffic, it is necessary to take up only three pieces of the switch, which can be done in about 10 minutes.
- 530. The whole of the Eolmer switch is represented in figure 1, plate 459. It is shown here turned to the left. The switch points, b and D, fit to the main line rails on the top instead of along the side. The tops of the switch points are shaped to a gentle grade and raise the wheels gradually until the flanges are above the rails of the main track. At this point the wheels may follow the switch and they definitely leave the main line when the one wheel crosses the frog at \mathcal{O} , figure 3, plate 459. Figure 2 shows how the points are attached

PLATE 459 DETAIL OF FROG 田田田田田 EXISTING ROAD 3001300 EOLMER REMOVABLE SWITCH. F1G. 23 22.933 Z DETAIL OF SWITCH POINTS 7.520 0 000 U ELEVATION AB and figure 3 shows the type of frog used. It is necessary to take up only three pieces of the switch, the two points and the frog, to reestablish the main line. The pieces of rail MM may be left in place. Naturally the turning off of a locomotive and railway gun carriage to an epi by means of a removable switch requires care and very slow speed. It has been used, however, with perfect success and the saving in time in installation is so great as to commend its use.

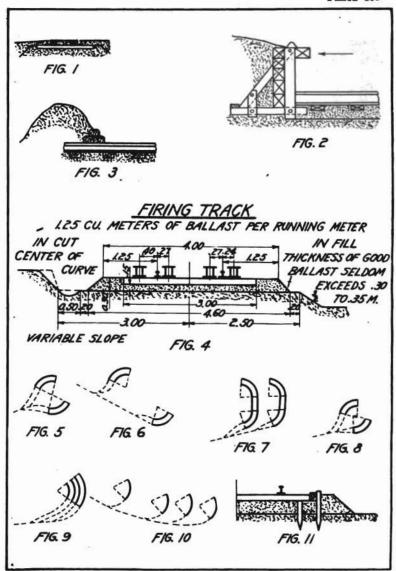
531. Grade Crossings.—Crossings for the passage of wheeled vehicles are shown in section in figure 1, plate 460. On both sides of the track, slopes of well rammed earth covered with gravel or rock are made. Inside the track the space is brought to the level of the rails by well rammed gravel and earth flanked by ties or timbers placed 0.05 meters from the rails, and spiked to the ties. It is of course preferable to build up the entire space between the rails at grade crossings with timbers if they are available.

532. BUFFER STOPS.—At all dead ends of tracks some variety of buffer stops should be constructed. If material and time are available, an effective stop can be constructed of ties reinforced by a mound of earth as shown in figure 2, plate 460. If less time is available a stop may be constructed of several ties laid on the track and reenforced by a mound of earth, figure 3. A single tie backed up by two rail clamps of the variety used with the 19 and 24 centimeter French railway mounts is effective.

533. Reversing Triangles (WYES).—In artillery parks or yards or in a position on the front in the vicinity of which a number of firing positions have been installed, i. e., any place where it is not practicable to provide turntables of the usual type for reversing locomotives, railway mounts, etc., reversing triangles or wyes must be provided. In yards this may be especially laid out for the purpose or on the front it may be made by connecting an existing spur with the main line by an additional curve forming a triangular inclosure or wye.

EPIS.

534. Railway mounts are operated on a specially constructed piece of track called a "firing track" (epi de tir). These tracks (epis) are constructed for two classes of gun mounts: (1) Those which are supported by firing beams (Poutrelles) at the moment of firing, so that the shock of recoil is absorbed by sliding friction along the beams; (2) those in which the shock of recoil is absorbed by hydraulic cylinders, the mount being securely clamped to the track which, in the case of the heavier guns, is reenforced to withstand the shock of firing. Epis are curved in such a way that guns can be oriented, to cover the desired field of fire, by moving them along the track. The "Orienteur officer" places grade marks on the web of the outer rail of the curve as a guide for the battery commander in placing the gun.



CROSSINGS, TRACK ENDS, AND FIRING TRACKS

SLIDING MOUNTS (MATÉRIELS a GLISEMENT).

535. Guns mounted on sliding carriages are fired from a track called a firing track or epi, laid on the arc of a circle so as to permit the orientation of the piece to cover the field of fire selected. For firing, beams (poutrelles) are placed parallel to the rails and screwed to the ties; the jacks which relieve the wheel trucks of their load bear on these beams and provide friction for absorbing the shock of recoil.

536. Firing Beams.—The above platforms or beams are about 37.50 meters long. This length permits 8 grads (7.2 degrees) field of fire for a curve of 200 meters radius and 10 grads (9 degrees) for a 90-meters curve. They should not be fastened to the ties before the gun is ready to occupy the position to fire. They are then fastened with screws in the holes that will be mentioned in the next paragraph.

537. Firing Epi Construction.—The firing epi for each piece is a curve constructed with special T rails (45 kilograms) and chamfered ties (0.15 by 0.30 by 3 meters). Firing tracks have no super-elova-The gauge is from 1.45 meters (4 feet 9.062 inches) for a curve of 150 meters radius to 1.455 meters (4 feet, 9.312 inches) for the smallest radius (90 meters). The special ties are not shod, but are delivered bored for track screws. They should be spaced 0.54 meters, C to C, on center line of track. Holes are provided in the ties to receive the screws for both rails and beams. To prevent ballast from getting into these holes it is well to plug them with straw or hard grease. The ends of the tie in which the distance between the holes for the rail and the beam is the greater must be laid on the inside of the curve. After the ties are laid, their proper position should be verified by running the eyes over these holes, figure 4, plate 460. Track screws of a standard type and size only should be used in these ties; nothing else that might change them or prevent their being used again should be used. At rail ends, the screws must be carefully screwed down and not driven down with a hammer.

538. BALLAST.—The ties should be laid on a bed of excellent ballast, 0.15 meters (6 inches) thick, extending 1.50 meters beyond each end of the ties. The tie should be completely buried in the ballast throughout its length. The resulting bed of ballast will be 4 meters wide at the top and 4.60 meters at the bottom; this will require about 1.50 cubic meters per meter of track. The ballasting should be done with special care, the tamping being done preferably with bars.

539. Epi Limits.—An epi is usually defined by its point of beginning and the direction of its two ends, but to avoid confusion it

should always be made plain whether extreme directions refer to the desired field of fire, or to the construction of the track itself. Sufficient trackage must be provided for the auxiliary equipment, either ahead or to the rear, depending on its relation to the working of the gun; the length of the curve must exceed that corresponding to the field of fire prescribed in order to provide for corrections in aiming, usually an equivalent of 10 degrees are added to each end, making a total increase of 20 degrees in the curve.

- 540. Epi Specifications.--In general the firing epi has a uniform curvature; but in a very exceptional case the terrain may make it necessary to adopt an irregular curve; in such case the radius must never be less than 90 meters (approximately 300 feet), and the extreme direction must be maintained in such a manner that the tangents to the curve will sweep the entire field of fire progressively as the gun advances along the epi. In general also, the epi should be level, but to facilitate its adaptation to the terrain, a grade not exceeding 5 millimeters per meter (5 per cent) may be used. In every case the epi should be constructed in cut, so as to assure a solid platform for firing; exception may be made for those sections of the epi occupied only by the end trucks in extreme fire since they would never receive the shock of recoil. If fill is unavoidable, as for instance in crossing a ditch or depressed road, the fill must be made with good ballast well rammed, with no voids whatever that could cause settlement. When the cutting becomes deep it is well to have its sides made in steps to facilitate the get-away of personnel at the moment of firing.
- 541. Battery Epis.—In whatever way the epis of a battery are arranged, sufficient space (at least 50 meters) must be allowed that there shall be no danger that one shall suffer from the blast of the other. When the two epis are near each other, they should be concentric so as to insure a common direction of fire. Usually two epis are constructed together with a common center, having respective radii of 90 and 140 meters.
- 542. Group Epis.—With a group consisting of four pieces, the "group epi" may consist of four epis together made up of two "battery epis" in some form, bearing in mind the "blast" mentioned in connection with "battery epis." Parallelism of four pieces may be secured by arranging the epis in a forceps form, figure 5, plate 460. This form may be approximated by separating the curve centers, figures 6, 7, and 8. Other forms necessitated by the terrain are, the "palm," consisting of four epis with a common center, figure 9, or of four epis curving the same way, but having different centers, figure 10. A gun must always be at least 50 meters from the field of fire of neighboring pieces.

MOUNTS WITH HYDRAULIC RECOIL (MATÉRIELS & FREIN).

543. Among the gun carriages provided with hydraulic recoil, some of the lighter ones (6 to 10 inches), may fire from any track on the condition that the track be reenforced whenever it is used for firing. The material is not dismounted. The stability of the carriage is secured generally by the use of clamps which fasten the carriage to the rails and by hinged outriggers provided with jack-screws supported by footings placed on the ground. The stability is increased by adding several well-tamped ties under the rails, and by placing, under the ends of the ties, on the side of the recoil, longitudinal ties held in place by several stakes sunk deeply into the ground. If the ground is too yielding, long stakes may be sunk into the ground between the ties, on the heads of which supplementary ties are placed. In addition longitudinal ties are laid against the ends of the ties and are held in place by stakes, figure 11, plate 460. A thorough tamping under the ties concerned is indispensable.

544. The carriages for the larger guns (12 to 16 inches) require the construction, under the firing track, of very strong platforms sunk into the ground, of which the details differ according to the caliber and the design of the mount. The installations require from one-half to four days, likewise according to the caliber and design.

CAMOUFLAGE OF RAILWAYS. (37)

545. The camouflage of railways, especially firing positions, to conceal them from the view of airplanes and above all to keep them from appearing on photographs is very difficult. The Germans, who were very attentive to this question were, in general, not able to conceal their tracks and firing positions except in the woods.

546. At the beginning of the appearance of the railway artillery at the front, little attention was paid to the camouflaging of the tracks. The mobility of this artillery, the great distance between the pieces and its distance from the lines (nearly always more than 5 kilometers) have been its best protection. It has remained almost unharmed, while according to the maps found on prisoners, it is established that the curved epis of the Somme were nearly all known to the enemy, and most of the firing took place in view of the "drachens" (observation balloons). It is nevertheless of interest to conceal preparations for attack from the enemy and to hide from him the cannon in action to avoid counter-battery fire.

547. Access Tracks.—It has been recognized as advantageous to conceal the switch and the first 200 meters of the turnout to a firing position under tents of cloth and fireproof raffia. It is desirable to place the tracks in a woods, disturbing the trees as little as possible, and bringing the branches together over the track. Tracks may be

laid along the edge of woods to conceal at least partially the new earthwork, or on beaten roads, thereby avoiding earthwork which easily attracts attention. The rails and ties may be masked under ballast or cloth and deceptive road ends may be made at a noticeable point such as quarry, a wood, a farm, or another road by a false branch made up entirely of painted cloth. The true entrance should be concealed under cover of the woods, making a turnout and a false entrance further along.

548. Firing Epis.—Experience has shown that one need not consider the masking in a group of curved epis of any but the directing gun ("Directrice"), by concealing the switches and completing the curves by false track. Complete camouflage of the whole work would be long and of little use. It will be well to make false epis in the neighborhood by means of a simple turning over of the earth with a plow, by simulating pieces covered with tarpaulin, and by placing on the true epis false shell holes to make it appear that the access to or the use of them is impossible.

549. Single epis, curved or straight, are much easier to camouflage. First, one can often place them in woods or ravines; when they are very short, as in the case of the howitzers, it is even possible to cover them completely with cloth or raffia. It is desirable to avoid the use of geometrical curves in the access tracks. In open country these epis can be prolonged by a false road or a false track to a natural point of attraction, as another track or road, or to a quarry or a town; if one doesn't succeed in concealing the railroad, one has at least a chance for hiding the epi itself, and that is what is most important.

GARAGES.

550. Components.—Each garage for heavy railway artillery comprises chiefly, a line track, a passing track paralleling the line track throughout the length of the garage, and which serves as a maneuvering track, some storage tracks reserved either for firing trains or for personnel trains, and branches on the maneuvering track, plate 461. At some place in the complete system there must be a Y track for turning. In certain garages, the tracks for personnel trains are not ballasted. This economical plan presents no difficulties provided the personnel trains only are admitted to them. As far as possible, no tracks for firing trains should have dead ends, in order that they may not be blocked in. Garages are established at suitable points where the ground is level, near a road to facilitate supply renewals and where water may be had. Usually two or four groups can be united.

551. LENGTH OF TRACKS.—The lengths adopted for the storage tracks vary according to the equipment. For a group of four 32-centimeter guns there is generally allowed 350 meters for the firing

SCHEME OF DEVELOPMENT OF RAILWAY ARTILLERY.

trains and 350 meters for the personnel trains. The radius of 150 meters has been adopted as the most suitable for curves on garage tracks; for sharper curves over which guns are to be moved super-elevation must be given.

552. WATER.—If the water supply points be near, the locomotives go there, separately according to a rotation regulated by the commanding officer of the camp. If there is a place to fill water cars, or if the source of water supply is distant, provision is made for one or several water trains, which circulate as conditions require, to supply all groups which occupy the garage. In case the source is distant, locomotives supply themselves at the water cars of the group.

553. FUEL DEPOTS.—It will be convenient to arrange, at a suitable storage point, a small depot, independent of the fuel supply which the groups maintain in the supply cars, where all the groups may replenish their supply.

554. Miscellaneous Installations.—It is advisable to build a ballasted road to accommodate automobile trucks, for supply replenishment, between the nearest main road and the garage. In each garage, there should be built a hut or switchman's shanty for the yardmaster and a hut to serve as a telephone central for connecting the units stationed at the garage. The telephone lines will connect the yardmaster with the "chef de la gare" of the junction of the railway artillery line with the main line and with the post of the switchman stationed at the exits of the garage. It is necessary, moreover, to provide for each garage such operating equipment as red and green flags, green, red and white lanterns, lights for the yardmaster's hut, and materials for maintenance of switches. The maintenance of the garage trackage is the duty of the permanent personnel of the garage, aided if necessary by auxiliaries furnished by the various groups. A small supply depot should be established for this purpose.

MAINTENANCE OF TRACKS.

555. REQUIREMENTS OF GOOD TRACKS.—A good track must be regular in alignment and profile without kinks or sharp bends. The inspector satisfies himself on these points by going over the line and verifying the regularity of alignment, straight or curved. To verify the profile by a glance of the eye, place the eye from time to time close to the rails, looking along the track as far as possible. The ends of the rails must not touch each other, a space between them sufficient for expansion being required. Each joint must be formed with two splice-plates fastened with four bolts (for heavy work six bolts are used). Flange rails must be fastened to each tie with at least two screws; double-headed rails must all be wedged into the bearings by the wedges of wood or iron. Every bent or broken rail makes

traffic dangerous, and must be replaced. Loose ties (insufficiently tamped) must be made solid by tamping; broken or rotted ties which depress under the passing of trains must be replaced at once, as they cause derailments. The spacing of the ties must not exceed 80 centimeters, C to C, to avoid bending of the rails. The ballast must be porous and firm; if the base is wet or muddy it lacks resistance, and must be drained or the track will not retain its profile.

556. Dressing and Raising the Track.—Defects in the alignment are rectified by a gang of 6 or 10 men, equipped with pinchbars or levers and directed by a gang foreman. The pinch-bars are set under each rail and the men heave together, at the command "Oh Heave!" At points which are too low it is necessary to raise the track by means of large wooden levers called handspikes or with small jacks. The jacks are set under the ties, and never under the rails. The ballast should be adjusted under the lifted ties. For correcting the track grade, three wooden leveling blocks of the same height should be used; two are set on the rails at points of correct grade and the third on the rail to be raised. The point between is at grade when the tops of the three blocks are in the same plane. The heights of the three leveling blocks should always be checked before using them.

557. Replacing and Tamping Ties.—To replace a tie it is necessary to remove some ballast, remove the screws from the tie, lift out the wedges and the cradles and withdraw the tie by means of picks. The new tie is then slipped under the rail and tamped temporarily; after placing the screws, or the cradle and wedges, if used, the tamping is completed. Four workmen are sufficient. In tamping, two men work together at the same end of a tie, piling a little ballast against each side, and forcing it under by blows of a mattock or a tamping bar.

558. Replacing the Rails.—The splice plates and a row of screws or spikes are removed along the rail if flange rails are used; the extreme splices and all the wedges are removed if double-headed rails are used. A cut of rail of equal section and length may then be set in the opening, the men being placed about a meter apart along it. Its flange will be engaged under the heads of the screws or spikes in place, or in the opening of the cradle, some space being allowed at the two ends of the rail. The splices and the screws, spikes, or wedges will then be replaced and the job finished by dressing or tamping. All screws and bolts should be greased before screwing them in.

559. REPAIRING A CUT MADE BY A SHELL.—A shell of large calibor falling on a track ordinarily breaks 8 or 10 ties, and twists the rails for a distance of from 20 to 30 meters. It is necessary first to provide the ties, rails, splices, holts, wedges, and screws estimated to be required for the repair. Laborers should be set to filling the hole,

ramming the soil in layers at the same time that the trackmen are removing the twisted rails and the ties on which they rest. As soon as the shell hole is filled the ballast can be restored and the ties and rails replaced, spliced, and spiked or wedged. The work will be finished by dressing the track for alignment and profile, and complete tamping.

560. Track Drainage.—New drainage ditches should be made deep and old ditches kept clean. They should always be provided in cuts and on level ground to assure a flow of the water. If necessary, drains of tile, stones, or of bundles of boughs should be installed beneath the track and joining the two ditches.

561. Handling of Track Material.—Two men can carry an ordinary tie (weight 80 kilograms). It requires three men to carry a tie with cradles attached (weight 125 kilograms). Four men are needed for firing track ties (3 meters long, 160 kilograms). Rails ordinarily weigh, double headed, 38 kilograms per meter, and flanged, 45 kilograms per meter. For the carrying of rails, an allowance of one man for each meter of length is made. Small supply depots of rails, ties, splices, etc., for possible repair work, are generally established at intervals of about 1 kilometer along military railroads. It is necessary that all officers of railway artillery be able to direct a small job of construction or repair work.

DEPLOYMENT OF RAILWAY ARTILLERY ON THE ATTACKING FRONT.

562. Railway artillery, being difficult to conceal, is ordinarily employed in the mass. In the region of attack, there are united as many positions as possible with a view to meeting various tactical situations; positions in the rear for demolition fire, advanced positions to be occupied on the days of attack, and contingent positions for pursuit, whence to support the infantry as long as possible.

563. There is constructed, parallel to the front, a supply line (voie de recade), plate 461, connected with two operating lines. This track is generally constructed by the S. C. F. (service de Chemin de Fer—equivalent to our railway engineers). From this line, which the Army uses for rationing and the transportation of munitions, there extend various branches which lead to position 1, 2, 3, etc. Near the supply line there are distributed the garages for firing trains and personnel trains, the water-supply points, etc. A single supply line may extend over 40 to 50 kilometers length along the front.

Nors.—The French use the expression "voice de recade," here translated "supply line," to apply to the track system approximately paralleling the entire western front from Dunkirk to Belfort, and style the train that traverses it daily "The Recade."

564. The access tracks that lead to the position are sometimes 4 or 5 kilometers long; with an average of 2 kilometers to a position,

the four curved epis of a group represent a total length of from 600 to 800 meters. The equipment of an attacking front generally calls for the laying of 200 kilometers of track, taking into consideration the retention of existing trackage. The amount of earthwork involved in the construction of the access tracks and firing tracks of a group sometimes reached 8,000 to 10,000 cubic meters per position, the average being 2,000 to 3,000 cubic meters per position. The extent of trackage for railway artillery garages and ammunition dumps on the front of any army is from 15 to 20 kilometers.

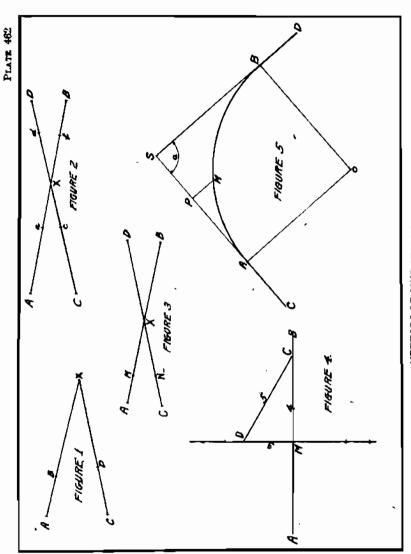
565. A military laborer, who costs 5 francs per day, excavates 2 cubic meters per day and lays 4 meters of track on an average. Ordinary ties cost 15 francs each, firing track ties 25 francs, and rails 60 francs per 100 kilograms. This gives an idea of the expense of railway artillery trackage. It is necessary that the entire personnel of the railway artillery be entirely familiar with their duties, to make the best use possible of the powerful and expensive equipment that is entrusted to them.

SUPPLEMENT TO TRACK LAYING.

566. To STAKE OUT A STRAIGHT LINE BETWEEN TWO FIXED POINTS.—The chief of the party places himself 20 meters behind one of the points and sends the rodman 50 meters ahead. The rodman places and drives a stake so that its foot is in line with both fixed points. (Lining it in by eye.) He continues to place stakes at desired intervals which the chief of the party lines in from his original position as long as he can effectively do so. If the line goes through a depression, the chief may go forward and line up stakes with those already set.

567. To Find the Intersection of Two Alignments.—A rod or stake X, figure 1, plate 462, may be set at the intersection of alignments AB and CD, by placing observers at A and C or at stakes on AB and CD, respectively, who line in the rodman's pole or stake alternately until it coincides with both lines. If the rodman is using a stake, he carefully drops it and drives it in where its point strikes.

568. If the operator is alone, he stations himself at the approximate intersection and marks the spot with a stake, figure 2. He then places a second stake on AB about 10 meters from the intersection, lining it up with the first stake and A or B, as the case may be. Next a third stake is placed on AB and about 10 meters on the other side of the first stake. He then disregards the intersection stake and begins to line up the stakes a and b with A and B. From a he lines in b with B, moving b (not a) until it is in line. Then he sights from b and lines in a with A, moving a (not b) until it is in line. It may be necessary to go from a to b a number of times in



METHODS OF LINE STAKING.

this procedure until the stakes are perfectly in line. Stakes c and d may then be lined in with C and D in a similar manner. The locating of X as the intersection of ab and cd needs no explanation.

569. To Erect a Perpendicular at a Point M of an Alionment Determined by Two Stakes, A and B, Without Instruments.—This solution is based on the fact that if the legs of a right triangle are 3 and 4 or any multiple of 3 and 4 units in length the hypotenuse is 5 or a similar multiple of 5 units in length. From M toward B a distance of 4 units (meters, yards, or any length marked on a stick) is measured and staked at C. Then a length of 3 units is measured on one string or stick and 5 on another. The 3-unit string is attached to M and the 5-unit string to C. If their ends are brought together, keeping them uniformly tight, a point D is located on the desired perpendicular. MD is the perpendicular.

570. To Measure Distance Atong the Grade.—The chain is stretched on the ground. The rear chainman keeps his zero mark on the head of the starting stake, or against the pin already set. The head chainman stretches the chain and sticks the pin at the end mark. He stands on the side of the chain, the shoulders in line with the rear chainman, and head turned his way: he moves backward or forward according to the directions of the rear chainman. The arm extended indicates to which side he ought to go; the arm suddenly lowered indicates that he is to stake the pin.

571. After sticking the pin the chainman ahead moves on, keeping the chain stretched. When the rear chainman finds the pin previously set, he holds his zero mark and directs the head chainman, waving him on when the pin is stuck. When the head chainman is out of pins, he will still continue to stretch the chain its full length from the last pin set, then leaving his handle on the ground, he comes back to the rear chainman, from whose hands he receives anew the 10 pins, which he is careful to count while returning to his place. This is what is called the exchange of pins, which takes place every hundred meters. The chief of party takes note each time so as not to forget the number of hundreds.

572. To MEASURE BY HORIZONTAL STEPS.—If the ground slopes down the head chainman takes a loaded pin in his right hand, raises the handle to get the chain horizontal and pulling on it hard, lets the pin drop. He replaces it afterwards by an ordinary pin.

573. LAYING OUT A CURVE.—The tangents CA and DB, figure 5, plate 462, are given and they are to be joined by a curve the length of whose radius, R, is assumed, hence is known. If instruments are available, it is best, of course, to set a transit at A and having computed the subtended angle for a standard chain length, lay off from A successively the points on the curve to B. If a transit or compass is not available the curve may be staked approximately by the method of ordinates and abscissa as follows: For any abscissa

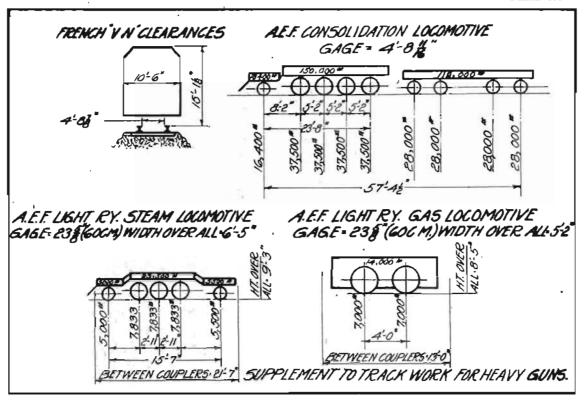
AP, which may be called X, the ordinate PM or Y is found approximately by the formula Y = X/2R. Thus, for example, if R = 150 meters, a table of ordinates and abscissa can be quickly computed.

The distances X are then measured from A along AS and the corresponding distance Y perpendicular to AS, thereby locating points on the curve. It will be best not to attempt to locate more than half the curve from AS. The same values may be used in locating the other half of the curve from BS.

Table of coordinates on the tangent for laying off curves.

(Equal distances every 10 meters on the arc.)

from .	Radius of the curve (meters).														
the arc	90		100		110		120		125		130				
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from y.					Radiu	s of the c	ourve (m	eters).							
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A. B. P. CONSOLIDATED, LIGHT RAILWAY STEAM, AND LIGHT RAILWAY GAS LOCOMOTIVES.

SECTION 6.

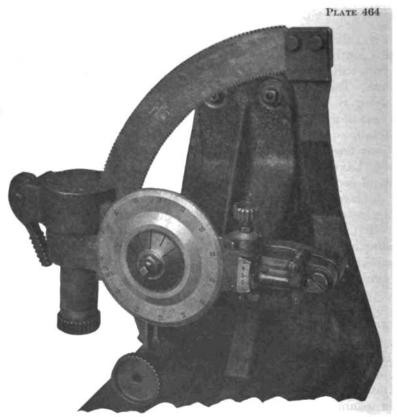
PREPARATION OF FIRING DATA AND SCHEME OF FIRE CONTROL FOR LAND WARFARE.

574. This discussion of the preparation of firing data and the scheme of fire control must necessarily be brief, and hence incomplete. No attempt will be made to give more than a general outline of the procedure. The theoretical points connected with the different methods of laying the piece will be considered first. Next the procedure in the case of a sliding mount firing from a curved epi will be described in detail, and, finally, a discussion will be given of the various corrections made to firing data and the methods of determining them.

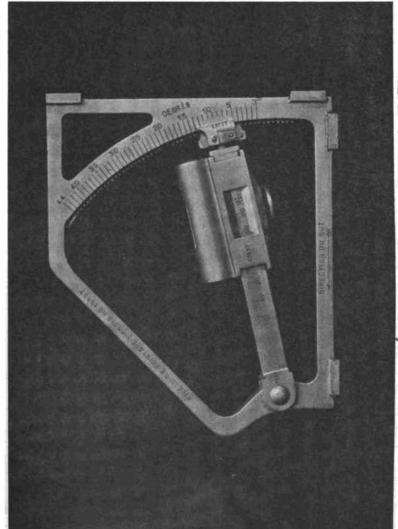
575. LAYING THE PIECE.—Laying the piece includes the operations of giving the gun the required elevation and direction. Laying in elevation is accomplished through the use of a vertical measuring instrument, such as the range quadrant, elevation quadrant, (pl. 464), or gunner's quadrant (pl. 465). Laying in direction is accomplished through the use of a goniometer (French) (pl. 466), or a panoramic sight (American) (pls. 467 and 468), in connection with an aiming or reference point.

LAYING FOR DIRECTION.

576. Laying for direction is accomplished through the use of a few instruments of which there is a wide variety of designs, and on one of two principles differing radically in their basic conception. Under the one principle the laying diagram assumes the reference point at a finite distance from the sighting instrument, and under the other it is assumed at an infinite distance. In either case the sighting instrument is set at a calculated or measured angle (usually calculated), which is one of the two supplementary angles between two vertical planes, one of which passes through the axis of the gun and the other through the line from the gun to the reference point, and the gun is moved until the vertical cross line of the instrument is laid on the reference point. Obviously, then, when the sighting instrument is laid on the reference point the gun is pointing in the direction of the target. To determine the deflection angle, it is necessary to know the gisement of the line from the theoretical position of the gun to the finite or infinite reference point and to be able

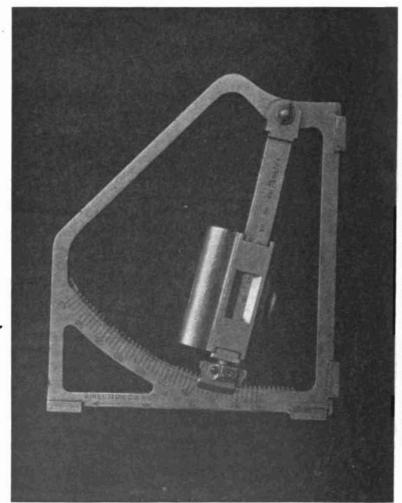


STANDARD ELEVATION QUADRANT USED WITH ALL RAILWAY MOUNTS.



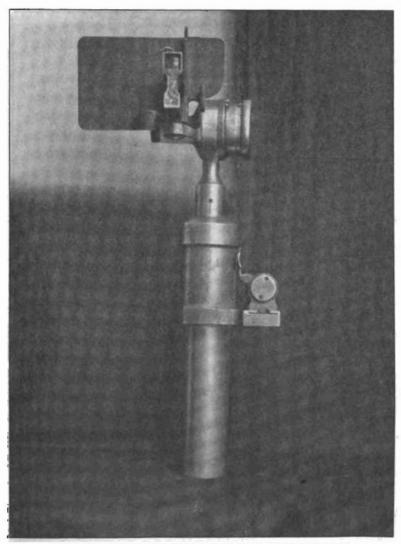
STANDARD GUNNER'S QUADRANT USED WITH MEDIUM AND HEAVY GUNS.

PLATE 465A



STANDARD GUNNER'S QUADRANT USED WITH MEDIUM AND HEAVY GUNS.

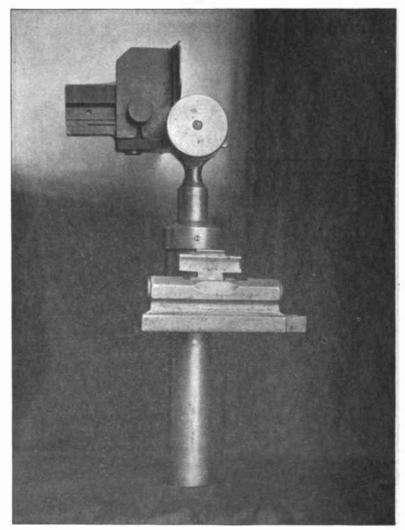
PLATE 466



GONIOMETER (FRENCH) FOR TRAINING GUNS IN AZIMUTH.

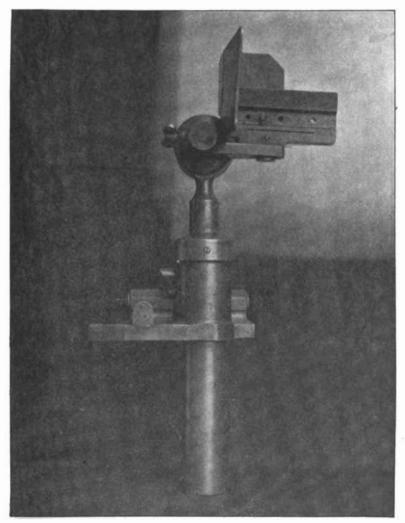
181768—21—41

PLATE 466A



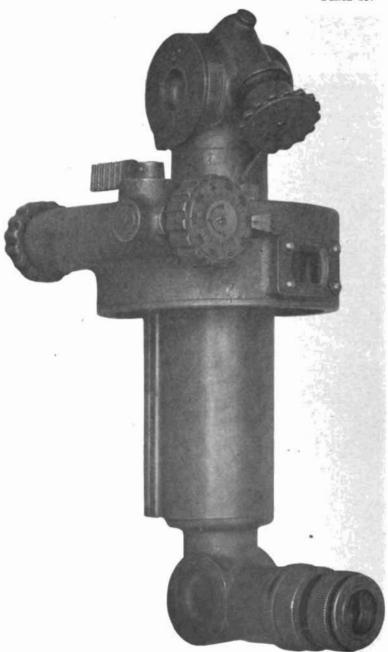
GONIOMETER (FRENCH) FOR TRAINING GUNS IN AZIMUTH.

PLATE 466B

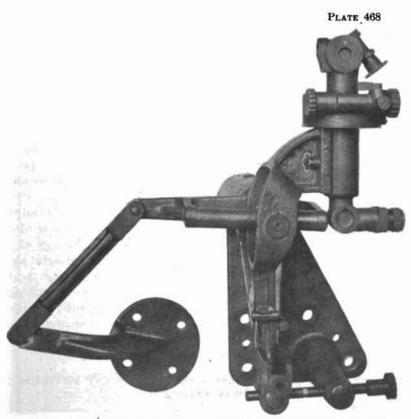


GONIOMETER (FRENCH) FOR TRAINING GUNS IN AZIMUTH.

PLATE 467



STANDARD PANORAMIC SIGHT USED WITH ALL RAILWAY MOUNTS.



PANORAMIC SIGHT MOUNTED ON AUTOMATIC SLOPE COMPENSATING MECHANISM.

to compute the gisement of the gun-target line. (The gisement of a line is its angular direction, measured clockwise, with reference to a north and south line through the zero point of the system of quadrillage. Azimuth is a somewhat analogous term, but is not exactly the same, since it is the angular direction of a line also measured clockwise, but with reference to a north and south line through the point at which the line is being considered. Since north and south lines are not parallel, obviously the azimuth of a line running, e.g., north 45° east, is not the same at points 5 miles or even 1 mile apart.)

577. Finite Aiming Point.—If the sighting apparatus is directed on a visible and fixed reference point, either improvised or natural, at a finite distance, this point is called a finite aiming point. Under such circumstances the goniometer, or panoramic sight, is always attached to the gun and is set at the calculated angle. This scheme of laying is most generally applied to field mounts and to railway artillery having fixed emplacements.

578. Infinite Aiming Point.—If instead of a visible and fixed reference point an aiming rule is used, we have what is called an infinite aiming point. An aiming rule is a bar of iron L-shaped in cross section about a meter and a half in length, which is mounted on two heavy iron stakes set about a meter apart (pl. 469). Provision is made in the mechanism on the heads of the stakes for adjusting the bar both vertically and horizontally. In the outside of one leg of the bar there is a V groove in which two of the legs of the small iron tripod holding the goniometer, or panoramic sight, slide. When mounted on this rule a sight may be moved through a distance of nearly a meter and a half, all positions of the line of sight being parallel to each other. The use of an aiming rule, of course, always involves the use of either another sight or a mirror, adjustable for horizontal angles, mounted on the gun. The use of the aiming rule will be described in detail later.

APPLICATION OF FINITE AND INFINITE AIMING-POINT METHODS TO RAILWAY ARTILLERY.

579. On the basis of methods of traversing and schemes of fire control railway artillery may be divided into three classes:

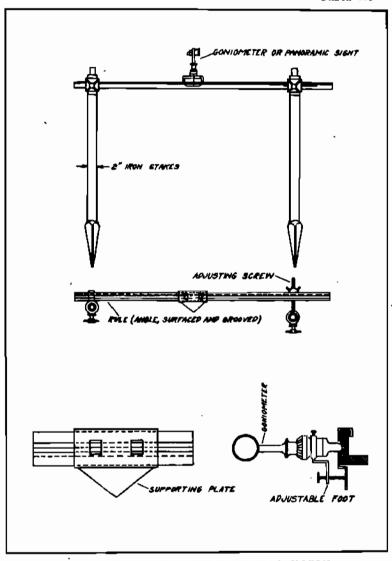
Class 1: Guns provided with traverse and firing from fixed or semifixed emplacements on a straight track.

Class 2: Guns provided with limited traverse and firing from a curved track.

Class 3: Guns having no traverse and firing from a curved track.

580. OPERATION OF CLASS 1—The emplacements of such mounts are so designed as to have satisfactory stability throughout the range of traverse provided. It is obvious that nothing can be secured in

PLATE 469



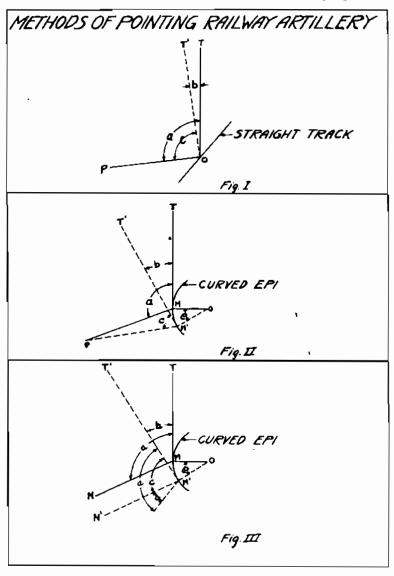
AIMING RULE FOR USE WITH RAILWAY ARTILLERY.

the way of traverse by moving the mount along a straight track. Since the emplacement is assumed to have satisfactory stability, there is no objection to the use of a finite aiming point. If OT, figure 1, plate 470, is the plane of fire, and the aiming point is P. and the deflection angle a is known, either from calculation or measurement, the gun is laid in direction by setting off on the sight an angle equal to a and traversing the gun until the vertical cross line of the sight is on P. If it is desired to change the direction of the plane of fire to OT', it is only necessary to set the sight at a new angle equal to a minus b and to bring the sight again on the aiming point P. The method of infinite aiming point is likewise applicable to this class of artillery, and the writer recommends its use if time permits. When the guns are operating at extreme ranges, and it is not possible to observe the fire for accuracy, even slight displacements of the emplacement may throw the plane of fire off the target. Displacement of the emplacement does not have this effect when an infinite aiming point is used.

581. OPERATION OF CLASSES 2 AND 3.—Guns which are provided with car traverse usually have so little traverse that it is necessary to operate them on curved tracks to cover a large target or to enable them to operate on several targets. Guns which have no traverse must of course always operate on curved tracks. Any mount which must be operated on a curved track can not be operated with entire satisfaction through the use of a finite aiming point. First, it is inevitable that the track will be displaced from firing, and, second, it is quite probable that it will be necessary to operate on more than one target from the same track. When a finite aiming point is used, a displacement of the track involves a correction in the deflection angle, and the calculation of this correction is laborious. Further, a change of target with a finite aiming point, figure 2, plate 470, involves a calculation in the determination of the new deflection angle far more laborious than is required when an infinite aiming point is used, figure 3, plate 470. Although angle e equals angle b, figure 2, there is no simple relation between angles a, b, and c, and the computation of angle c becomes an entirely new trigonometric problem. In figure 3 it will be seen that the determination of the new deflection angle c involves only the determination of the angle e. For, angle e equals angle b; assuming M'N' parallel to MN, angle e then equals angle d, since angles b and d are equal. (b plus c-a-c plus d.) The new deflection angle c therefore equals the old deflection angle a minus the angle e.

582. PROCEDURE IN DETAIL FOR SLIDING MOUNT ON CURVED EPI.—Under the head of "Procedure in preparing for action," section 5, it was mentioned that in the instructions received by the commander of heavy artillery to operate on a certain group of targets,

PLATE 470



the coordinates of these targets were given. From these coordinates the target may be located on a military map. On plate 471, T is one of the targets that has been so located. The artillery officer in charge of that sector decides that a position in the vicinity of G is to be the firing position and the orienteur officer, having the location of T and the approximate position of G, proceeds with the preparation of the data required for the construction of the epi curve as follows:

583. In general, one can see from any spot in France several prominent objects, church spires, monuments, etc., the exact locations of which are given in coordinates on the military maps; M, plate 471, is one of the points which the orienteur finds within view of G. Assuming that the artillery to be used is of the sliding type, class 3, the center and radius of the desired curve, the firing positions on the curve for the various targets and the extent of the curve must be determined.

584. From the approximate position of G, the center C is located, the radius being given, and if possible a stake is placed at C. The exact position of C is then determined from M and possibly other known points in sight by triangulation: The position of C is located in terms of the same system of coordinates as M and T. When the position of C is known, the gisement of the line C T is determined either from the map or by computation. With the length and gisement of the line C T determined, the epi is constructed and the various positions of C at which the gun will be placed for operation on the various targets are located, and the gisement of the various gun target lines G T determined.

585. After G is located (on the outer rail), two other points 31 meters in front and 4 to the rear are located. Through these two points a line is run which is extended to the rear a distance of 80 meters. At the end of this line the aiming rule is placed on two iron stakes A and R. This rule is about a meter and a half long and is normal to the G O line. Provision is made on the two iron stakes for any necessary adjustments of the rule. The next step is to determine the gisement of the normal to the aiming rule by means of a goniometer mounted on the rule. After the gisement of this normal is determined the value of the deflection angle O G T can be computed. It is possible to compute this deflection angle in another way, as follows: Knowing the gisement of the line C T and G O and the value of the parallax angle C T G, it is possible to compute the deflection angle, corrected for wind and drift, by the use of Wilson's correction board.

586. With the sliding type mounts it is not possible to operate with satisfaction, using a panoramic sight and a distant aiming point.

PLATE 471

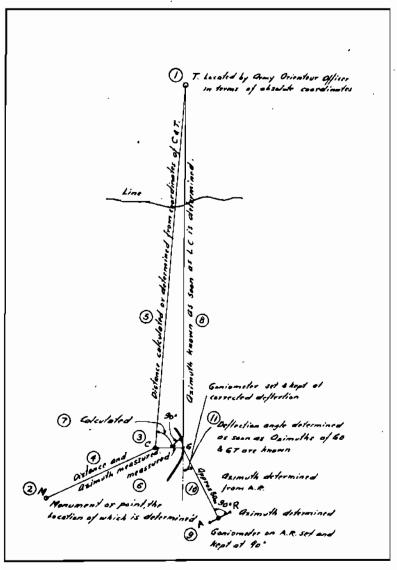


DIAGRAM OF FIRE CONTROL OF SLIDING TYPE OF RAILWAY MOUNTS.

In the event of lateral displacement of the track, which is inevitable, the continued use of the same deflection angle and finite aiming point does not by any means place the gun on the target. When the aiming rule is used, the only effect produced by lateral displacement of the track is the movement of the line of departure of the projectile to a new path, parallel to the former path and a distance from it equal to the extent of displacement, which may be only a few inches.

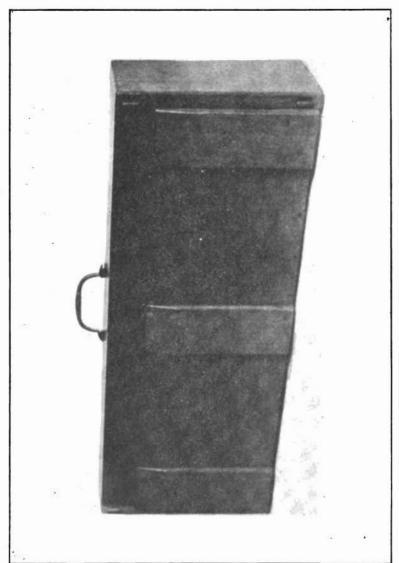
587. In action, the goniometer on the aiming rule is set normal to the rule. A mirror may be substituted for this goniometer. The goniometer on the mount is set at the corrected deflection angle. The mount is moved along the epi by means of the translating mechanism until the operators at the two goniometers G and O are each able to see the shank of the other goniometer at the same time. When this is possible, the gun is properly laid.

588. In the rapid determination of both the corrected deflection and range, Wilson's correction board, plates 472 to 475, is an invaluable instrument. By its use a computation that may require as much as an hour with possibility of error may be made with little mental effort and little chance of error in less than five minutes. This instrument determines the deflection, corrected for wind, drift, and parallax. It likewise determines the range corrected for atmosphere, wind, powder velocity variation, variation in projectile weight, and height of site.

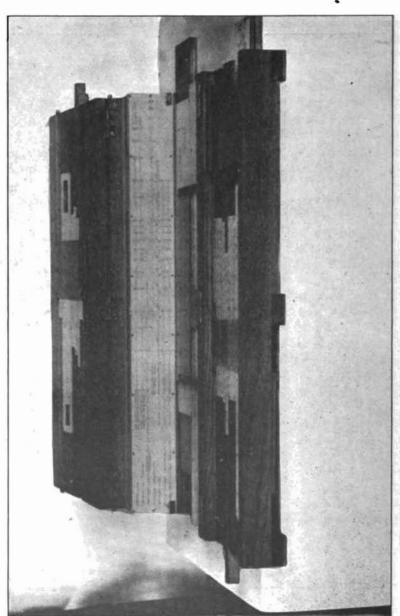
589. Comments concerning certain of the above factors entering into the correction of the range and deflection may be of interest. With reference to the atmosphere, a certain degree of saturation is assumed by the French as a standard. The thermometer and barometer readings then enable one to determine the density.

590. The air service of the Engineer Corps sends out every few hours, by wireless, data on the ballistic wind. Their method of determining the ballistic wind is as follows: Small balloons of a standard size, about a meter in diameter, are inflated with hydrogen until their lifting capacity is a certain amount. A balloon is released from a certain spot which becomes an origin for later computations and the position of the balloon is observed at regular intervals. From all of these observed readings mean directions and mean velocities are computed in terms of various elevations. The information that is sent out is then: Elevation, X; velocity, Y; direction, Z; Y being the mean direction of the wind for a maximum ordinate of X. This mean effective wind for elevation X is called the ballistic wind. This data is given for various elevations, so that the various battery commanders firing guns with trajectories of different maximum ordinates will all have the data they need.

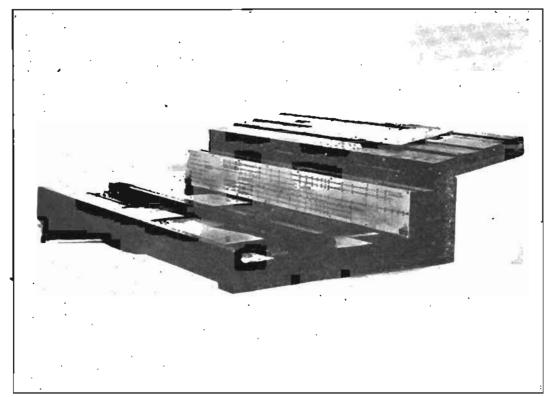
591. The correction board already mentioned may also be used to analyze certain results in the field. For example, if the range is X,



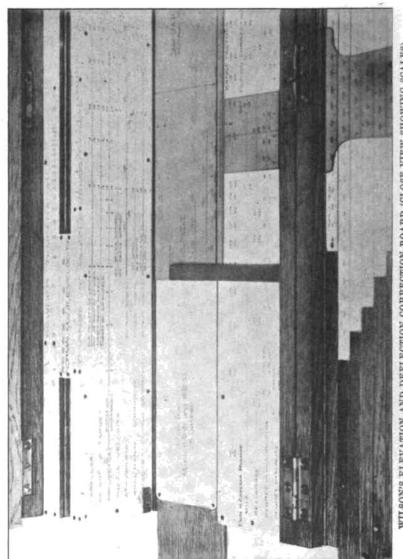
WILSON'S ELEVATION AND DEFLECTION CORRECTION BOARD (CASE CLOSED).



WILSON'S ELEVATION AND DEFLECTION CORRECTION BOARD (CASE OPEN FOR SERVICE).



WILSON'S ELEVATION AND DEFLECTION CORRECTION BOARD (CLOSE VIEW SHOWING SCALES).



WILSON'S ELEVATION AND DEPLECTION CORRECTION BOARD (CLOSE VIEW. SHOWING SCALES).

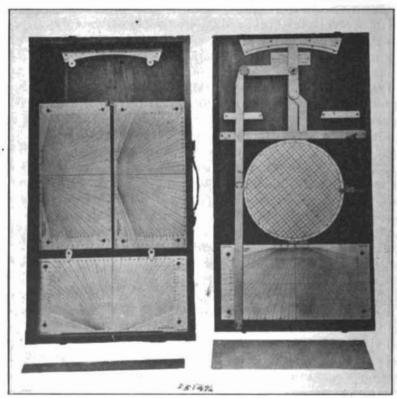
the corrected range Y, and the center of impact of the group of shots is at a point whose range is Z, assuming the wind, atmosphere, and projectile weight factors to be correct, one may work back to determine the actual powder velocity.

592. For the correlation of the observations of the terrestrial observers the deviation board, plate 476, is the best device. This board was devised by Col. Pirie in France and later modified and simplified to two sheets of paper and a triangle or T square, plate 477. The board is an adaptation of the French system, which is as follows: A sheet of paper is stretched over a plate of zinc and the point T, target, is located about in the center, figure 1, plate 478. The positions of the three observers, O_1 , O_2 , and O_3 , are then located accurately, either on or off the board, usually off. With these points as centers, two arcs are drawn for each. A line through O, and T locates zero for that observer; the arcs are graduated on each side of zero; so also for O. and O_3 . When the observers at these three points observe a burst it is plotted as shown; e.g., O, reports the burst 5 mile to the right; a line is drawn through the 5-mil points on the two arcs whose center is $O_{\mathbf{z}}$. Similar lines are drawn for O_1 and O_2 , according to their reports. The burst is supposed to be in the center of the resultant triangle.

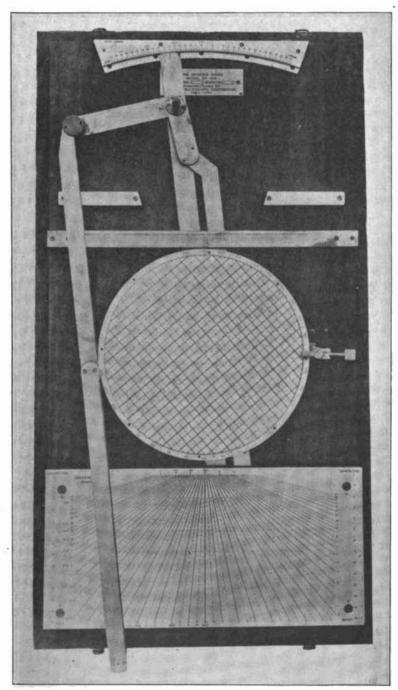
593. In the French Army the aerial observer uses a photograph of the region on which the target is located; this photograph is carefully ruled in checker-board fashion. The observer locates the burst on his photograph and reports the distance to the right, left, over, or under. The battery commander plots these reports on a sheet ruled as in figure 2, plate 478. It will be noted that the up and down lines are convergent; they pass through the battery position. It will be noted also that these lines are labeled both in yards and in angular units for the quick translation of the observations. The horizontal lines are likewise labeled in terms of distances and angles. It may be well to mention here that one car of the standard A. E. F. design, plate 479, was fitted to serve as a fire-control car. Plans were made to supply these cars for service in France, but on advice from France that they were not desired the plan was abandoned.

181768-21-42

PLATE 476

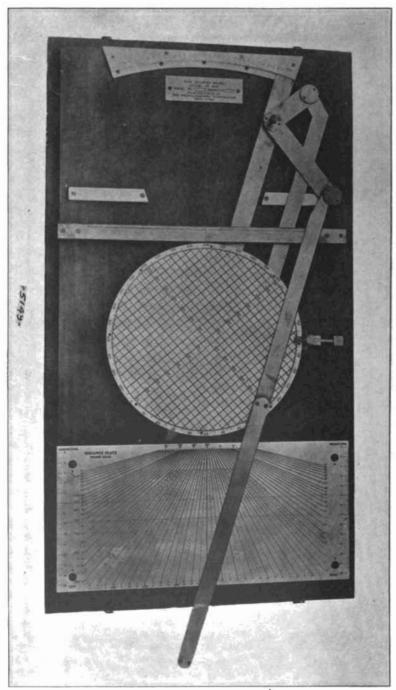


PIRIE DEVIATION BOARD.



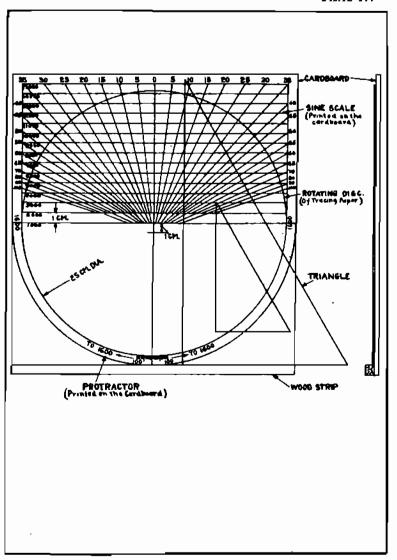
PIRIE DEVIATION BOARD.

PLATE 476B

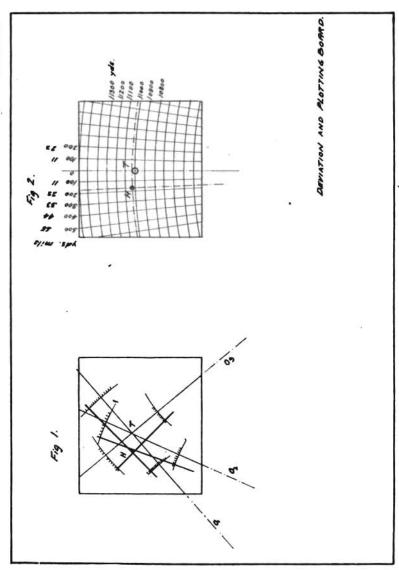


PIRIE DEVIATION BOARD.

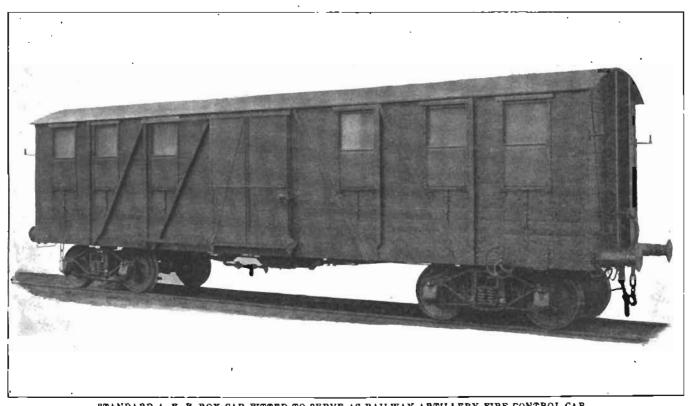
PLATE 477



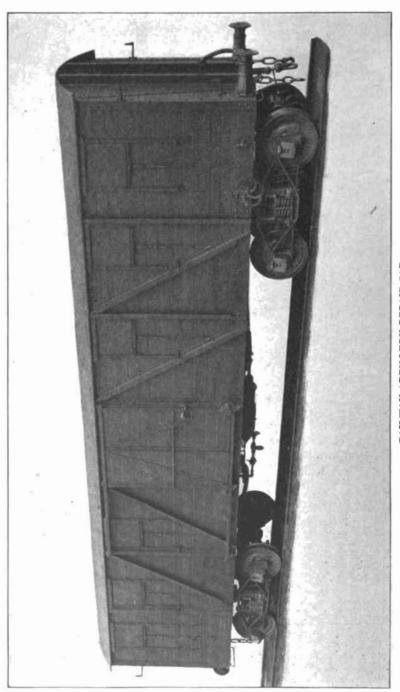
UNKLE'S SIMPLIFIED DEVIATION BOARD.



SIMPLE DEVIATION AND PLOTTING BOARDS.



STANDARD A. E. P. BOX CAR FITTED TO SERVE AS RAILWAY ARTILLERY FIRE CONTROL CAR.



RAILWAY ARTILLERY REPAIR CAR.

SECTION 7.

ASSEMBLY, DISPOSITION, AND MAINTENANCE OF RAILWAY ARTILLERY IN LAND WARFARE.

594. It is intended to treat here the general problems of the care of matériel that come up in connection with railway artillery. These will be treated under the headings of assembly, disposition, and maintenance.

595. ASSEMBLY.—Ordinarily, railway artillery is shipped on its own wheels, but in the case of the European war, all of that which came from England and America had to travel by water and was, of necessity, disassembled to a greater or less degree.

596. The experience of the English and of the American Navy indicates that such mounts should be disassembled as little as possible, and, in general, it was found possible to limit the subdivision to the following:

1 unit, gun and cradle.

1 unit, main girder and carriage.

1 unit, each span bolster.

1 unit, each truck.

On the very heavy mounts, it was necessary to make a separate load of the cradle. In all cases, also, the small and projecting parts were removed and packed separately.

597. The importance of providing heavy pieces such as the girders with proper lugs and rings for hoisting and handling, can not be too strongly emphasized. The designer often loses sight of this detail so valuable to the men who are charged with loading and unloading and assembling. As little work as possible should be left to be done at the assembly shop; in particular, drilling and riveting.

598. Particular care should be exercised in protecting bright exposed metal surfaces before shipping overseas. In many cases this was not done with guns and parts received in the present war, and considerable time was lost in cleaning.

599. A careful study was made of the erection of the American naval mounts and a summary of recommendations with reference to

equipment and personnel is given below. The equipment should include besides a full line of suitable hand tools:

- (a) At least two, and better, three or four parallel and adjacent tracks at least 700 feet long for unloading and erection.
- (b) Compressed-air plant and distribution system.
- (c) A locomotive crane of suitable capacity.
- (d) Overhead cranes of suitable capacity.
- (e) Three tool houses.
- (f) Field shop and office.
- (g) Office for Superintendent of Construction.
- (h) Barracks.

The personnel recommended for this work includes:

- (a) Commanding officer—major.
- (b) Construction officer—captain.
- (c) Adjutant, camp administration—lieutenant.
- (d) Accounting and purchasing officer—lieutenant.
- (e) 150 men, subdivided as follows:
 - 19 checkers.
 - 10 laborers, yard and camp.
 - 3 laborers, warehouse.
 - 1 chauffeur.
 - 3 office force.
 - 26 guards.
 - 2 tool keepers.
 - 3 orderlies.
 - 3 mess.
 - 1 latrine man.
 - 15 expert mechanics.
 - 58 railroad men—car and locomotive builders, track men, etc.
 - 3 extra men.

This arrangement was contemplated for the erection of a program of six months. With an actual organization about the same, a 14-inch mount was erected in 10 days.

600. DISPOSITION.—In the British Army, the railway artillery is classed as corps artillery and distributed as such. The plan followed in the American and French armies is the one which would be inferred from section 2, "The Scope of Utility of Railway Artillery," and section 5, "Procedure in Preparing for Action." This artillery is too valuable, too expensive, and too slow in building to be used except as necessity requires. It is felt that there is no merit in keeping the pieces located in various positions along the front on the theory that they would probably be needed in those localities.

Railway companies do not purchase a number of locomotive cranes and place them at short intervals along the line for chance emergencies. The cranes, as well as the railway artillery, are so mobile that they can be quickly transferred wherever needed, and, when not needed, are kept where they are both out of the way, well protected, and easily maintained. The British scheme of corps railway artillery is felt to have resulted in very poor economy in the utilization of this matériel.

601. In the case of the French and American Armies, a certain camp, about 30 miles behind the lines, was established for both the matériel and personnel of the railway artillery. In the yards of this camp were found the mounts and all rolling-stock equipment. At this distance behind the lines it is comparatively easy to maintain the personnel of the groups and not in any way to draw upon the facilities required to maintain the personnel at the immediate front. This camp was likewise on a well-established railway line and all supplies could easily be secured. This plan worked out well in both Armies.

602. Inspection.—Inspection of railway artillery is carried out in different ways by the different armies. In the French Army the inspection service is under the Commission A. L. V. F. (heavy railway artillery). Regular inspections are made at considerable intervals and routine notes are taken on condition of materiel. Upon the occurrence of any accident a member of the inspection service is at once sent for to render an opinion as to what should be done. Such records as were seen of the French guns were quite general in character.

603. In the British Army the inspection service is under the Ordnance Corps. It makes regular and special inspections, in the same manner as the French, but more frequently and in greater detail.

604. In the American Army the inspector was detailed from the Ordnance Department, but his line of authority was not clearly defined, and efforts were made to bring him under the authority, respectively, of the Railway Artillery Reserve (the operating branch), the Ordnance Repair Shop (the maintenance branch) and the Engineering Division of the Ordnance Department (the technical and designing branch). A final arrangement was never worked out.

605. As a result of observation and experience, however, it is felt that the inspector should, of necessity, be free from the authority of the artillery commander, whose use of the guns the inspector's work is expected to keep within proper bounds, and likewise free from that of the officer in charge of maintenance, whose work the inspections should constitute a check on.

606. It is felt that the arrangement employed in the French and British Armies, where the inspector is responsible solely to the Technical and Design Service, is the proper one. Inspections should be frequent and thorough and adequate records of each piece of matériel should be kept. As an illustration of what it is felt is required in this connection, an abbreviated copy of the Railway Mount Service Book, as made up for the use of the American Army, is given on the following pages.

607. Text and Outline of Railway Gun and Mount Service Record.

[Cover.]

RAILWAY GUN MOUNT SERVICE RECORD.

PREFACE.

Railway artillery is comparatively new to all armies, and especially so to the Army of the United States. In consequence, many difficulties have been experienced in the manufacture of railway artillery material, and considerable delay has been entaited by the necessary study of many unfamiliar details.

Similar difficulties and delays in the future can be minimized by studies based upon current experience. To make this study complete, it is necessary to check the theoretical knowledge of the designer by the practical experience of field personnel; to know whether the various parts function properly; and if not, why not.

While the records desired are more elaborate than those heretofore requested of battery commanders, the arrangement of the book is such as to make it a convenient means of recording the desired information. Ample spaces, under descriptive headings, are provided for information concerning practically every principal part of the carriage; difficulties experienced, observations, recommendations, and explanatory sketches.

Only the conscientious cooperation of the battery commander in furnishing complete data will enable the designers to produce the nearly perfect machine that the field personnel would like to have.

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Information in detail—											
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Forms of report of premature											

INSTRUCTIONS.

This book is always to remain with the mount, and is never to be removed except for the purpose of making entries, after which it is immediately to be returned to its proper place on the mount.

Entries.—The entries are to be made at least once every 24 hours, when the mount is in service, by the gun commander, under the supervision of the battery commander.

Record of assignment of mount.—The entries indicated on this page will be made immediately upon receipt of the mount.

Daily gun record.—In this section of the book, under the respective headings, there will be entered the number of shots fired, proportional weight of powder charges, type of shell, type of fuse, range, and elevation. In the column headed "Remarks," there will be entered short notes, such as a note of an inspector's visit, damage to gun or mount, nature of work the gun is used for (i. e., counterbattery, interdiction, or destruction), date sent to or received from the repair shop, date of transfer to another battery, and other short items with reference to any detailed entries on other pages.

Information in detail.—The table under this head indicates the desired information concerning each principal part or group of parts, but is not intended to limit the information furnished. This should be entered on the blank pages following the table and should include all available data as to poor functioning, weaknesses developed, wear noted, changes suggested, etc. Make these entries as soon as difficulties are experienced or defects noted. Sketches are of great value and should be a feature of such entries. Before an entry in this section the number of the page on which it is to appear should be entered in the index pertaining to the part or group concerned.

Reports of prematures.—These are to be made on the blank forms bound into the back of the book. They are to be rendered in accordance with the instructions printed thereon.

RECORD OF ASSIGNMENT OF MOUNT.

Date.	Gun cal ber.	i- Mode		uffea- on.	umber,	Battery.	Regiment.	Battery comm der.
	Gun:	<u> </u>			N RECOI	·		,
	Modifi	cation	•••••			•	: = .	
Date.	Number Full charge.	Reduced charge.	Size of powder charge.	Type of shell,	Type of fuse.	Range.	Eleva- tion.	Remarks.
,		! !			: !			

INFORMATION IN DETAIL.

On the pages following this table there will be entered full data concerning faulty functioning, weaknesses developed, undue wear, etc., with recommendations and explanatory sketches. The table indicates the nature of the desired information concerning the principal parts of groups, and will serve as an index to the entries. Make entries as soon as a fault becomes apparent, and index them in the designated spaces below.

	'		Inc	ex.	
Part or group.	Information concerning—	Page.	Page.	Page.	Page
Опл	Wear of bore, shifting of hoops, and all other in- formation concerning tube, hoops, or jecket. Give model, modification and number of gun,	 			
Breech mechanism	and date of entry. Condition of obturator, replacement of parts, wear action, etc. (live model, modification			,	
Firing mechanism	and number of the gun, and date of entry. Difficulties experienced, observations and sugges- tions. Ulve model, modification and number			I	
Cradle	(Slue date of antro	1		· · · · · · · ·	
	Difficulties, slowness, jamining, etc. Give date of entry.	ſ			
Traversing mechanism	targets, etc. Give date of entry.				l
Recoil	oil, etc.; case of silding mounts, action of recoil,				
Recuperators	troubles, suggestions, etc. Give date of entry. Operation, leakage, renewal of oil and air, troubles, etc. Give date of entry.	-		· · · · · ·	· · · · ·
Сагтіаде	Traversing rollers, trunnions, bearings, antifric- tion device, etc. Give date of entry.	i		1	
Sights	Give date of entry.				
Main girders and transoms Truck and frames Translating mechanism	Ali details of interest. Give date of entry All details of interest. Give date of entry Action and condition. Give date of entry				
Jacks					
BolstersBrakes	All details of interest. Give date of entry				
Outrigger	of entry, Rigidity of mount, rapidity of mount, rapidity				
Firing beamsLocding mechanism	of setting, bending, etc. Give date of entry. Details as to wear, etc. Give date of entry. Rapidity, ease of handling, and suggested im-	-	 		
Power unit	provements. Give date of entry. Reliability, power, and other points of note.				
Rnis	Give date of entry. All details of interest. Give date of entry				
Transbordeur	anife:	l			
A mmunition car	Give date of entry.	l			
Ground platforms	date of entry.				
Narrow-gauge equipment	ments, etc. (live date of entry.				
Other cars	All details of interest. Give date of entry				

[Faint ruled, both aides, with horozontal and vertical lines 5 millimeters apart, for entry of information in detail, 81 pages.]

MORTARS, 37-MM. CALIBER AND ABOVE.
Organization
Gun, howitzer, or mortar
Date of premature
fire Rounds per min. formins. before accident. Did projectile
burst inside or outside the bore? Distance from muzzle
Color of smoke observed: Black Gray White
TYPES AND MARKINGS OF AMMUNITION.
Taken from round fired, or next of same lot?
Fuse: Type Model Shape head
Color head Color body Lot No
Projectile: Type Model Color ogive Color
body Stamped markings Lot No
Cartridge case: Stamped markings Lot No
Propellant: Type
Weight
Normal
Reduced Zone No
Bag markings.
EXAMINATION OF PRAGMENTS OF PROJECTILE AND PUSE.
Did explosive adhere to fragments? How?
Edges: Sharp, square, or melted? Smoke blackened or heat blued?
Fragments: Large or small? Where found?
Remarks:
[Pages 137 to 144 will be duplicates of this copy, but will not bear folio No.; they will be perforated inch from the hinge.]
INSTRUCTIONS.
Original and two carbon copies of this report will be made by the battery commander as soon as practicable after the premature occurs, and will be sent direct to the Chief Ordnance Officer of the Army. Details concerning abnormal or short rounds should be noted under "Remarks". (Signed)
Battery Commander.
808 MAINTENANCE -The discussion of reilyer artillary must of

608. MAINTENANCE.—The discussion of railway artillery must, of necessity, be very incomplete, but an effort will be made to enumerate the chief matters which have come to the writer's attention in connection with it. First, cannon and then mounts will be considered and the types of wear and breakage and the methods of repair will be

discussed. Then shop equipment and organization for taking care of maintenance will be set forth.

- 609. CANNON.—The chief difficulties requiring maintenance in connection with cannon are derangement of breech and firing mechanisms, coppering of bore; bursting and swelling of tubes, and wear. The derangements of breech and firing mechanisms are merely small mechanical difficulties, the caring for which requires only a supply of spare parts and small size machine-tool equipment.
- 610. Coppering of the bore from rotating bands is a very serious difficulty. On the 14-inch Navy guns, after about 200 shots, this deposit of copper had reduced the range 5,000 yards. A most satisfactory method of remedying and of preventing this coppering, has been devised and used successfully in the French Army. This consists in introducing into the powder chamber a tin-lead alloy, which melts on firing and combines with the copper on the gun to form a brass, which no longer adheres as before to the interior of the bore. This process may be carried out best by attaching the alloy to the base of the projectile, by dipping, spraying with a metalizing pistol, or soldering on a disk of the metal. The introduction of foil of alloy into the powder bags appears to be satisfactory for small calibers, but does not give satisfactory results in large calibers.
- 611. Bursting and swelling of the tube are due to premature explosions of H. E. shells. French records show that such accidents occurred on an average of once in every 32,000 rounds with the 75's and once in every 14,200 rounds with the 155 Filloux guns. Such guns are usually discarded, but a process devised by Col. Canonica, of the Italian Army, is in use in Italy for reclaiming such material. This process consists of selecting two ruptured guns, in which the break is at different ends, cutting them in two and screwing the two good halves together. The threads are obtained by turning down the end of one part and boring out that of the other, each for about half the thickness of the metal and for 8 inches of length. Threads are cut very carefully so that the rifling matches when the two pieces are screwed home. Finally a ring is shrunk on outside the junction. This scheme has been used successfully on a considerable number of 149-millimeter cannon.
- 612. Wear, however, is the great and important problem in the maintenance of cannon. Care in cleaning of projectiles, faithful use of anticoppering methods, etc., may assist, but every gun will sooner or later wear so much that its range and accuracy are reduced below the economical limit. This wear occurs at the breech and muzzle ends principally, and consists in a gradual eating away of the rifling. At the breech end, this occurs more or less evenly around the circumference and is thought to be due to the intense heat of the burning powder gases which are projected against the forcing cone, as they follow the projectile. This wear causes the so-called "advance of the

forcing cone," i. e., the projectile must be pushed further and further toward the muzzle before it will seat properly in the rifling. The result is an enlargement of the powder chamber, a change in the density of loading, and a corresponding change and uncertainty as to muzzle velocity. The use of rifled projectiles, previously described, is designed to eliminate the necessity for a forcing cone, to allow a powder chamber the same size as the bore, and so to eliminate as much as possible of this wear. At the muzzle end, the wear is confined almost entirely to the rear edge of the lands, the edge which does not press against the rotating band. It is thought to be due to the mechanical erosion of the very high velocity gases which leak through the small orifice. This wear destroys the rifling progressively from the muzzle back to the breech and results in greater and greater dispersion of the shots.

613. The life of guns is given in a number of instances in the tabulated information of section 10. The figures there given for French guns in Volume II are from actual experience. From this experience the following formula for determining the life of large caliber guns has been developed:

Life in rounds
$$= \frac{2.5 \times 10^7}{V^2 \times D \times (D-2) P^{1.7}}$$

where V = muzzle velocity in feet per second divided by 1,000.

D = caliber in inches.

P = maximum powder pressure in long tons per square inch. The guns from which this formula was derived are nearly all very old models, and few, if any, had the advantage of the sort of care in firing that has now been discovered to be advisable. It is felt from isolated instances which have been compared with this formula, that a large gun operated with cleaned projectiles, and proper decoppering methods, should have a life at least 50 per cent in excess of that indicated by the above formula.

- 614. The methods available for the repair of worn-out guns are:
 - (a) Rechambering.
 - (b) Reboring.
 - (c) Relining.
 - (d) Retubing.

Rechambering consists of machining out the forward end of the powder chamber until the eroded metal is removed and a new forcing cone is formed. The piece is then supplied with a large powder charge, so arranged as to give the same muzzle velocity, and a considerable additional life, perhaps 40 per cent, may be obtained. This method is applicable only to guns, as they wear out at the breech end first, while howitzers wear about evenly at breech and muzzle ends. The advantages of this method are the simplicity with which it can be carried out and the very good results obtained. The

disadvantages are the fact that it adds only fractionally to the life of the gun, that it is inapplicable to short pieces, and that it requires a special powder charge for such guns as are repaired by it.

- 615. Reboring consists of turning out the entire interior of the bore to a large diameter and rerifling. This necessitates the use of a different caliber of ammunition, and of a lower powder pressure and muzzle velocity, reducing the range, in some cases, materially. The life should be almost as many rounds at the new caliber as at the old. The advantages of this method are that no forging equipment or shrinking arrangements are necessary, and that the life of the gun is doubled. The disadvantages are the reduction in range and the necessity for using a different caliber of ammunition.
- 616. Relining consists of turning out the interior of the bore to a larger diameter and inserting a liner, in which the rifling of the original caliber is cut. This liner is usually inserted by shrinking the gun over it, but the method of autofrettage or expanding the liner into the gun by hydraulic pressure is also being developed. This method is probably inapplicable to small calibers on account of the thinness of the liner that would have to be used. The advantages of this method are that it requires a fairly light forging and that it gives a gun practically as good as new and using the same ammunition as the old one. The disadvantages are the forging facilities required, the length of the process, estimated as nearly 900 hours on the United States 12-inch gun, and the fact that there is considerable doubt about the possibility of rechambering relined guns.
- 617. Retubing consists of disassembling the gun and building it up again around a new tube, just as it was built up at first. This, of course, gives a gun in every way as good as new. The disadvantages are, of course, the great amount of forging and shrinking equipment required, and the length of the process.
- 618. Mounts.—Wear and tear on railway mounts are of the same character as take place on railway rolling stock and seacoast gun carriages. Breakages and derangements are of a purely mechanical character, and generally of fairly minor magnitude. Repairs require, principally, a well-equipped machine shop, and no detailed discussion of them is called for.
- 619. ORGANIZATION AND ARRANGEMENTS FOR MAINTENANCE.—In the British Army the maintenance shops for railway artillery were under the command of the ordnance officer at the base at Calais. In the French Army they were under the chief inspector of artillery, for fairly light repairs. Major repairs were made at the works of the Schneider and other private corporations. In the American Army the exact arrangement was never finally fixed, but to all intents and purposes, the repair shops for railway artillery were under the commanding general of the railway artillery reserve. It is felt, as a result of observations of the workings of these various systems, that

the shops should be directly under the control of the engineering division of the office of the chief ordnance officer. They should not, of course, be under the inspection service, but should be coordinate with it and under the same authority.

- 620. In the French Army most of the enlisted personnel required for the operation of the shops was assigned permanently and was not drawn from the various groups of artillery stationed near them. There were about 80 workmen permanently attached to the shops. These, with the four artificers attached to each battery, are easily able to handle the maintenance of not only all of the railway artillery of the French Army but likewise of a great amount of field artillery.
- 621. One feature which strikes one most forcibly in both the French and British repair shops is the evident skill of all the men. One does not see in any American shop the type of men used in these shops. The captains found in charge of all the shops were of the type of the highest caliber shop manager in America. These men are not only men of a great deal of shop experience, but high-grade graduate engineers. It is estimated that their average age is about 45 years. The use of such men as these in these positions is in the highest degree necessary.
- 622. LOCATION AND EQUIPMENT OF SHOPS.—The scheme of disposition of inactive artillery just discussed makes the problem of maintenance a very easy one to solve in a very satisfactory fashion. In the yards of the camp where the railway artillery is mobilized, shops of the desired degree of permanency are built and equipped to handle all except the serious and most extensive of the maintenance work. Cars damaged very seriously by shell fire, or guns which must be relined or retubed must of course be sent back to the manufacturer or to the biggest base shop. In the French camp, the shops are well built brick structures of the type that one ordinarily finds used for medium heavy manufacturing. In the American camp the shop was similarly constructed, but was a steel frame building covered with corrugated iron.
 - 623. The equipment of the French shops is about as follows:
 - 2 24-inch lathes with 10-foot bed.
 - 8 smaller lathes, about 12 by 72 inches.
 - 2 horizontal milling machines.
 - 4 shapers.
 - 1 high-pressure air compressor for filling recuperator air hottles.
 - 1 vertical boring mill.

Oxyacetylene welding and cutting outfits.

3 large forges.

Portable forges.

1 drop hammer.

- 1 portable air compressor for use with air tools.
- 1 circular saw.
- 2 band saws.
- 1 50-ton shop crane.
- A good vise and bench for every man in the shop.
- 624. The equipment of the American shop was about as follows:
 - 8 lathes, 8 by 12 inch swing.
 - 1 lathe, watchmaker's.
 - 6 grinders.
 - 2 shapers.
 - 5 drill presses, up to 20-inch radius.
 - 3 screw machines.
 - 1 planer, 8 to 12 foot bed.
 - 1 power hacksaw.
 - 1 power cold saw.
 - 2 band saws.
 - 1 Landis bolt machine.
 - 2 300-foot air compressors.
 - 1 welding and cutting outfit.
 - 2 10-ton bridge cranes.
- 625. Experience with the American shop leads to the recommendation, slightly modified from that submitted by the commanding officer of the shop (38), that an equipment about as follows is necessary:
 - 10 lathes, sizes from toolmaker's to 26-inch by 16-foot.
 - 2 turret lathes.
 - 1 planer, 48-inch by 16-foot.
 - 2 shapers.
 - 7 grinders, tool, cylinder and surface.
 - 5 drill presses, 5-foot to high speed.
 - 4 power saws, hack, cold and wood.
 - 2 milling machines.
 - 1 power hammer, 6-inch stroke.
 - 1 heavy straightening press.
 - 1 planer and joiner.
 - 1 boring and mortising machine.
 - 1 48-inch wood lathe.
 - 1 brass cupola.
 - 4 oxyacetylene cutting and welding outfits.
 - 1 air compressor, 300 cubic feet, air tools.
 - 1 150-ton bridge crane with 10-ton auxiliary.
 - 1 10-ton high-speed crane.
 - 1 150-ton locomotive crane.
 - 1 15-ton locomotive crane.
 - 1 4-foot bulldozer.
 - 1 screw punch, 1-inch hole in 1-inch plate.
 - 2 jib cranes, 21 tons capacity.

- 626. With all these facilities provided, it has been found unnecessary to carry more than a few tools to the front with the mounts, i. e., anvil, portable forge, oxyacetylene outfit, hammers, chisels, brace and bits, drills, files, etc. No special repair car is employed in either the British or French armies, and neither organizations felt it to be advisable. A standard A. E. F. box car was fitted to serve as a repair car, plate 501, but the plan to provide them for service in France was abandoned. One was used to good advantage at the proving ground.
- 627. In the same way, practically all spare parts are carried at the shops in the main railway artillery camp or camps. The only spare parts carried with the mounts are for the firing mechanism, some bolts, screws, and miscellaneous stock. Such a car would be wasted unless the alterations or provisions made in it to carry spare parts would not interfere seriously with its use for something else. It surely would not be used to carry spare parts.

DUTIES OF THE RAILWAY ARTILLERY ORDNANCE OFFICER.

628. Although the following material, which was prepared by the writer, is given in another publication as noted above, it seems wise to give it here also in order that all material that has any reference to railway artillery may be contained in these two volumes. The following paragraphs will repeat information already given, but are included herein without modification just as they are given in the Ordnance Field Service Manual.

[Exact copy of Chapter X of Ordnance Field Service Manual (39).]

DUTIES OF THE RAILWAY ARTILLERY ORDNANCE OFFICER.

- 629. "Before proceeding with an enumeration of the duties of an ordnance officer of railway artillery, a brief explanation will be given of the organization and functions of what may be termed a "Railway Artillery Reserve," as it is at present understood.
- 630. Railway artillery in combatant service is quite analogous to the wrecking service of any railway organization. By this it is meant that although it is a definite part of the combatant organization as a whole, it is not a part and is not under the jurisdiction of the organization of any one army. The term "reserve" is used to imply that it is a branch of artillery not in use in daily routine service on the front, but is held in reserve at a central point for that peculiar and special type of work for which it has been designed and is peculiarly fitted. The point at which this artillery is held in reserve is known as the "Camp of the Railway Artillery Reserve," and may be considered to a certain extent in the light of a permanent camp. This camp accommodates during all of the time that it is not in active service not only the artillery itself, but the entire artillery personnel.

It includes, likewise, the heavy semipermanent railway artillery repair shop, general equipment, ammunition and spare parts depots, and a proving ground for the calibration of ammunition and proving of guns. The ammunition used by this artillery is not used by any other type of artillery, and it requires, in general, special facilities to handle it.

- 631. From the above brief explanation, it will be seen that the functions of the railway artillery ordnance officer are, as far as they concern the general equipment depots, quite analogous to those of a camp ordnance officer. The functions, with reference to the administration of an ammunition and spare part depot, ammunition inspection service, and artillery inspection service, are analogous to the functions of the Army ordnance officer. The functions with reference to the artillery maintenance service are peculiar to this type of service.
- 632. The railway artillery ordnance officer will be qualified as an adviser on all technical ordnance matters, including the effects of the various calibers and types of artillery for any specified work. under the supervision of the proper staff sections, he is responsible for the efficient service of ordnance supply and maintenance, including inspection and repair work in the Railway Reserve, and supervises and coordinates this work. He exercises general supervision and control of all ordnance supply, repair, inspection and maintenance work, and facilities within the Railway Artillery Reserve in so far as technical matters are concerned, and is in direct control of supply. repair, inspection, and maintenance of the artillery. He makes, or causes to be made, such inspection of ordnance materiel and repair and maintenance facilities as he may consider necessary and permits no alterations in ordnance equipment without the authority of the chief ordnance officer, excepting in emergencies. He causes periodic inspection to be made of all storage facilities under his jurisdiction and sees that proper practice is observed in storage, particularly that ammunition is properly cared for and maintained, and that the necessary technical information is available.
- 633. He maintains such records as enable him to keep the commanding officer of the Railway Artillery Reserve fully informed as to the condition and sufficiency of ordnance matériel, all repair and maintenance facilities under his jurisdiction, and the condition of all ammunition. He makes such technical reports and keeps such records as are required of him by the commanding general of the Railway Artillery Reserve, by the chief ordnance officer, and by higher authorities. He is authorized to correspond directly with the chief ordnance officer on questions in which the policy of the Railway Artillery Reserve is not involved. He causes to be carried out such

technical instructions for repair, maintenance, and alteration of ordnance matériel as may be prescribed by the chief ordnance officer.

634. There are assigned to the railway artillery ordnance officer as assistants the following officers with their necessary commissioned and enlisted assistants for the operation of the services mentioned: Supply officer and artillery armament officer. The accompanying table shows the organization of railway artillery center for approximately 300 guns:

Ordnance personnel for railway artillery center for approximately 300 guns.

	1	2	3	4	5	6	7	8	9		
_			Supply warehouses.					Armament.			
1	Units.	Office of R.A.O.O.	Ad- minis- trative office, 2.	Gen- eral sup- plies, 2.	Artil- lery and parts, 2.	Am- muni- tion, 3.	Inspec-	Main- te- nance Table Ex- hibit 1.	Totals.		
2 3 4 5 4	Colonels. Lieutanant colonels. Majors. Captains. Pirst lieutenants.	● d 2	•c 1	41			*6 2 3	1 1 2	1 2 3 7		
7	Second lieutenants	. <u></u>	- 1 2	2	1	1 2	•/3	- 2 - B	24		
9 10 11 12 13	Ordnance sergeants, Sergeants, first class Sergeants Corporals Cooks	*h 1 */1	2 6 3	2 1 2 4 1	1 1 2 4 1	2 2 4 10 2	*/5 */3 42	25 81 2	22 5 42 58 6		
14 15	Privates, first class Privates.		4	· 20	10	10 50	42	48 16	100		
16	Total enlisted		17	35	24	80	16	131	307		
17 18 19 20 21	Aggregate	8	10	37	25	82	23	137	7 33 1		

REFERENCES FOR PRECEDING TABLE.

- a 1 artillery armament officer, 1 supply officer.
 b I artillery inspector, 1 ammunition inspector.
 c Administration assistant.
 d I field inspector, 1 proof officer, 1 assistant to armament officer.
 In charge of sections.
 Technically trained assistant.

- o Clerks.
 L'Chio! clerk.
- (Stenographer.

 J Permanent personnel, clerks.
- Headquarters section and two plateens of an ordnance depot company.
 Two plateens of an ordnance ammunition company. Table 242.
 To be armed with rifles or pistols only when deemed necessary by commanding officers.
- 635. The administrative assistant in the office of the railway artillery ordnance officer is a captain. He is charged with the duties of maintaining the records of the entire ordnance personnel, both commissioned and enlisted, and with the proper keeping of office

records. He is authorized to make all emergency purchases, being appointed an agent officer for this purpose.

636. The supply branch is in charge of a lieutenant colonel, who is the supply officer of the Railway Artillery Reserve. He is charged with supplying equipment to troops and ammunition and spares for artillery. He requisitions for equipment, spares, and stock direct to the Chief of Ordnance of the Army if in the zone of the interior, or to the chief ordnance officer if in the theater of operations. He requisitions for equipment both regular and special in anticipation of demands to be made on his depot. He may requisition by telegraph when stores are urgently needed for the equipment of any troops, or the replacement of lost equipment, or for instruction purposes.

637. When an automatic supply of stores has been ordered in anticipation of the needs of the troops in the camp of the Railway Artillery Reserve, the supply officer keeps in touch with the supply

and requests its expedition when necessity arises.

638. Supply officers of the various organizations located at the camp of the Railway Artillery Reserve requisition for items of ordnance property needed by the troops of their units, these requisitions having the approval of the organization commanders. These requests will be sent directly to the railway ordnance officer.

639. The supply officer has commissioned assistants in charge of administrative, general supplies, artillery and artillery parts, and

ammunition sections.

640. The administrative assistant is charged with the account, and record work necessary in the office of the supply officer.

641. The officer in charge of the General Supply Section is charged with the receipt, storage, and issue of all ordnance stores except artillery and ammunition.

642. The officer in charge of the Artillery and Artillery Parts Section is charged with the receipt, storage, and issue of all material classed as railway artillery and spare parts thereof.

643. The officer in charge of the Ammunition Section is charged with the receipt, storage, and issue of all ammunition, including the

loading of the special ammunition cars.

644. The assistants to the supply officer shall maintain such records as are necessary to keep the supply officer informed as to the stock on hand, the receipt, issue, and probable needs of general supplies, artillery and artillery spares, and ammunition. Similar blanks specified for the ammunition parks of the Army are to be used by the Ammunition Section.

645. The artillery armament officer is responsible for the inspection, repair, and maintenance duties in so far as they pertain to artillery and ammunition used by and in charge of the Railway Artillery

Reserve. He maintains such records as enable him to keep the railway artillery ordnance officer informed at all times as to the condition of all artillery, its availability for service, the state of the guns as to wear, etc. He will be prepared to furnish the railway artillery ordnance officer all necessary technical information on ammunition. He is personally responsible for the field inspection of all artillery. He specifies what repairs are to be made in the railway artillery repair shop or in the field and passes on their satisfactory completion. He will make periodic inspections of all artillery in the artillery park, will be responsible for the condemnation of guns unserviceable from wear or accidental damage, and will see that all field organizations are instructed on the proper use and care of their material. He is likewise charged with the administration of maintenance facilities shops, etc., provided for such work as is hereinafter specified.

- 646. Inspection shall be made of all artillery at least eight or ten times during its normal life. This inspection will consist of a visual examination of the bores for coppering, pastilles, cracks, or other injuries, the operation of the elevating, traversing and breech mechanisms, and the accuracy of the sighting mechanisms; it will also include the questioning of the battery mechanics regarding the operation of the recoil systems and the length of time between the renewals of the recoil fluid and examination of the gun books.
- 647. A star gauge and a plug gauge record should be made at least two or three times during the life of the gun, and gutta percha impressions of any abnormal conditions, such as excessive wear, unnatural erosion or swells.
- 648. The artillery inspector will make a final inspection of all repairs made in the artillery repair shop and is responsible to the artillery armament officer that all field and shop repairs and maintenance are properly executed. He maintains such records with reference to the condition of each individual gun, carriage, etc., as enable him to inform the artillery armament officer of its exact status with reference to its availability for service, the remaining life of the gun, and of the characteristic field behavior of the gun and carriage. He will supervise the proving of guns and carriages, the firing of range tables, and the proving of improvised artillery accessories. He will investigate and report upon all accidents chargeable to defects in the artillery material. It is his responsibility to see that all technical investigation called for by the chief ordnance officer with reference to the behavior of the guns and carriages are properly carried out, and he shall maintain his routine records with such thoroughness and exactness as will assist to the maximum services responsible for the design of the material.
- 649. The artillery inspector will be provided with one closed car for field inspection service and one light repair truck for carrying of

inspection instruments. He will be provided with the following miscellaneous equipment:

Star gauges suitable for the various calibers of guns.

Plug gauges.

Bore sights.

Gutta percha impression outfits.

Alidade.

Planimeter.

Steel tapes.

Micrometers.

One complete set of drawing instruments, including Universal drawing instruments.

Flexible curve.

Complete set of Universal curves.

650. The ammunition inspector is responsible for the inspection of all ammunition, storage and handling facilities, and will see that safety instructions are complied with. He will make periodic examinations of the condition of ammunition both by visual inspection in the storage house and by trial on the proving ground. He is responsible for the furnishing of all technical information on ammunition, both to the troops and to the artillery armament officer. He will investigate and report upon all accidents that may be chargeable to ammunition, and will keep the artillery armament officer informed as to the behavior of ammunition and any defects discovered. He is responsible for the calibration of all ammunition as called for by the commanding officer, Railway Artillery Reserve. He is responsible for the collection, examination, and report on specimens of captured or unexploded enemy ammunition. He shall maintain such records as will be of maximum service to those organizations responsible for the design and manufacture of ammunition and he will conduct such investigations as may be called for by the chief ordnance officer. He will be provided with a full set of drawing equipment, Ideal drawing instruments, flexible curve and Universal curves and beam compass.

651. The railway artillery maintenance officer is in charge of the special railway repair shop and handles all necessary repairs and general maintenance on all artillery and motor vehicles. He supervises the making of all modifications in artillery as specified by the chief ordnance officer or required by field emergencies. He is responsible for the maintenance of such records as enable him to keep the artillery armament officer informed as to the condition and adequacy of all his facilities and the supply officer as to his needs for spare parts and raw materials. He is responsible for the making up of any necessary designs for emergency equipment or replacements. He shall maintain such records as will be of maximum assistance to

the various ordnance design services with reference to the performance of the various designs of mechanisms and the materials used therein.

652. Since the personnel of the railway artillery repair shop is responsible for the maintenance of all artillery, it is the duty of the maintenance officer to take under his charge the special mechanics assigned to each battery while the artillery organizations are in the park. These men will be used in the general maintenance service and will be given such training as will enable them to properly maintain their artillery in the field.

SECTION 8.

EQUIPMENT FOR RAILWAY ARTILLERY.

- 653. TABLES OF INITIAL EQUIPMENT.—It is not intended in the following to attempt to give definite rules for what should constitute total accessory equipment for railway artillery. Certain general recommendations will be made, however, which are based on French and British experience and observations by members of the Ordnance Department in France. It is probable that these will be of some value in the future (40).
- 654. A definite understanding was never reached between the Ordnance Department in France and the Ordnance Department in Washington with reference to the lists of equipment prepared in France for the American Railway Artillery. The Engineering Division of the Ordnance Department in France prepared lists which included primarily items of equipment in use by the French and British services, but which, due to different service conditions, were not familiar to the Ordnance Department in Washington. In addition, an attempt was made to complete the lists as nearly as possible from the information received from Washington on drawings, tables of equipment, etc. Only incomplete information had been received at the time, however, with reference to the requirements for the 8-inch gun and 12-inch mortar, for which the tables were being made. The lists were consequently not considered complete, but were nevertheless forwarded to Washington. It seems that this procedure led to some misunderstanding; e.g., items which had been left out for the lack of sufficient information were, when the lists were gone over in Washington, assumed as not wanted. It was hoped that, by combining the ideas of requirements as contained in the lists prepared in France, and the requirements necessitated by the particular type of mount worked up in Washington, at least sufficient equipment would be provided. The lists as they were prepared in France covered only the initial battery equipment, to a large extent based on the equipment carried by the French batteries.
- 655. DEPOT AND AUTOMATIC SUPPLY.—Neither the experience of the French nor the British service was sufficiently extensive to enable one to establish figures with reference to depot supply and

automatic supply. For this reason, and in order that an ample initial supply might be furnished, the arbitrary amount of one complete battery equipment for each three batteries was requested for the initial depot supply. It was intended that after sufficient knowledge had been gained with reference to rate of consumption. certain items could be put on an automatic supply list. It was feared that an arbitrary assumption of figures for automatic supply would lead either to an excessive accumulation of certain articles, or to the supplying of insufficient quantities of other items. date no further knowledge has of course been gained on this subject. so it is impossible to give any figures covering either the number of parts to be kept on hand in a depot, or to be supplied automatically. A close study of each particular mount in the design office will lead to fairly reasonable assumptions for requirements of spare parts. In determining numbers of spare parts, it is certain that destruction of parts by shell fire need not be considered.

656. SPARE PARTS, TOOLS, AND ACCESSORIES CARRIED WITH THE BATTERY.—Assuming that the railway artillery is operated from one or more large camps or centers which are equipped to handle all repairs except relining or reboring of guns, and extensive rebuilding of damaged carriages, and assuming also that the radius of operation is such that for any medium repair work not necessitating the withdrawal of the mounts to the shop, they can be reached by a mobile repair truck within a reasonable time, it is evident that only a very limited supply of spare parts need be carried with the battery. It is also evident that only a limited number of ordinary repair tools would be required.

657. The system of operating railway artillery from one large center is well established and highly recommended. of handling medium repair work with repair trucks, while not tried out to any great extent in connection with railway artillery, nevertheless seems to have many advantages. First, as mentioned above, the quantity of repair tools and spares carried in the field with the mounts can be considerably reduced; second, the number of skilled mechanics can be limited to a great extent and utilized to much better advantage on repair trucks and in the repair shops than they would be if permanently assigned to a battery. The tables of organization for railway artillery provide 28 enlisted ordnance men per regiment of 24 guns. As railway artillery never operates in units of regiments, these men, if kept with the guns, must be divided between the six batteries. This of course results in an uneven distribution of skilled and unskilled men. If, instead, the men are kept at the shop which is provided with a sufficient number of repair trucks, supply trucks, good automobiles and motor eveles, it is obvious that any S. O. S. call from the front for repairs and spare parts can be answered by picked men for the particular kind of repairs required, and the best results obtained in the same or less time. It is thought that one repair truck per group of eight guns would be required on an active front. This discussion is largely on maintenance, but it is evident that the quantity of equipment which should be carried is a direct function of the scheme of maintenance employed. Assuming that the repair-truck scheme is adopted, the following recommendations for equipment to be carried in the field are made. As the equipment will of course vary with the type of mounts, the recommendations must be considered very general.

- 658. Tools and accessories recommended-
- A, Tools and material required to make emergency track repairs:
 - 1. Standard track tools.
 - 2. A few pieces of rail, bolts, spikes, and fishplates.
 - 3. A few standard ties.
- B. Tools and accessories for operating train:
 - 1. Lantern, lamps, flags, etc.
 - 2. Car pusher and replacer.
- C. Tools, accessories, and material for emplacement.

This will, of course, vary with the different types of mounts and can very easily be determined. The material and items constituting platforms, outriggers, etc., should be ample in regard to spares if easily broken or damaged.

D. Tools, accessories, and parts for gun and breech.

In determining the spare parts to be carried with the gun in the field, it should be kept in mind that only such parts as can be easily replaced should be considered; as, for instance, firing mechanism and firing pins, a few extra bolts and nuts, washers, packing, springs, cotterpins, etc. It should also be kept in mind that, besides adding to the weight which is hauled around unnecessarily, a good deal of time is consumed in taking care of parts which seldom will be required, and could better be cared for in the depot.

E. Tools, accessories, and spare parts for carriage and mount.

The statement made under D applies to this section. Such articles as journal bearings, brake shoes, air-brake hose, brake pins, and cotter pins should be carried in small quantities. It does not seem necessary to carry spare couplers and buffers, however, it may be advisable to carry a limited number of emergency knuckles.

F. Jacks, cordage, blocks, etc.

Only such jacks should be carried as demanded by anticipated difficulties, as, for instance, the need of auxiliary jacks for raising the car for the 12-inch mortar. A good supply, about 200 feet per gun, of 11-inch rope and about 200 feet of 1-inch rope should be kept on hand, and two sets of double tackle blocks for 11-inch rope. One spare triplex block with chain of capacity used for loading cranes. Twine packing and whipping and tarred hemp yarn, 1-inch, should be carried in ample quantities.

G. Carpenters' tools:	Per battery.
Axe	I
Augurs—	
Screw, solid, wing-eyed, 14-inch	
Screw. golid. wing-eved. 1-inch)

G. Car	penters' tools—Continued.	
	Bits, twist	
	1-inch	1
	}-inch	1
	-inch	1
	1-inch	1
	Brace, ratchet, for bits	1
		1
	Chest, tool, carpenter's	1
	Chieel, wood—	
	14-inch	1
	1-inch	1
	}-inch	3
	Mortising	1
	Gouge, 1-inch	1
	Gouge, 1-inch	1
	Dividers, 8-inch	1
	Drift, steel, round, 4-inch.	1
	Gimlet—	
	}-inch	1
	t-inch.	1
	•	1
	Hammer, claw	1
	Augur, 10-inch	1
	Saw, croescut	1
	Hatchet, wood handled	1
	Mallet	1
	Oil stone, 4 by 2 by 8 inches	1
	Pencils, carpenter's	1
	Pinchers, pair	1
	Plane, jack	1
	Rasp, wood—	
	Flat	1
	Round)
		1
	Rules, folding, 6-foot	1
	Saw—	
	Hand, rip, 36-inch	1
	Hand, crosscut, 26-inch.	1
	Blade, 5-foot, with handles	1
	Square, combination, 8-inch blade	1
H. Ma	chinists' tools:	
	Chest, tool, machinists'	1
	Chisel—	
	Cape, steel	1
	Cold	1
	Dividers, spring nut, 6-inch, pair.	1
	Drill, breast, with chuck	1
	Drill, twist, straight shank. Morse original, for breast drill-	•
	inch	1
	• .	
	ra-inch	1
		1
	3 inch.	1
	} inch	J
	13-inch	1

H. Mach	ninista' tools—Continued.	
	Drill, ratchet	1
	Drills, for ratchet drill, twist	1
	1-inch	1
	{-inch	1
	}-inch	1
	1-inch	1
	Emery stick, fine	1
	Files—	-
	Flat bastard, 12-inch	1
	Round bastard, 12-inch	1
	Square bastard, 12-inch	1
	Flat, second cut, 10-inch.	1
	Round, smooth, 10-inch	1
	Square, smooth, 10-inch	1
	Taper, 8-inch	1
	Hammer, machinist, ball pein, 13 pounds	1
	Handles, file, assorted	12
	Jaws, copper, for bench vise, pair	1
	Oiler, machinist's, small	ī
	Pin, drift, 1} by 1 inch	i
	Punch, center	î
	Saw, hack, adjustable	2
	Saw, hack, 12-inch blades.	36
	Scale, steel, square combination.	1
	Vise, bench, about 4-inch jaw	ī
	Wrenches, monkey—	-
	6-inch	1
	12-inch.	î
	18-inch	1
1 Black	esmith's tools:	•
	Anvil, 100 pounds.	1
	Borax, pounds	i
	Chisel, hot, 2-inch blade	2
	Forge, portable, "Buffalo," 24 by 30 inches, with tank	1
	Hammer, blacksmith's, 13 pounds, with handle	1
	Hammer—	-
	Sledge, 10 pound, with handle	1
	Set, 14 pounds, with handle.	1
	Hardie, 2-inch blade, 1-inch handle	i
	Punchee, blacksmith's—	•
	f-inch.	1
	j-inch.	1
		1
,	Swages, pair— 	٠,
	1-inch	1
	1-inch	1
	1-inch.	
	Tongs, blacksmith's, pair—	1
	inch	1
	1-inch.	_
	1-inch.	I 1
	•	1
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J. Tinn	er's tools and supplies:	
	Acid, muriatic, pint	
	Sheet zinc, ounce	1
	Blow torch	
	Jron, coldering, with handle, pounds	
	Mallet trimmers	
	Sal ammoniac, lump, pounda	
	Snips, tinners'—	
	Large, pair	٠
	Small, pair	1
	Solder, soft, pounds	4
	Zinc, alloy, for brazing, pounds	4
K. Miss	cellaneous tools and accessories:	
	Buckets, water As required	d
	Cans	
	Emery wheel, hand	1
	Extinguisher, fire	Ė
	Machine spike, steel, 11-inch.	1
	Needles, sail	4
	Palms, sewing, leather.	1
	Wrench, Stillson pipe, 14-inch	1
T. Mine	rellaneous material for repair:	•
D. 10190	Bolts and nuts, assorted.	
	Round iron—	
	1-inch by 5-foot pieces	2
	A-inch by 5-foot pieces.	2
		2
		Ю
	, , ,	10 10
	Pins, cotter, assorted	H
	••	Ю
		i O
	• • •	0
	- ·	0
	• • •	·U
	Screws—	
	Machine, assorted.	
	Wood, assorted.	
	Steel angles, har, plates, etc., should be carried in small quantities and a	u
A. 102	required.	
M. F176	e-control equipment:	_
		2
		1
		2
	(2
		2
		2
		2
	-	2
		2
	y	1
		1
		1
		1
	Logarithmic tables in degrees and grads	2

M.	Fire-control equipment—Continued.	
	Drawing board 28 by 28 inches	2
	Alidade with level	ì
	Alidade with telescope	
	Straightedge ruler	2
	Triangles 60 degrees.	2
	Triangles 45 degrees	2
	Large board (28 by 28 inches) squared	1
	Zinc sheets, squared	1
	Drawing pencils, No. 3.	25
	Erasers, rubber	6
	Paper, drawing, rolls	6
	Tracing paper, rolls	6
	Red ink, bottles.	3
	India ink, bottles	3
	Theodolite	1
	Barometer, aneroid, metric	1
	Compace declinator	1
	Thermometer (Centigrade)	2
	Field glasses, prismatic, type E. E., Signal Corps	2
	Slide rule or omnimeter	2
	Sighting rod	_ 1
	Wooden stakes	6

SECTION 9.

SUMMARY OF RECOMMENDATIONS.

659. The following is a summary of the recommendations made in the previous pages in regard to railway artillery for the United States Army:

660. Guns.—It is recommended:

A. That the Railway Artillery Program include the following guns:

12-inch, 25-caliber howitzer. 16-inch, 25-caliber howitzer.

10-inch, 50-caliber gun.

14-inch, 50-caliber gun.

661. MOUNTS.—It is recommended:

- A. That the 12-inch howitzer be mounted either on the same carriage recommended for the 10-inch gun below or on a carriage of characteristics similar to those of the carriage already developed for the 12-inch, 20-caliber howitzer, plate 194.
- B. That the 16-inch howitzer be mounted on a combined sliding, rolling, and quick emplacing carriage, embodying the sliding recoil features of the 14-inch model E carriage, the rolling recoil features of the 16-inch model 1918 carriage, and the quick emplacing features of the 8-inch carriage (outrigger) and 280-millimeter German carriage (pedestal), if practicable, or the base ring of the 14-inch model E if the German pedestal is impracticable.
- C. That the 10-inch, 50-caliber gun be mounted similarly to the German 280-millimeter, but with modifications, plate 59, to allow firing from the wheels for limited fire and quick emplacement for wide-angle fire.
- D. That the 14-inch, 50-caliber gun be mounted on the same carriage recommended for the 16-inch howitzer above.
 - 662. EQUIPMENT.—It is recommended:
- A. That spare-parts cars be not furnished, and that equipment in general be supplied in accordance with the recommendations given in section 8.

663. Shops -Maintenance. - It is recommended:

A. That shops in every case be established at the railway artillery camp to handle maintenance of all such artillery. In the interest of hasty evacuation with minimum loss, should such evacuation become

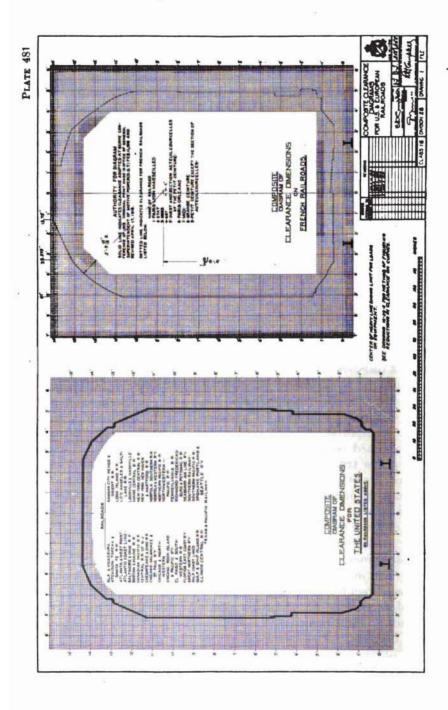
necessary, it is recommended that the shop be of the semiportable type.

- B. That shop equipment be provided in accordance with the recommendations of section 7.
- C. That special attention be given to the obtaining of officers of long experience and special ability in shop practice for the supervision and operation of these shops.
- D. That special attention be given to obtaining several officers and a number of men who are thoroughly familiar with the commercial railway companies' methods of maintaining standard rolling stock. Further, that some of these officers and men be retained for peacetime service. In the event that this is not possible, it is recommended that several C. A. C. officers and a number of men be detailed for a time to the maintenance service of some railroad company in order that they may become familiar with the difficulties experienced and the routine and emergency measures applied.

SECTION 10.

RAILWAY CLEARANCES AND TABLES OF CLASSIFIED INFORMATION.

- 664. RAILWAY CLEARANCES (41).—In order that the material contained in this report may be complete from the standpoint of all who are interested in any phase of railway artillery, it seems wise to include a discussion on railway clearances. The discussion given in the following paragraphs is based on a handbook on clearances, prepared in the Railway and Seacoast Carriage Section of the Ordnance Department, and with which the writer has had some connection. In the handbook referred to, individual maps and clearance diagrams are given for each of the roads listed on plate 481. A key map is given likewise of all those main lines represented by these roads and over which the railway artillery would be transported, east, west, north, and south, and along the coasts and borders, in the event of an emergency. There are too many individual maps and clearance diagrams to include in this work and it seems best to omit the key map, since this volume is for general distribution.
- 665. Composite Diagram for American Railways.—The composite clearance diagram of railways may be termed an outline or diagram of such shape and dimensions that when the transverse section of the various railway vehicles remain within its limits, these vehicles can be transported over all sections of the roads concerned with a predetermined clearance from obstructions, so long as the distance between the truck centers of these vehicles is kept within certain specified limits. Such a composite clearance diagram of railroads is perhaps an indefinite outline unless full explanation is given as to what it covers. The diagram shown on plate 481 covers all American railroads listed thereon. These roads include all coastal lines, Mexican border lines, some transcontinental lines, and a few central, north, and south lines.
- 666. The information from which the clearances were drawn was obtained direct from the chief engineer's office of each railroad. From this information a composite diagram was then drawn for individual railroads. These composites were then compiled into a master composite diagram. The clearance information obtained showed either actual obstructions or clearance limits with an allowance of 4 inches between the clearance line and actual obstructions. The composite clearance diagrams allow 4 inches clearance between actual obstructions and the outline.



- 667. The diagram makes no allowance for curves, but it is safe for equipment whose truck centers do not exceed 40 feet. On railway mounts whose trucks centers exceed this dimension, allowance must be made for the overhang of the mount in rounding curves. It is safe to figure a maximum curve of 17 degrees, 337 feet radius, on the main lines of railroads shown. Hence, the width of the mount will be reduced at least as much as the computed off-set on a 17-degree curve. A full discussion of railroad curves will be given later.
- 668. It was early recognized that to compile a clearance diagram of every railroad system in the country would be an endless and indeterminate task as well as being worthless when completed. The futility of attempting to establish such an absolute clearance diagram of every road is best illustrated by the following facts: There are over 250,000 miles of railroads in America. Some of these roads are inaccessible to any but the lightest railway equipment and are located in the interior mountainous regions. For instance, some standard gauge railroads are used only by the lumber interests. Special logging cars and locomotives comprise the rolling stock of these roads. Obviously no piece of railway artillery could ever be transported over such tracks. Such roads would therefore be useless for railway artillery shipments and have not been considered.
- 669. Other railroads, while using standard equipment, touch only the small central and western interior towns. These roads are generally branches of the larger systems and it is improbable that any emergency could ever arise for their use. If it did, the branches would have to be rebuilt. These roads are not considered on the diagram.
- 670. To compile a maximum clearance diagram of all the big railroad systems of the country would result in such limitation of dimensions of the railway mount that one could not use it for the design of the heavier caliber guns. The branch lines of some of these systems present limitations that sometimes interfere with their standard equipment, but the territory covered is so important that lighter rolling stock is used. Hence it would be unwise to limit the diagram by including all branch lines of the big systems. Some of the branch lines, however, are of vital importance and these have been included. If it is not possible to reach an important point from one line on account of some limiting feature, it has generally been found possible to detour to that point.
- 671. It must not be presumed from this discussion that railway clearances can be compiled into a fixed outline or diagram. The more progressive railroad companies are constantly changing their clearances and improving their curves. So to keep up to date, it is necessary to keep in touch with the railroad engineers. These changes should be checked up every six months and the diagrams changed if affected.

- 672. METHOD OF USING AMERICAN COMPOSITE DIAGRAM.—The master composite clearance diagram shown on plate 481 is complete for all the railroads listed thereon. As previously stated, the clearance outline shown is 4 inches within the actual obstruction line. using this diagram the matter given later under the headings of "Railroad curves," "Offset of middle ordinate," and "Elevation of outer rail on curves" must be carefully considered. In other words, the outline of the railway mount or equipment considered must not only come within the diagram, but if the truck centers are greater than 40 feet, allowance must be made for the three items just men-The method of computing these allowances is given under the proper heading, and these dimensions must be deducted from the clearance outline shown on this American clearance diagram. All of this is true only in the event that the truck center distance of the equipment is greater than 30 feet. It is impossible to state absolutely the degree of curvature of all lines covered by this diagram. It is a safe assumption to state that the maximum curve over any road on which railway mounts are liable to be run is approximately 17 degrees. The radius of this curve is 337 feet.
- 673. The middle ordinate or overhang at the center of equipment whose truck centers are 30 feet on the 17-degree curve is 4 inches, as determined by the formula given under paragraph 682 on middle ordinate of curves. It is readily seen that this offset enters into the calculations in determining the extreme width of the railway mount.
- 674. The elevation of the outer rail on curves does not present such limitation to the width of railway artillery as might be supposed, for the reason that the extreme width of railway artillery mounts at or near the maximum height is generally less than the clearance diagram. Since the elevation of the outer rail affects the width a perceptible amount only at its extreme height, it is evident that there is ample room between the outlines of the mount and the upper portion of the clearance diagram. The contour of the railway mount will, however, determine this feature.
- 675. On such equipment as the ammunition cars this elevation of the outer rail is of extreme importance, since the car has its extreme width at the height of the eaves of the roof.
- 676. COMPOSITE DIAGRAMS A AND B.—For ready reference in looking up limiting features of the American composite clearance diagram, diagrams A and B are given as covered on plates 503 and 504, respectively. The limiting features and the railroads on which these occur are shown on these diagrams together with actual dimensions above the rail. The two diagrams are, of course, covered by the master clearance diagram, and are only included for the detailed information which they contain. These two diagrams are to be

used in the same manner as the master composite diagram and the full line on each one indicates 4 inches actual clearance inside of the obstruction line.

677. French Railway Diagrams.—As the Ordnance Department was shipping railway mounts to France, it was vitally interested in the clearances of railroads in that country. Accordingly, information was secured which enabled the section to draw the French composite clearance diagram. This was placed on the same tracing as the American composite, for it was of vital interest. It is practically the same diagram as was being used by the officer of the Director General of Military Railways in designing railway equipment for use in France. This diagram was based on proceedings of the International Conference at Berne in the year 1913. No map was prepared for this European clearance diagram.

678. The railroads in France do not report exactly the same clearances as shown on the Berne conference diagram. It was, therefore, decided to split the European composite diagram in two (pl. 484). That part of the diagram on the left of the center line represents the "Passe-Partout" or Berne conference clearance diagram, and the part on the right of the center line represents a composite of nine French railroads. A table of clearance for European railways is given on plate 485.

679. CURVES—MIDDLE ORDINATE.—All of the American diagrams were worked out on the basis of having 4 inches between the clearance line and the actual obstruction. On straight-line tracks and on curves of large radii, this is sufficient for mounts whose truck centers do not exceed 40 feet. When the truck centers exceed this distance additional side clearance is necessary. The two components of the element of side clearance in rounding curves are the overhang of the mount and the elevation of the outer rail. Before taking up these two features, it may be profitable to fix in one's mind the meaning of the accepted manner of expressing the amount of curvature of a railroad track. Curves on a railroad are usually expressed in degrees and minutes. This degree in this country means the central angle subtended by a chord 100 feet long. Approximately 1 degree of curvature is equivalent to a radius of 5,730 feet. Thus:

$$5,730 \times 2 \times 3.1416 = 360 \times 100$$

 $36,001,7 = 36,000$

Hence, to obtain the radius of a curve in feet, divide 5,730 by the number of degrees of curvature.

680. In the metric system, instead of the chord being 100 feet, it is 20 meters or 65.61 feet. So with the central angle remaining the same, the radius will necessarily be less. This can be represented

by 65.61/100 for a 1 degree curve, or approximately # English measurement. Thus—

10 degree curves = $\frac{5730}{10}$ = 573 feet radius, American, fig. 1.

- 10 degree curves = $\frac{65.61}{100} \times \frac{5730}{10} = 375.9$ feet radius, French, figure 2, plate 487.
- 681. The middle ordinate distance must be subtracted from the width when it is sufficiently large to come within clearance limits. In other words, the diagrams allow clearance only for equipment having truck centers less than 30 feet, and when this is exceeded, the width of the mount must be decreased by the number of inches of overhang.
- 682. Overhand.—The overhang at the center of a car will be the same as the middle ordinate of the chord whose length is the distance between truck centers, figure 3, plate 487. This distance may be obtained by laying out the truck centers on a curve of given radius or from the approximate formula—

 $d = \frac{c^2}{8R}$ used, where R = radius to center of track c = truck center distanced = middle ordinate.

In the event that the mount is equipped with span bolsters an additional (d) will have to be figured, fig. 4, plate 487. Thus—

$$d = \frac{c^{2}}{8R}$$

$$d' = \frac{c'^{2}}{8R}$$

$$R' = R - d'$$

683. Super-Elevation.—The super-elevation of the outer rail on curves will, of course, decrease the clearance. The amount of this super-elevation is a function of the train speed and the degree of curvature. An empirical formula for finding the elevation which gives results sufficiently close is—

 $E = .000685S^2D$, where

E= Elevation of outer rail in inches.

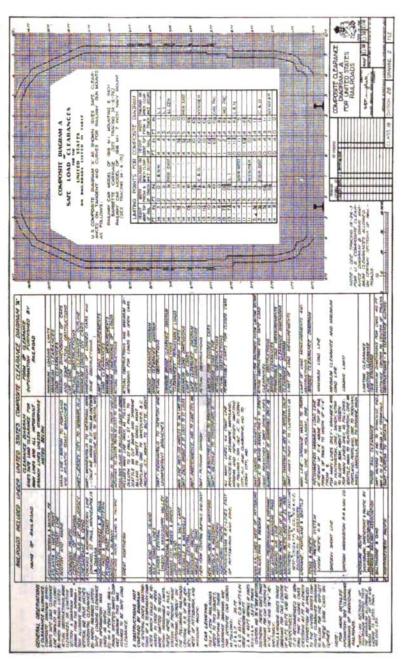
S =Speed in miles per hour.

D = Degrees of curvature.

Example for 10 degree curve.

 $E = .000685 \times 30^2 \times 10$ E = 6.165 inches.

(Taken from American Locomotive Co.'s Handbook.)



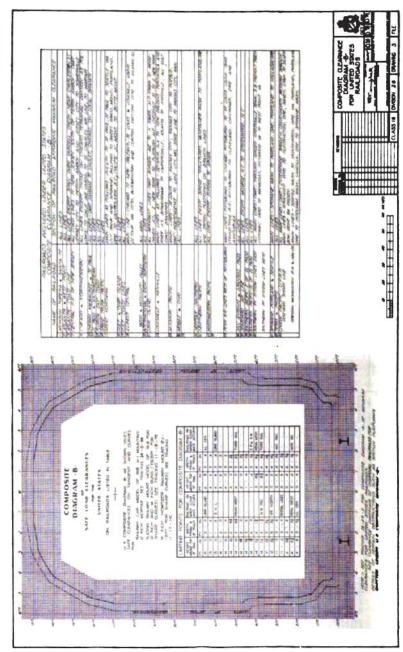
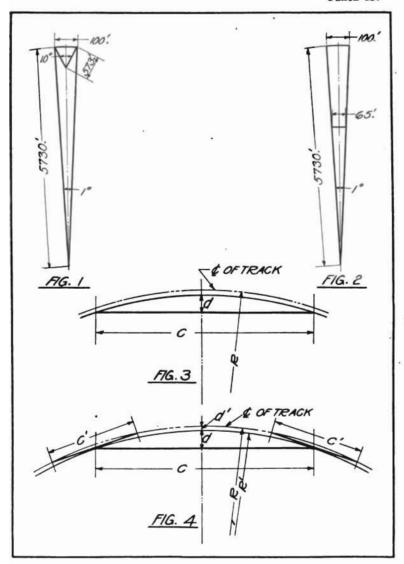


PLATE 484

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PLATE 487



RAILWAY CURVES.

684. SPREAD OF RAILS.—In 1910, the A. R. M. M. Association recommended the widening of the gauge of track at curves as follows:

Curves 8 degrees and less should be standard gauge. Gauge should be widened inch for each 2 degrees or fraction thereof over 8 degrees, to a maximum of 4 feet 91 inches for tracks of standard gauge. Gauge, including widening due to wear, should never exceed 4 feet 91 inches.

- 685. Weight.—The weight of the railway mount is just as important as clearance in determining where and how it may be transported. Each type of mount, of course, weighs differently, and no attempt has been made in this clearance data to state what weights can be handled over the lines shown.
- 686. Inquiries were instituted as to what loads American railroads could handle when the clearance data was being obtained. The majority of railroads reported that they could handle loads of 180,000 pounds safely. On weights above this amount, most of the answers were either negative or ambiguous. The railroads, therefore, indicate that no general statement will be made as to what load they can handle. It was necessary to take up each type of mount with the roads in question giving full information as to wheel loads, wheel bases, total length of equipment with an outline or silhouette of the mount. The route contemplated was also given. Only by this procedure can a definite statement be secured from the railroads.
- 687. The axle loads for all railway mounts for use in France were fixed under the direction of Gen. Pershing. This was a limit of 17 metric tons per axle or approximately 37,500 pounds. The M. C. B. Association standard capacity for an axle with 6 by 11-inch journals is 50,000 pounds. So the wheel loads on all railway mounts were comparatively low. This decision required the extremely heavy mounts to have many wheels. The 12-inch, 50-caliber American gun sliding railway mount has 32 wheels. The 10-inch French Schneider sliding railway mount has two trucks of 12 wheels each. From the foregoing, it will be noted that while the total weight of some of the mounts (the American 12-inch gun sliding mount weighs 600,000 pounds), is exceedingly high, the loads per wheel are low.
- 688. Those dimensions with which the Service would be concerned in routing railway artillery over the United States are given with the various existing railway mounts on the following data and profile sheets. In each case the transverse section given within the United States composite clearance diagram is a composite of the obstructions throughout the length of the car that figure in the clearance. In the event that the clearance of any particular mount over certain roads is found so close as to be doubtful, it will be best to look up the drawings of that particular mount in the handbook to determine just where the limiting features on the mount are located.
- 689. TABLES OF CLASSIFIED INFORMATION.—It was mentioned in the preface that at the request of the French and British Technical

Services, sections 3 and 10 were being divided and all descriptions and tabular data on French, British, and Italian mounts would be given in a second volume which would be available for official use only. The result is that less than one-third of the descriptive matter of section 3 and the tabular data of section 10 can be given in this volume. The American mounts on which data is given herein represent the highest points in the development of railway artillery so that an accurate conception of its present status can be gained. All of the data on the German mounts has been gained from study of captured handbooks and examination of the mounts themselves.

Table of classified data (42).

OUN.

			Total le	ngth.	 	Diameter ove	r powder	
No.	Caliber.	Model.	Dimen	sions.	Calibers.	chamber.		
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	
C. D. E. F. 44. B. C. D. 56. 66. B. 7. 8. 9. 10. 11. 12. 13. 14. 15. 15.	8-inchdo	1888, 1888 Mk. I and II U. S. N., Mk. II-1 U. S. N., Mk. IIII U. S. N., Mk. IIII U. S. N., Mk. IIII U. S. N., Mk. V 1919, Mk. I and II 1888, 1888 Mk. I and II U. S. N., Mk. I U. S. N., Mk. I U. S. N., Mk. I 1990, 1890 Mk. I 18905 U. S. N., Mk. I 18919 U. S. N., Mk. I 18919 U. S. N., Mk. I and II 18919 U. S. N., Mk. I and II 1919 U. S. N., Mk. IV do do do 1918 Mk. I do 1919 Mi	3. 8395 8. 2042 7. 0739 6. 4922 7. 7343 8. 7503 8. 7722 10. 4708 9. 3281 8. 3591 8. 3591 8. 3591 11. 2014 15. 4432 11. 2014 15. 4432 14. 7637 18. 1610 18. 1610 18. 1610 7. 8295 7. 8295 7. 8295 7. 8295	7n. 1111. 4 823 278. 6 225. 6 804. 5 344. 5 343. 23 357. 21 329. 1 141. 12 442. 6 441. 6 609. 6 581. 25 71.5 71.5 71.5 71.5 71.5 71.5 71.5 71.	22. 53 38. 6 32 30 35 40 42. 64 34 10 30 30 30 30 40 50 50 50 50 50 50 50 50 50 50 50 50 50	M. 0. 28448 . 7346 . 7812 . 781 . 781 . 781 . 781 . 781 . 8382 . 9779 . 9906 . 9906 . 9905 . 9452 1. 1303 1. 143 . 8376 1. 1607 1. 2192 1. 2192 1. 2192 1. 1292 1. 1165 1. 15748	7a. 29 29. 97 30. 75 30	

OUN - Continued.

No.	Diameter	of muzzle.	Total w	elght.	powder ch		Leng powder c	th of hamber.	Capaci powder ch	ty o(namber.
•••	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
nerican:	М.]n,	Kg.	Lb.	.w	In.			— м.і	In.
1,	0.1778	7	953	2, 100	0.12141	4, 78	0. 3632	14. 3	0.0041	25
2	. 2857	11.25	13,758	30 30N	. 4 , 24511	9.65	1. 2994	51, 159	, 0596	3,63
3.\	3516	14	14,623	32, 218	. 2413	9.5	1. 2954	51,	. 0592	3,61
B	. 3683	14.5			. 2413	9.5	1. 2875	50.69	. 0562	3, 4
C.,	.3175	12.5	13,344	29, 400	.2413	9.5	1, 2753	50, 21	0519	3.17
D	3048	12	11.892	26, 200	. 2413	9. 5	1, 2753	50, 21	. 0519	3,17
E	3556	14	19, 402	40, 544	. 2413	P. 5	1. 5588	61.366	. 0858	5, 24
F	.3748	14, 75	19,063	42,000	2794	11	1.3931	54, 85		-,-
4A	. 4267	16.8	30,502	67, 200	2997	11.8	1.6634	65.49	.0166	7. 1
8		10.0	00,002	27,200		710			10100	-, -
C										
D			••••				. ,			
5	. 5334	21	13,217	29, 120	.3175	12.5	. 5367	21.13	.0438	2.6
6.1	. 5334	2i !	52, 198	115,000	3608	14.2	1.9692	77, 53	. 1992	12.1
В	. 1826	19	wa, 100	110,000		47.	1.000			**, *
7	. 1020	15	80, 340	177,000	.3886	15.3	2.0657	81.33	2393	14.6
Ř.	. 5275	20, 77	18, 420	40, 582	3403	13.4	8469	33, 345	. 0784	4.7
9	. 6096	24. //	45, 728	144, 808	. 4287	16.8	2. 2457	88. 415	.3165	19, 3
ΙΔ	.5943	23.4	81, 702	180,000 :	. 4191	16.5	2. 2457	88. 4L5	.3203	19.5
10	. 5943	23.4	81,702	180,000	4191	16.5	2,2457	88.445	. 3203	19.5
12			81, 702							
13	. 5943 . 5943	23.4		180,000	. 4191	16.5	2. 2457	88.415	. 8203 . 3203	19, 5
	. 7035	23.4	81,702	180,000	. 4191		2. 2457	88, 415		19,5
14		27.7	40, 932	90,180	. 4267	16.8	1. 1607	45. 698	. 1686	10, 20
15	, 7035	27,7	40,932	90,180	. 4267	16.8	1. 1607	45.698	. 1888	10, 21
_16	. 6858	27	154,598	340,601	. 5588	22	3.08008	121.263	. 6552	40,0
man:								- 1	ì	
17			10,500	23, 131			• • • • • • • • • • • • • • • • • • • •		· · · · · · · · · · · · · · · · · ·	- · • • · · · • · • ·
18,			16, 526						• • • • • • • • • • • •	
19		.,	18,908		•					
20	'		25, 634	56, 475						
21	<i></i>	-,-,-,	45,300	99, 795	• • • • • • • • • • • • • • • • • • • •		1, 9994	78, 7106		
22			77,552	170.847	- 425	16.73 .			i	

					Rifling.					Maximum	n powder.
			Grooves.					Twist		press	
No.	Number.	Wid	th.	Depth	1.	Width le	unds.	Angle.	Calibers per turn.	Kg./cm.1	Lb./in.*
	(19)	(20)	(21)	(22)	(23)	(24)	(25)	(26)	(27)	(28)	(29)
narican:	12	M/m 5.3746	In. 0.2116	M m. 1.016	In. 0.04	Mm. 3.858	In. 0.14	4° 30'/8° 55'	40-20	2,038.9	29,00
2	42	7.4422	. 293	1.27	.05 {	5.842	. 23	}7° 10′	25	2,531.1	36,00
3A	48	6.4262 9.4894	. 253	1.524	.06	6.858 3.81	. 27	3° 30′ 7° 10′	50-25	2,671 7	38,00
В	32	10 5333	4147	1.27	. 05	4.419	- 174	7° 10′	25	2,249 8	32,00
C		12.3113	. 4847 . 4847	1.27	.05 .05	4.419	.174	7° 10′	25 25	2,601.4	37,00
F			. 1017	1.21 ;		1.719				2,531.1	36,00
F	72	5.3111	. 2091	1.524	.06	3.556	. 14	3° 30′/7° 10′	50-25	2,671.7	38,00 38,00
В	60	9.4894	. 3736	1 . 524	.06	3. 81	- 15	3° 30′/7° 10′	50-25	2,671.7	30,00
C											
D	72	9 4894	3786	1.524	.06	3, 81	- 15	4° 30′/8° 55′	40-20	2,601.4	37,0
56A	72	9.4894	3736	1.524	.06	3, 81	.15	3° 30' 7° 10'	50-25	2,671.7	38,0
B					• • • • • • • • • • • • • • • • • • • •						
7	108	5.3111	2091	1.524	.06	3. 556	.14	4° 30′ 8° 55′	32 40-20	2,671.7 2,601.4	38,00 37,00
9	126		2091	1.778	.07	3.556	. 14	3° 30′ 7° 10′	50-25	2,671.7	38.00
10										2,671.7	38,00
<u> </u>	. 				·········					2,671 7 2,671 7	38,00 38,00
12 13		····								2,671.7	38,00
14	144	5.3111	2091	3 048	.12	3.556	. 14	4° 30'/8° 55'	40-20	2,671.7	38,00
15	144	5 3111	2091	3.048	. 12	3 556	. 14	4° 30′ 8° 55′	40-20	2,671.7	3×, (x 38,00
l6	144	11118 9	. 2091	3.048	. l2	3.556	. 14	3° 30′,7° 10′	50-25	2,671.7	36,0
rman: 17	52		1					5° 43'	31		
18	64							5° 43'	31		
19	52							5° 43'	31		
20	52			<i></i>				5° 43′	31		
22	80 100	5.5626	.219			5.994	236	5° 43') มีเ		

GUN-Continued.

	Muzzle	Velocity.	Mussle		Velocity of rotation at muzile	Life in		Maximu	m range.
No.			((max.), f. p. m.	rounds.	Ran	ge.	Elevation.
	(30)	(31)	(33)	(33)	(34)	(36)	(36)	(37)	(38)
nerican: 1	M./e. 896 822 594/792	F1./z. 1,300 2,700 1,950/2,600	M./ T. 73.13 867.27 973.65	Ft./ T. 704 8,348 9,872	9, 968 10, 697 7, 918	910	Km. 9.14 15.63 19.19	Ydo. 10,000 17,000 21,000	40 degrées. 15 degrées 10 minute 42 degrées.
B. C. D.	670 701 701 868 1,021	2, 200 2, 200 2, 300 2, 300 2, 900 3, 250	761-92 761-92 761-92 1,129-28 1,618-29	5,710 7,334 7,334 10,970 15,578	7,920 8,280 8,280	850	29. 2	31,944	Do. Do. Do. Do. 45 degrees.
44 B C. D	688 457	2,250	2,249.42	21,652	6,480 4,500	1, 150	24.58	28,900	Do. Do. Do. Do. Do.
6A B 7 8	792 975 594 883	2,600 3,200 1,950 2,900	5,168.52 1,919.26 7,272-8	82,802 49,750 18,474 70,000	5, 400 8, 850 4, 834	370 240	26.80 41.18 19.74 29.25	29,000 45,000 21,600 82,000	38 degrees. Do. 40 degrees. 45 degrees. 30 degrees.
10	853 853 853 853	2, 800 2, 900 2, 800 2, 800	7,920.51 7,920.51 7,920.51 7,920.51	76, 240 76, 240 76, 240 76, 240	**************************************	220 220 220 220 220	*36. 56 36. 56 36. 56 36. 66	40,000 40,000 40,000 40,000	38 degrees. 43 degrees. 40 degrees. 36 degrees.
14	579 579 822	1,900 1,900 2,700	4,315.59 4,815.59 *12,616.36	41, 540 41, 540 121, 480	4,276 4,276 1,630	890 390	21. 23 21. 23	23, 000 28, 000 26, 256	45 degrees. Do.
18						4415.4	24 26.4 18.7	28, 881 20, 457 33, 914	45 degrees. Do. Do. Do.
~							31 47.48	51, 948	47.5 degrees.

						C	Characteristics.									
	Туре.	Model.	Make.	M	Firing	ang)s.	Rec	ol).								
No.				Extent of traverse.	Maxi-	Mini- mum	Туре.	Lan	gth.							
	(39)	(40)	(41)	(42)	(43)	(4)	(45)	(46)	(47)							
merican:	-			Degrees.	D. Min.		- 1	₩.	Is.							
1	Outrigger	1917	U. S. Ordnance	360	40	i o	Crad)e	0, 845	12							
2		1918	do	360 360	15 10	Ιo	do	. 533	ЯL							
JAAE	do	. 1918 MT	do	380	42	l o	do	1.219	48							
В	do	do	do	260	42	ا ا	Ido	1.219	48							
Č		do	do.	380	42	ō	do	1.219	48							
Ď	do			260	42	آ ا	do	1.219	48							
E.				340	42	آ ا	do	1.219	48							
	do		40	360 360	42	ı ă	do	1.219	48							
4A				200	45		S)(ding	*[*1	39.8							
				8	45		Shuingdo	•1	39.8							
B				, <u>,</u>	45	, ×		Ψ1 Ψ1								
<u>C</u>		40		ļ ,		l š	do		39.8							
	do				45		do	el	39.8							
5		. 1918 MII		360 10	66	20	Cradle	. 762	30							
6A		. 1018	Batignolles	10	38 38	18	do	.9	35.							
В		do	do	10		15	do,	.9	35.4							
7		. do,		0	40	18	Sliding	er[30.							
8	Outrigger	do	do	360	l 60	, 20	Cradio	. 914	36							
9	Sliding-ground platform		do	068-3 (i 30	0	do	1.82	36 60							
10		. Mr. I		10	30 46	15	do	1,142	45							
11		Mk. II	do	ľ	43	ň	Rolling	1.01	40							
12		1918		1 5	36		Suding	•1·01	39.							
18		1919		13	38 38		40	•5	39.							
14		1018		10	85	20	Cradio	3,219								
				360	88	20 20			48							
16		E	go			20	do	1.219	48							
16	Rolling		. ao	0	40		. Cradle—rolling	1.219	48							
erman:	ا ما ما		l		l a-		1									
17	Oround platform	. 170-millimeter, 1915	. Krupp	1 36-360	47 80	20	Cradie	. 381	15							
18		. 210-millimeter	.[do	1 25-360	45	20	do	.81	24.							
19		. 240-millimeter	. do	14-360	48	20	do	. 508	20.							
20	do	.ldo	-ldo	360	45	20	do	. 596	23.							
27		. 280-millimeter	do	J 2-360	45	20	do	, 762	20							
22	.,do,	, 380-millimeter, 1918		2-360	1 33	. 20	do	1.25	49.							
,		al manageri (Arg	* · · · · · · · · · · · · · · · · · ·	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		, 20		1	79,							

MOUNT-Continued.

	Characteristics.				Dimen	aions.		
No.	Loading system.	Rate of fire per hour.	Length buff		Center to	center of colsters.		trunnlon track.
	(48)	(49)	(50)	(51)	(52)	(53)	(54)	(55)
merican:		60	₩ . 9.75	Feet. 29.79	₩. 8.24	Feel. 20. 5	₩.	Feel.
2	Crane and tray	50	14.103	46.27	9.29	30.6	2.26	7.4
3¼		45	14.103	46.27	9.29	30. 5	3. 30	9.84
			14.103	46.27 48.27	9.29	30.5 30.5	3.30 3.30	9.84 9.84
D	do,		14.103	46.27	9, 29	30.5	3.30	9.84
E	do	43	14.103	46.27	9.29	30.5	3.30	9.86
F		45 {	14.103	46.27	9.29	30. 8	3.30	9.84
14	Trolley and tray	j 20 [27.2003	89.24	17. 29	56.75	3.55	11.66
B	dodo	: 20 i	27.2003	89.24	17.29	68.75	3.55	11.60
Ç	do	20	27.2003 27.2003	89.24 89.24	17.29 17.29	56.75 56.75	3.55 3.55	11.66 11.66
ν	Crane and tray	20 25	14,103	40. 270	9.29	30.8	2.91	9.56
	'do	:::: 2 0	19, 967	65. 51	12.96	42.58	8.24	10.69
В.	·do	20	19.967	65. 51	12.98	42, 58	3, 24	10.62
7	Crane and shot truck	20	20, 611	100.43	19.40	63.86	3.60	11.89
8	Crane and tray	25	12.85	42.16	, 8.53	28	2.88	9.45
9			21.90	72.08	15.59	51.16	3.08	10.12
10		30	25.804	84.66	18,45	54	2.74	8.96
11			27. 67 34. 68	90.81	15.84	52	3.24 3.49	10.66 11.48
12	Crane and shot truck.	20	32.84	113.8 107.77	18.84 18.38	61.83 60.33	3.49 3.49	11.48
			17.77	58.33	10.97	36	3.26	*10.7°
15			15.18	49.83	10.15	33.33	1.77	5.81
16			36.75	120.58	22,50	73.83	●2.84	9.33
erman:	7,11,11, 5,11,11,11,11,11,11,11,11,11,11,11,11,11	}						
17.,	Rand tray	60	16.75	54.94	13.53	44.37	. <i>.</i>	<i></i>
18	T70lley tray	40	15.86	61.98	11.569	38.99	2.75	9,02
19		30	15.85	51.98	11.89	38.99	3.07	10.00
20	do	30 [19.68	64.58		*******		
21		30	21.01	70.91	14	45, 92	3.4	11.16
23	Windiass shot truck	20	31.61	103.68	21.15	69.37	3.07	10.0

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American: Meters Feel Meters Feel Kilograms Pounds Kilograms Mone Kilograms Pounds Kilograms Pounds Kilograms Mone Kilograms Mone Kilograms Pounds Kilograms Mone Kilograms Mone Kilograms Pounds Kilograms Mone Mone	•		Dime	nslons.				Well	thts.		
American: Meters. Feel. Meters Feel. Kilograms. Pounds. Pounds.	Na.	Maximum	width.	Center to	center of les.	Recollin	ng parts.	Top carriag	e complete	Cart	oody.
1.		(56)	(57)	(58)	(59)	(60)	(61)	(62)	(63)	(64)	(65)
2.	American:	Metera.	Feet.			Kilograms.	Pounds.	Kilograms.	Pounds.	Kilograma.	Pounde.
3A	2	2.89	9. 5	1.77				30,049	66, 292	24, 23×	53, 400
C. 2.89 9.5 1.77 5.83 16,421 36,178 26,402 58,300 27,887 6 6 6 8 1.77 5.83 16,421 36,178 26,402 58,300 27,887 6 6 7 8 8 8 1.77 5.83 16,421 36,178 26,402 58,300 27,887 6 7 8 8 8 8 1.77 5.83 16,421 36,178 26,402 58,300 27,687 6 7 8 8 8 8 8 1.77 5.83 16,421 36,178 26,402 58,300 27,687 6 7 8 8 8 8 8 8 8 8 8	3 <u>A</u>			1.77				26, 402	58,300	27, 637	61,000
D											61,000
R. 2.89 9.5 1.77 5.83 16,421 36,178 26,402 5×,300 27,687 6 F. 2.89 9.5 1.77 5.83 16,421 36,178 26,402 5×,300 27,687 6 4.A 3.06 10.01 1.17 n3.85 183,121 403,440 None. None. 105,913 23 B. 3.06 10.01 1.17 n3.85 183,121 403,440 None. None. None. 105,913 23 D. 3.06 10.01 1.17 3.85 183,121 403,440 None. None. None. 105,913 23 D. 3.06 10.01 1.17 3.85 183,121 403,440 None. None. None. 105,913 23 D. 3.06 10.01 1.17 3.85 183,121 403,440 None. None. None. None. None. None. None. None. No											61,000
F. 2.89 9.5 1.77 5.83 16.421 36,178 26,402 58,300 27,687 6 4A. 3.06 10.01 1.17 83.85 183,121 403,440 None. None. 105,913 23 B. 3.06 10.01 1.17 83.85 183,121 403,440 None. None. 105,913 23 C. 3.06 10.01 1.17 3.85 183,121 403,440 None. None. 105,913 23 D. 3.06 10.01 1.17 3.85 183,121 403,440 None. None. 105,913 23 5. 2.89 9.5 .99 3.25 18,941 41,730 27,271 57,890 27,234 6 6A. 2.94 9.66 1.4 4.59 56,114 123,628 34,210 75,370 28,573 6 18 2.94 9.66 1.4 4.59 56,114 123,628 34,210 75,370 28,573 6 7. 2.63 8.66 1.06 3.5 249,645 550,000 None. None. None. 105,913 23 S. 3.0 10.5 1.21 4.0 68,375 150,640 None. None. None. 123,006 27 S. 3.20 10.5 1.21 4.0 68,375 150,640 None. None. None. 123,006 27 S. 3.20 10.5 1.21 4.0 68,375 150,640 None. None. None. 121,006 27 S. 3.20 10.5 1.21 4.0 68,375 150,640 None. None. None. 110.11 150 150 150 150 150 150 150 150 150 1											61,000
4A. 3.06 10.01 1.17 n3.85 183,121 403,440 None. None. 105,913 23 23 23 24 24 24 24 2	P										61,000 61,000
B.											233,340
C. 3.06 10.01 1.17 3.85 183,121 403,440 None. None. 105,913 23 D. 3.06 10.01 1.17 3.85 183,121 403,440 None. None. 105,913 23 5. 2.99 9.5 .99 3.25 18,941 41,730 22,271 57,880 27,234 66 6A. 2.94 9.66 91.4 94.59 56,114 123,628 34,210 75,370 28,573 68 R. 3.2.94 9.86 1.06 3.5 249,645 550,000 None. None. 123,006 27 8. 2.99 9.83 1.01 3.33 22,326 48,188 22,306 62,383 46,687 10 8. 3.20 10.5 1.21 4.0 68,475 150,640 None. None. None. None. R. 11 2.94 9.66 1.08 3.41 276,879 610,000 None. None. None. R. 12 2.81 9.25 1.04 3.44 315,000 683,945 None. None. None. R. 13 2.68 8.84 1.03 3.41 329,400 724,850 None. None. None. R. 15 3.09 10.16 1.44 4.75 43,165 95,100 None. None. R. 16 3.09 10.16 1.44 4.75 43,165 95,100 None. None. R. 17 None. None. R. 18 3.04 10 1.21 4.0 385,815 850,000 None. None. R. 19 3.4 11.15 None. None. R. 10 None. None. R. 10 None. None. R. 10 None. None. R. 11 None. None. R. 12 None. None. R. 13 None. None. R. 14 R. 15 R. 165 R. 165	R										
D	Č.				3.85						233,340
5.	D										233,340
6A.											60,000
R											61,814
7	B		9, 86								61, 81
9.			8. 66	1,06	3.5	249, 645	\$50,000				271,000
9 . 3.20 10.5 1.21 4.0 68,375 150,640 None. None. 68,184 15 10. 2.87 9.41 1.37 4.5 37,673 83,000 None. None. None. None. 11. 11. 11. 11. 11. 12. 12. 13.	8		9. 83		3.33			2×,306	62, 383		102, NH
10	9									68, 154	150, 221
12. 2.81 9.25 1.04 3.44 315,000 687,945 None. None. 96,000 21 13. 2.69 8.84 1.03 3.41 329,400 724,850 None. None. 100,000 22 14. 2.94 9.66 91 30 43,165 95,100 None. None. None. 155. 309 10.16 1.44 4.75 47,165 95,100 None. No	10.,,										
13											
14. 2.94 9.66 91 3.0 43,165 95,100 None. None. None. 15. 3.09 10.16 1.44 4.75 43,165 95,100 None.											211, 4%
15. 3.09 10.16 1.44 4.75 43,165 95,100 None. None. None. None. None. 18. 3.04 10 1.21 4.0 385,815 850,000 None. None. None. None. 17. None. None. None. None. 18. None.										100,000	220, 300
18. 3.04 10 1.21 4.0 385,815 850,000 None. None. 98,950 #21	14										• • • • • • • • • • • • •
17.	(arman	3.04	10	1.21	4.0	341, 413	830,000	None.	None.	94,350	*218,000
18.		,						! Name	Nana		
19. 3.4 11.15 None None None None None None None None											
21None. None. None.	19	3.4	11. 15		i			None.			
21None. None. None.	20	3.4	21. 10					None			
	21.							None.	None.		
22			•••••	1.36	4.46		1				

Table of classified data (42)—Continued.

MOUNT—Continued.

			Weig	hts.					Trucks.		
								N	umber ax	les per truc	k.
No.	Span t	olster.	Axle load, 1	nsximum.	Total v	reight.	Number.	Front.	Rear.	Exterior.	Interio
	(66)	(67)	(68)	(69)	(70)	(71)	(72)	(73)	(74)	(75)	(76)
erican:	Kilograma.	Pounds.	Kilograms.	Pounds.	Kilagrams.	Pounds.			ì		
l	None.	None.	5, 147	11,374	20,660	45, 498	1 2	2	2		
2	None.	None.	19,404	42, 750	77,616	171,000	2	2	2		
3.4	None.	None.	19,908	43, 850	78, 978	174,000	ءَ ا	2	2		. ,
В	None.	None.	19, 903	43, 850	78,978	174,000	1 2	2	2	1	
Č	None.	None.	19,903	43, 850	78,978	174, 800	l 2	2	2		
D	None.	None.	19,908	43, 850	78,978	174,000	1 2	2	2		
Ē	None.	None.	19,908	43, 850	78,978	174,000	1 2	2	2		
P.,	None.	None.	19,908	43, 850	78, 978	174,000	1 2	2	3		
4		None.	15,508	34, 167	183, 121	403, 440	1 2	6	6		
В		None.	15,508	34, 167	183, 121	403, 440	1 2	6	6		
C		None.	15,508	34, 167	183, 121	403, 440	1 2	6	6	I	
D		None.	15,508	34, 167	183, 121	403, 440	1 2	6	6		
3		None.	14, 181	81, 133	80, 340	177, 000	1 2	3] 3		
6A	None.	None.	18,530	40, 825	146, 175	322,014	l ā	1 4	4		
B	None.	None.	18,830	40, 835	146, 175	322,044	قا	l i	1 4		14
7	1	11020,	16,664	36,692	249,848	560,000	l ī	l	I	. 4	
8.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	None	None.	16,309	85, 931	88, 620	195, 243	l į	****	3	`	
9	None.	None.	24,987	55.061	198, 218	486.700	1 2	1 1	4		
		Mone.	24,056	53,000	244, 000	537, 532	1 1			3	1
10			15,977	36, 200	276, 879	610, 000	1 7			Ĭ	
11.,,	45,000	99, 185	18,430	33, 992	306,600	679, 845	1 7		1,	Š	
13	38,700	85, 256	16,900	37, 230	329, 400	724, 850	1 7			· .	
13,	None.	None.	12,966	28,566	141,957	312,760	1 3	A		-!	
14	None.	None.	18,534	40, 833	111, 205	246, 000	1 2	ı s	۱ š	;	1
15		*50,000	16,068	35,400	385, 815	850,000	1 1		ı .		1
16.:	22,696	-30,000	10,000	30, 100	300,000	200,000	· •		1	٠, ۳	
17	None.	None.	15,011	23,069	60, 045	132, 279	1 2	2	1 9	l	
		None.	11,804	26.004	84, 440	208,761	5	1 2	1		1
18,	None.		14,137	31,143	113,100	249, 159	1 2	1 1	1 7		
19		None.			100,100	227, 590	1 1	1 7	1 7		
20	. None.	None.	*14,500	31,943	103, 308		1 4	! :	?		
21	. None.	None.	•14,500	31, 943	180, 027	\$30,530	7		هه		1
2 ,	.l				267, 900	595,060	4	s anch.	4 each.		

	_	_	Wheels					Tot	al weight	of each tru	ck.		
No.	Journa	Me.	Туре.	Diatri	neter.	Fra	nt.	Re	LF.	Exte	erior.	Inte	riot.
	(77)	(78)	(79)	(80)	(81)	(82)	(83)	(84)	(85)	(86)	(87)	(88)	(89)
merican:	#f. 6. 101 by 0. 178	In. 4 by 7	 	М. 0.88	/n. 26	Kg.	Lb.	Kg.	Lb.	Kg.	Lb.	Kg.	Lb.
2 3A B C D E F A A B C C D B C D B C D B C D B C D B B C D B B C D B B C D B B B B	1.52 by .279 1.52 by .254 1.39 by .254	6 by 11 6 by 11 6 by 11 6 by 11 6 by 11 6 by 11 5.5 by 10 5.5 by 10 5.5 by 10 6.60 by 12, 2 5.5 by 10	Cast stee)	. 538 . 838 . 711	43 33 33 33 33 33 34 34 34 34 34 34 34 3	4, 765 4, 766 4, 765 4, 765 4, 765 4, 765 4, 765 23, 353 26, 353 26, 353 27, 353 28, 353 38, 353 38, 353 38, 363 38, 3	10,500 10,500 10,500 10,500 10,500 10,500 10,500 10,500 51,450 51,450 51,450 51,450 32,500	4, 765 4, 765 4, 765 4, 765 4, 765 4, 765 4, 765 23, 353 23, 353 23, 353 6, 808 14, 761	10,500 10,500 10,500 51,450 51,450 51,450 31,450 32,500				
8 9 10	. 165 by .304 .162 by .279 .228 by .304	6.5 by 12 6 by 11 9 by 12	Locomotive	.711 ,787 .914	28 21	12,709	28,000	12, 709	28,000		• • • • • • • • • • • • • • • • • • •		
11 12 13 14 15	.165 by .304 .165 by .304 .165 by .304 .152 by .279	6.5 by 12 6.5 by 12 6.5 by 12 6.5 by 12 6 by 11 6.5 by 12	do	.762 / .838 / .711 / .711 / .711 / .838 /	36 30 33 28 28 28 28	17, 475	28,500	17,475	38,500		36,000 37,300 40,000	10, 893 12, 119	24,0 26,7
17	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		Cast-steel spokes	. 838	* 33								

Table of classified data (42)—Continued. ANCHORAGE.

	_	Total			Pla	tform car.			
No.	Туре.	com- ponents.	Total	weight.	Туре.	Wei	ght.	Time to install.	Time to remove
	(90)	(91)	(92)	(93)	(94)	(95)	(96)	(97)	(98)
nerican:	iveet	i	Kg.	120,	None	Kg.	Lb.	45 minutes	25 minutes.
	lo	. 10	***************************************					do	
	lo	18						do	I Do.
Bd	lo	18			do			do	Do.
	10	16			مه			do	Do.
	lo	18			do		<i>-</i>) do	Do.
	lo	. 18			do	••	· · · · • · · · · ·	40	Do.
	ስለ በደ	18	10,000		Com, fist	+ 12,981		3 ponts	1 hour.
	lo	30	12,083	. 26, 620 . 26, 620	do		28,500 28,500	do. •	Do. •
	lo.,	30	12,083	26,820	do		28,600	do. •	Do. 4
	lo		12,083	26, 820	do		28,600	45 minutes	25 minutes.
5 Outr	weer		12,000	20,020	None		25,000	à hours •	I hour.
	and platform		15.680	34,550	Special	20,420	46.000	do. •	Do. *
В	lo	6	15,680	34, 550	do		45,000	do	Do. •
7, Sildi	ng., , , , ,,,,,,,,,,,,,,,,	. 48	67,750	149,419	Com. flat		28,000	45 minutes	25 minutes.
	rigger	. 18		٠.,,٠.,٠.	None			3 hours	2 hoeurs.
9 Slidi	ng-ground platform		30,867	68,000	Steel flat		44,000	3 to 5 days	12 hours.
10 Grou	uid platform	• 10		' ·.,	Com, flat		28,600	5 days	Not removed.
11,., Rolli	ing	0		į • • • · · · • • • · •	None			8 hours	1 hour.
12 slidi	ng	. 48	· - • • • • •	·.······	Com. fat		28, 500	do, •	Do. 4
13	10	. 48		,	do		28,600	8 to 5 days	13 ponta.
	ing-ground platform			· · · · · · · · · · · · · · · · · · ·	do	12,981	29,600 44,000	2 days *	Not removed.
	ind platform	· •			None	19,9/1	44,000	5 days	MOL Temoved.
rman:				j	None			I	
		1	İ	1				/15 minutes •	10 minutes.
17 Trac	k,d ground platform	. 10	`	ļ	Com. flat	12,981	* 28,600	12 hours	3 bours.
		(44	1				l	17 days 4	Not removed.
18	10.4	1 5 R6	}			12,98t	* 28,600	IS days	2 days.
19	40.4	1 14	!		l a.	40.00		7 days	Not removed.
	-V · , ,	- 1 ▶ 88	· · · · · · ·	1	¦do	12,981	• 28, 600	5 days	2 days.
20	ào,		.f	'	do			3 to 6 weeks	2 weeks.
21	do.4	1 4	1	1	40			[7 days =	Not removed.
200.000	40	· { b 86	J					15 days b	2 days.
22	do, 4		ľ		' do			2 to 7 weeks	3 weeks.

AMMUNITION—CAR.

	Lengt buff	h over lers.	Center t		Maximum ovoda	m beight rail.			Total	welght.	
No.							Capacity (105)	Long	ded.	Em	pty.
	(99)	(100)	(101)	(102)	(103)	(104)		(106)	(107)	(108)	(109)
merican:	Metera.	Feet. 39.83	Meters. 7.90	Feet. 28.23	Meters.	Feet. 11.96	Rounds.	Kilograma.	Pounds.	Kilograms. 15, 205	Pounds. 33,500
2	. 12.14	39 83	7.99	26.23	3.64	11.98	96	25,003	55,090	15,205	33,500
3 <u>A</u>		39.83	7.99	26.23	3.64	11.96	96	32 , 869	72, 416	15,205	33,500
B	. 12.14	39. 53	7.99	26.23	3.64	11.98	95	32,889	72,416		33,50 33,50
C	. 12.14 . 12.14	39.83 39.83	7.99 7.99	26.23 26.23	3.64	11.96	96	32,869 32,869	72,416	15, 205 15, 205	33,50
D	12.14	39. 83	7.99	26.23	3.64 3.64	11.96 11.96	96 96	32,869	72, 416 72, 416	15,205	33,50
F	12.14	39.83	7.99	26.23	3.64	11.98	96	32, 889	72, 416	15,205	33,500
4A	12.14	39.83	7.99	28. 23	3.64	11.98	48	29, 809	65, 674	15, 205	33,500
В		39. 83	7.99	26.23	3.64	11.96	48	29, 809	65, 674	15, 205	33,500
ŗ	12,14	39. R3	7.99	26 23	3.64	11.96	48	29,809	65, 674	15,205	33,500
D ,	. 12.14	39.83	7.99	26. 23	3.04	11.96	48	29,809	65,674	15, 205	33,500
5	12.14	39.83	7.99	26.23	3.64	11.96	48	39,380	86,760	15,205	33,500
6A	12.14	39.83	7.99	, 245.23	3.64	11.96	36 ;	37,098	81, 732	15, 205	33,500
_B	L2 14	39.83	7.99	26.23	3 64	11.96	35	37,098	81,732	15, 205	33,500
7		39. 83	7. 99	28. 23	3.64	11.96	36	32,150	70,832	15, 205	33,500
8	12.14	39, 83	7.99	26, 23 26, 23	3 64 :	11.96	48	32,528 39,171	71,660 86,300	15, 205 15, 205	33,500 33,500
9	12.14	39.83 39.83	7.99	26.23	3.84	11.96	24 25	36, 425	80, 250	15, 205	33,500
11,	12.14	39.83	7.99 : 7.99	26.23	3. 84 3. 64	11.96 11.96	25	36, 425	80, 250	15, 205	33,500
12	12.14	39.83	7.99	26.23	3.64	11.95	23,	36, 125	80, 25 0	15, 206	33,500
13	12.14	39.83	7.99	26.23	3.64	11.96	25	36, 425	80, 250	15, 205	33.500
14	12 14	39.83	7. 99	26.23	3.64	11.96	2ñ. ∣	41,531	91,500	15, 203	33,500
15	12 14	39.83	7. 99	26. 23	3.64	11.96	2 0 i	41,531	91,500	15, 205	33,500
16	12.14	39.83	7. 99	26. 23	3.64	11.96	20	44, 709	98, 500	15, 205	33,500
erman;								,	,	- 1	,0,0
17	[, , . , .] .						,,,,,,,,,				
18			.,								
19	[].										
20					.	,		, 			 .
21											
22	1										

AMMUNITION-POWDER.

		Weights of reduced charges,										
No.	Weight of full charge.		Α		В		С		D		E	
	(110)	(111)	(112)	(113)	(114)	(115)	(116)	(117)	(118)	(119)	(120)	(121)
merican:	Kilograme.	Pounde.	Kilograma.	Pounds.	Kilograms.	Pounds.	Kilograms.	Pounds.	Kilograme.	Pounds.	Kilogramu.	Pounde.
<u>l</u>	27.2	60				•••••			• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • •		
	27.2	₩60	26.32	= 58		:::::::::::::::::::::::::::::::::::						
3 <u>A</u>	37.3	= 82.375	32.04	× 70. 628	22.86	≥50.375				••••		
B	37.3	■ 82. 375	323.04	¥ 70.628	22.86	50.375						
<u> </u>	37.3	= 82. 375	32.04	¥ 70.628	22.86	50.375						
<u>p</u>	37.3	82.37 5	32.04	k 70.628	22.86	¥ 50. 375						•
<u>F</u>	37.3	= 82, 375	32.04	► 70.628	22.86	► 50.375	,-,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					• • • • • • • • • • • • • • • • • • •
	37.3	82.375	32.04	≥ 70.628	22.86	≥ 50.875					.[•••••	• • • • • • • •
<u></u>	72.76	≥ 160. 312	70.85	= 155	55.	k 121.187						
B	73.76	k 160.312	70.35	= 155	55.	121.187	4					
<u>c</u> ,	72.76	k 160. 312	70.35	≈ 155	55.	L 121. 187						
_D	72.76	≥ 160. 312	70.35	™ 155	55.	₹ 121. 187		*********				
5	28.9	63.69	19.29	42.5	14.58	32, 125	11.26	24.812	8.96	19.75	7.63	16.8
6 <u>A</u>	122.46	269 . 81	103.48	¥ 228.125	71.48	157. 5				·····		
B	122.46	= 209. SI	103.49	k 229, t25	4141							
7	152, 96	337	108.93	240								
8	43. 12	95				,,,						
9	245.1	- 540	238.29	525	190,63	k 420	177.02		, , , , , .			
10	213.33	470	159.99	352.5	61.27		[}]		<i>.</i>			
11	213.33	470	159.99	852. 5	61.27	135	1					
12	213.33	470	159.99	352.5	61.27	135						<i>.</i>
13	213.33	470	159.99	352. 5	61.27	135		<u>.</u> <u>.</u>				
14	106-93	240	78.07	172	59	130	48.79		42.49	98.5	1	
15	106.93	240	78.07	172	59	130	48, 79	107.5	12.48	93.5		
16.,,,	385.81	860										
orman;	I I		1		'		1					
17,		184, 84	I		j							
16	143,068	31 5. 2 2		.,								
19		64.15	[<i>.</i>	,			l- 				
20.,,,,,	43.83	99.87			·						. <i>.</i>	<i></i>
21	69.7	158.58		,,								
22	183.12	408, 45				1				ı		

718

	J			
L 24		¥7. 0-4704	In. 18.52	
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4			*** * *****	
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4				
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3				
. 3			**********	
3				
3				
	• •	• • • • • • • • •		(L)
4				
. 4				9
L 4				
l. 4		1. 1417	44.95	
L 4		1. 1417	44. 95	
		1.593	62, 72	
)		L. 1417	44 95	
,		1, 1417	44. 95	
1		1. 1417	44, 95	
1		1, 1417	44. 95	
		1.5015	62. 83	
		1. 505A	62. 83	
65		1. 8161	71. 50	
. 00	ı	r - 9101	11.00	

.				We	Lammb ha	4 1 4		
181768	Туре,	Turget,	Total.		Explosive,		Length base to point.	
 - 21_	(122)	(123)	(124)	(125)	(124)	(127)	(128)	(129)
C. D. E. F.	do	do	879. 27. 23 74. 80 101. 21 101. 21 101. 21 101. 21 101. 21 101. 21 231. 49 231. 49 231. 49 231. 49 231. 73 317. 73 317. 73 317. 73 753. 47 635. 48 635. 48 635. 48 635. 48 635. 48 635. 48 635. 48 635. 48 635. 48 635. 48	28. 80 165 323 323 323 323 323 510 510 510 510 510 700 1,670 1,660 1,400 1,400 1,660 1,660 1,660 1,400 1,660 1,660 1,660 1,400 1,660 1,660 1,400 1,660 1,660 1,400 1,660 1,660 1,400 1,660	70. 1. 47 1. 481 2. 45 2. 45 2	Zb. 3.24 5.4 5.4 5.4 5.4 5.4 5.4 5.6,3 56,3 56,3 56,3 56,3 56,3 56,3 56,3 5	1. 1417 1. 1417 1. 1417 1. 1417 1. 1417 1. 1417 1. 1417 1. 1417 1. 5958 1. 8161 799 1. 629	

AMMUNITION-PROJECTILES; B.

No.	_			Length base				
	Турс.	Target.	Total.		Explosiva,		to point.	
	(130)	(131)	(132)	(133)	(134)	(135)	(135)	(137)
_B		doNavaldo.	Kg. 27: 23 59: 44 14: 86 14: 86 14: 86 290. 05 290. 05 374. 07 485. 67	60 153 323 323 322 323 323 323 323 323 323 3	R9. 4 29 10.89 7 12 7 12 7 12 7 12 7 12 7 12 7 12 5 49 5 49 11 84 24 55 26 55	£b. 9. 44 24 7 15. 7 15. 7 15. 7 15. 7 15. 7 15. 7 12. 1 12. 1 12. 1 12. 1 12. 1 58. 51 58. 51		
S 9 9 10 11 11 12 13 14 15 16 German 17 18 19 19 19	II. F. shell	Len1. do. do. do. do. do. do. do. do. do.	544. 68 544. 68 544. 68				'	61. 05 61. 05 61. 05 61. 05 61. 05

. 72(

Table of classified data (42)-Continued. AMMUNITION-PROJECTILES: D.

	Тура	Target.		Weight,				
No.	1,440	1	Tot	Total.		losí ve.	/# PO\	
	(146)	(147)	(148)	(149)	(150)	(151)	(152)	(153)
merican:			Kg.	Lb.	Kg.	Zb.	¥.	In.
2							,	
B			- ,					
D		,4*-*,4		i				
E								
4 A								
B							********	(· - <i></i>
h ·	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,					4		
5 Long	point shellshell	NavaiLand	317.73	700	10.98 41.03	24.2 90.4	0.9672	38.6
, B								
8								
10								
13		.,						
14			., .,					
7man: 17		,						
18								
			• •		••••••	- 		
21	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,						*********	,
22								

NOTES.

- Approximate,
 For firing beams only—time for laying of,
 For ground platform.
 Can likewise be fired from wheels.

- # Mount is held by wedges.
 # On track.
 # Ground platform.
 # Concrete.

- A Steel.

 Turntable type.

 On truck.

- For land projectiles.

 For seacoast projectiles.

 Variable—see diagram.

APPENDIX I.

THE GERMAN LONG RANGE GUN (43).

FIRST DAY'S BOMBARDMENT-FIRST IMPRESSIONS.

690. At 7.15 on the morning of March 23, 1918, just two days after the Germans opened their offensive against the British Fifth Army before Amiens, the people of Paris were startled by an explosion of something that had fallen on the Quai de Seine. The explosion was of such magnitude that it could be heard over practically the whole of Paris. Fifteen minutes later there occurred another explosion of the same magnitude, but this time closer to the Seine on the Rue Charles V; 15 minutes later another explosion occurred on the Boulevard de Strasbourg near the Gare de l'Est. Until that time Paris had never been bombarded except from airplanes and Zeppelins, and the first thought of the people was that they were being bombarded from some new type of aircraft that was being operated at such a height that it was practically invisible.

691. The explosions continued to occur throughout the morning at very uniform intervals of 15 minutes, and by evening 21 explosions had occurred at the places shown on plate 509. These are mentioned by their exact location under March 23 in the table given as plate 510. After the first few explosions between 7 and 8 o'clock in the morning, business in Paris practically ceased. Stores were closed and part of the Metro system ceased to operate; ticket offices in some of the railway stations were closed, and great numbers of people could be seen walking the streets looking skyward trying to locate the planes that were dropping the supposed bombs.

692. Information of the extraordinary bombardment was tele-

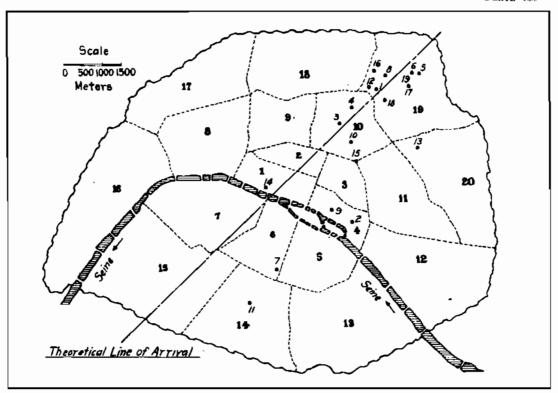
phoned and telegraphed over practically the whole of France within a few hours and was received everywhere in amazement. After a few hours on the first day a sufficient number of the fragments of the exploding agent were collected by officials in Paris to identify it as a projectile being fired from a gun, rather than a bomb being dropped from an airplane. By noon representatives of the Heavy

Artillery Section of the Ordnance Department, located at Tours, had made preliminary calculations in response to telephone instructions from Paris, giving the probable muzzle velocity at which a

projectile would have to start in order that it might travel from a few kilometers within a point of the German lines nearest Paris to the center of Paris. Inquiries were made likewise of the section as to the possibility that these projectiles could actually be coming from a gun within the German lines. The reply was that the probable muzzle velocity of the projectile, if it was actually being fired within the German lines, was not less than 4,500 feet per second. No such muzzle velocity had, to their knowledge, ever been realized, but with a gun of sufficient length and with a powder burning at a satisfactorily low speed, it was considered quite possible that the projectiles were being fired from within the German lines. By the end of the first day, officers of the French as well as the American Armies were quite certain that the projectiles were being fired from a newly designed long range gun, located within the German lines, and operating at a probable range of 110 kilometers (68.8 milés).

693. During the next few days some interesting theories were advanced in the various newspapers. In one case it was maintained that the projectiles which arrived in Paris were being fired from another much larger projectile, which actually served as a gun. This larger projectile was said to have been fired from a gun within the German lines and upon attaining a certain height, a charge of powder within the larger projectile was automatically ignited, firing the smaller one to a much greater distance. The theory that the projectiles were being fired from guns concealed in abandoned quarries or in heavily wooded regions near Paris received considerable credence and diligent search was made of all such places to be certain that it was not true. A third theory was that the projectiles were being fired from a pneumatic gun located within Paris.

694. A plotting of all the bursts for the first day showed results that were very puzzling. If the guns were being operated at comparatively short distances, the only way to account for the tremendous dispersion was on a basis of actual laving of the gun for different objectives. This theory did not seem plausible, however, because if the gun was actually laid on given objectives, these objectives were of relatively small importance. If, on the other hand, the projectiles were being fired from a gun at a great distance, it was seen at once that the dispersion was so great as to make it practically impossible to hit with any certainty any objective much smaller than that portion of Paris within the walls. It was noticed that the dispersion in direction, that is, to the right or left of the theoretical line on which the projectiles were arriving, was comparatively small, while the dispersion in range, that is, over or under the probable point at which the projectiles were supposed to arrive, was very great. Examination of the map, plate 488, shows that on this



LOCATION OF BURSTS ON FIRST DAY OF THE LONG-RANGE GUN BOMBARDMENT OF PARIS.

first day, when the gun was new, the average dispersion in range was very small compared with the dispersion on later days when the gun became worn.

695. Evidence received later indicates that at the end of this first day's bombardment the first gun was about half worn out. Eighteen projectiles had fallen within the walls of Paris and 3 outside; 15 people had been killed and 36 had been wounded. The destruction of property had been comparatively small. By "comparatively" it is meant that the destruction was small in comparison with that wrought by the 100 and 300 kilogram airplane bombs. Whenever the projectiles landed in the street or in an open plot of ground, the hole made was seldom more than from 12 to 15 feet in diameter and from 4 to 6 feet in depth. When the projectiles struck buildings it was not unusual to have them explode in the interior without showing any considerable signs of damage on the outside.

696. On the 24th of March 13 projectiles fell within the walls of Paris and 9 without, killing 11 people and wounding 34. On the 25th 4 projectiles fell within the city and 2 without. This was the end of the first gun. It was worn out, and no more firing was done until the 29th, when the second gun began its work.

697. Search of the files of the French War Office revealed the fact that full drawings and plans had been on hand for quite a long time for just such a gun as the Germans were probably using. These specifications had been submitted several years before and had been discarded because of the excessive expense and the tremendous difficulties involved in manufacturing such a gun. It was considered likewise by those who had turned down the specifications that the value of such a gun was extremely questionable. It was realized that its dispersion would be excessive and that with the powders with which the service was then familiar it would be exceedingly difficult to secure a muzzle velocity sufficiently uniform to do effective work.

DETAILS OF THE BOMBARDMENT.

698. When the bombardment was over, an examination of the period over which it had extended indicated that it had been divided into three distinct series. The first extended from March 23 to May 1, the second from May 27 to June 11, and the third from July 15 to August 9. It seems certain that this division into series was a part of the plan of the large offensives being waged during that time. The table, pages 751 and 752, gives the bombardment by days during this entire period and shows the number of projectiles falling within and without the walls of Paris each day, the number of people killed and wounded, and the exact places where the projectiles fell. During the first few days of the bombardment the first projectiles arrived between 7 and 8

o'clock in the morning and continued to fall at intervals of 15 minutes through a portion of the day. On later days the bombardment would begin at 12.40 noon.

699. Much has been said with reference to the effect of this bombardment on the people of the city of Paris. The writer's first direct acquaintance with the bombardment was during the third and fifth days. With considerable surprise it was observed that already the people were taking it quite philosophically; in fact it could not be seen that they were paying much attention to it at all. At intervals of about 15 minutes muffled explosions would be heard in different parts of the city, seldom two consecutive explosions in the same vicinity. Many people would stop for an instant and attempt to decide from what direction the sound had come, after which they would go on their way apparently unconcerned. It was, of course, still sufficiently novel to be of considerable interest, and people were talking about it everywhere. It is quite probable that the regularity with which the projectiles were arriving got on the nerves of some people, and that the bombardment was responsible for the departure of some of the people who were crowding the trains west and south from Paris. It seems more certain, however, that by the 1st of June the close proximity of the Germans to the city of Paris, together with the anxiety caused by another drive impending, added to the effect of the heavy bombardments from airplanes on every clear night, had far more effect than the gun. The visible destruction of property was so slight as to give little evidence to anybody traveling about the city that the explosions they were hearing from time to time amounted to anything. The newspapers were very careful to avoid any discussion or even a lengthy reference to the bombardment from day to day. and neither gave the locations of the places where the projectiles had fallen nor the number of killed or wounded.

700. The Germans must certainly have known that their gun was not a profitable investment for the destruction of property; hence they must have continued the bombardment purely for its destructive effect on the morale of the Parisians and its beneficial effect on the morale of the Germans. This is likely the purpose which prompted the construction of the guns. In his book, "My Thoughts and Actions," Gen. Ludendorf says: "During the battle we had commenced bombarding Paris from near Laon with a gun having a range of 75 miles. This gun was a marvelous product of technical skill and science, a masterpiece of the firm of Krupp and its director, Rausenberger. The bombardment made a great impression on Paris and on all France. Part of the population left the capital, and so increased the alarm caused by our successes." He is right; the bombardment did make a great impression; it made everyone more angry and alarmed very few. It is certain now that they

could ill afford to use their manufacturing facilities for the making of such guns as these at a time when they were so desperately in need of heavy field guns to assist their armies in their big drives.

701. Long-range or super guns received consideration from the Allies for a very short period. There was a tendency for a few weeks to favor the construction of a great number of them, but a saner view soon prevailed, and actual steps were taken for the construction of only a very few. Both the British and the French Governments began the construction of a few, some of which have now been finished. They built them, however, with a clear understanding that they could hope for but little more from them than the Germans were getting from their own. American Ordnance officers feel that it would not profit us to construct more than two or three such guns at most and probably none at all.

702. Within a very few days from the beginning of the bombardment it was possible through careful examination of the direction of the passage of the projectiles through various buildings, to determine quite accurately the direction of their arrival and the probable place from which they were coming. This place was in the Forest of Gobain, west of Laon. Very soon thereafter the French Air Service was able to locate in this same forest three positions, from any one of which, or possibly from all of which, the guas were being operated. Only one of these were sufficiently close to the German and allied lines to permit of any possibility of operating against it with the heavy guns then in service. The gun selected was a 34 centimeter (13.38 inches), 45-caliber French gun on a railway mount. This mount was run up to a point very close to the lines and behind a hill of such size as to effectively conceal it from German line observers. It was well camouflaged by nets against the air observer and against German sound ranging apparatus by placing two smaller guns at the right and left and several hundred yards behind it. These smaller guns were fired at intervals of one and two seconds before the larger gun, and evidently had the effect of so disturbing the German sound ranging apparatus as to make it impossible to locate the heavy gun. After a half day's firing from the 34-centimeter gun, air photographs indicated that the emplacement had been destroyed. The airmen undertook to demolish the other two emplacements and their photographs indicated that they had inflicted considerable damage. Apparently they did not secure any direct hits for the gun or guns continued to fire without any long intervals.

703. After the advance of the Allies it was impossible to determine from examination of the emplacement which had been nearest the allied lines whether a gun had actually been on this position or not. A German artillery officer who worked with the Americans for sometime in the forward area after the armistice and who spoke with such

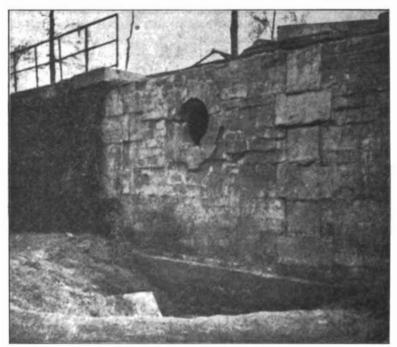
certain knowledge of the long range gun as to indicate that he knew the details of design and had seen it, insisted that the position that had been destroyed by the Allies had not had any gun on it.

704. Mention has already been made of the destruction of property by these long range projectiles. Except in a few places where the damage was so exposed as to attract attention, no matter how slight it might be, there was little evidence that the bombardment had any effect. On March 29, the day on which the second gun began to fire, and fired only four projectiles, the one projectile which landed within the city of Paris struck and knocked out the keystone of one of the arches in the roof of the Church of St. Gervais near the Hotel de Ville. The falling of the keystone caused a large part of the arch and the roof to collapse and most unfortunately the church was quite full of people at the time. Examination of the table below shows that this day holds the record for casualties. On one other occasion a projectile burst in the lobby of a hotel, killing a number of people, but doing comparatively little material damage. Some idea of the damage ordinarily wrought can be gained from examination of plate This shows the hole made by the explosion of one of the shells in the Garden of the Tuilleries. It will be noted that the wall is not damaged and that only a comparatively small hole has been made in the ground.

The bombardment of Paris by the German long-range gun, Mar. 28 to Aug. 9, 1918.

	Number of	projectiles.		
Dates.	Within the walls.	Outside the walls.	Killed.	Wounded
yr. 23	18	3	15	3
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25	1 4	. 2	1	
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30	1 4	5	13	
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PLATE 489



SHELL HOLE IN THE GARDEN OF THE TUILLERIES.

The bombardment of Paris by the German long-range gun, Mar. 25 to Aug. 9, 1918—Con.

		Number of	projectiles.		
	Dates.	Within the walls.	Outside the walls.	Killed.	Wounded
June	3. 4	3 1 1 2	1 2 3 2	2 4 1 8 1	10
Inly Aug.	11. 15. 16	18	1 1 7 4 4 4 10	6 3 32 8 7 1	6 8
	Total	193	120	256	65

705. Even during the active periods of the three series noted above there were many days on which the gun did not fire. It is quite certain that between the 25th and 29th of March the first gun was being removed and a new one placed on the carriage. By the end of the 25th of March 49 projectiles had arrived, and the probable life of the guns is not more than 50 rounds. It is likely that the guns were changed again between the 7th and 11th of April and between the 21st and 24th of April.

706. After the armistice it was learned that the Germans had constructed a total of seven guns. These guns were first constructed to a diameter of 21 centimeters (8.27 inches) and after being worn out as 21-centimeter guns were being rebored to 24 centimeters (9.45 inches). All of the projectiles of the first two series were 21 centimeters in diameter, but during the last days of the third series the projectiles were 24 centimeters in diameter, indicating that the entire seven guns had been worn out, and that probably the gun that had commenced firing on Paris on March 23 as a 21-centimeter gun had been rebored and was fired again as a 24-centimeter gun. It was learned also that the Germans were reboring the remainder of the seven guns and were constructing additional guns at Essen. Representatives of the Ordnance Department found in the Skoda Works at Pilsen three more guns which the engineer at these works said were under construction as long-range guns at the time of the armistice. In July, 1918, the Intelligence Service transmitted information to the effect that one gun had been destroyed by a premature explosion. No confirmation of this report has ever been found and it can not be considered a certainty.

707. The third series began on July 15 with 10 projectiles, followed by 4 projectiles on the 16th. The bombardment then ceased for three

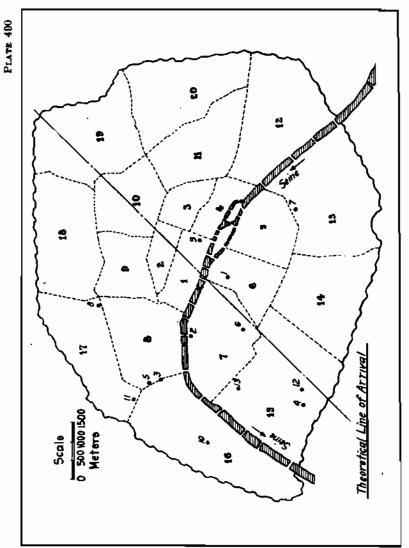
weeks, beginning again on August 5 and continuing daily until the 9th. On this day 12 projectiles arrived, only two of which fell within the walls of Paris. The famous bombardment was finished. A comparison of the distribution of the bursts on this last day, plate 490, with the locations on the first day, plate 488, is very interesting. On the first day a considerable portion of the projectiles fell within a very small area in the northeastern section of Paris. On this last day it will be observed that they are scattered over the eastern section of Paris and no two are very close together. The last projectiles of the entire bombardment fell between 1 and 2 o'clock on August 9. Already the Allies in their successful drive north of the Marne and between Soissons and Rheims were driving the Germans back so rapidly and had made such progress as to put the long-range guns in serious danger.

708. Plate 491 shows the location of all of the bursts within the walls of the city, a total of 183; 120 more fell outside the city, making a total of 303 fired from seven 21-centimeter guns and probably one gun rebored to 24 centimeters. The bombardment included 44 active days. Even before the last day of the bombardment American forces operating north of the Marne had captured an emplacement 9 kilometers (5 miles) north of Chateau-Thierry. This emplacement will be described in detail later. It was 86 kilometers (53.4 miles) from Paris and it is understood that it was a new emplacement from which the Germans had hoped to operate the super guns more effectively.

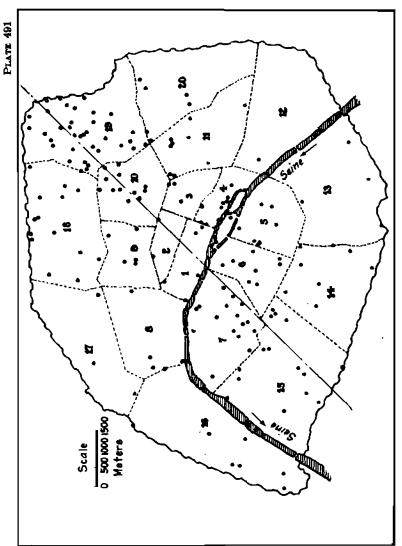
DESIGN OF THE GUN, CARRIAGE, AND EMPLACEMENT.

709. Introduction.—It has been mentioned before that the Germans used seven guns of a caliber of 21 centimeters (8.27 inches), that they had rebored at least one of them to 24 centimeters (9.45 inches), and that at the time of the armistice three more guns were under construction at the Skoda Ordnance Works at Pilsen in Austria. During the period of active warfare many reports were received with reference to the design of the gun, but never any information with reference to the carriage. The various reports on the gun agreed quite closely in the essential details.

710. In May, 1919, a commission of Ordnance officers was sent to the Skoda Works in Austria for the purpose of investigating their methods of constructing large and small ordnance. While there they secured additional data from the chief engineer of the plant with reference to the design of the gun, and saw the three guns which had been in process of construction on November 11, 1918. This chief engineer stated that when the first German gun began to fire on Paris, it was as much a surprise to the Austrians as it was to the Allies. Shortly thereafter he went to France to examine the gun and observed



LOCATION OF THE BURBTS ON AUGUST 5, 1918.

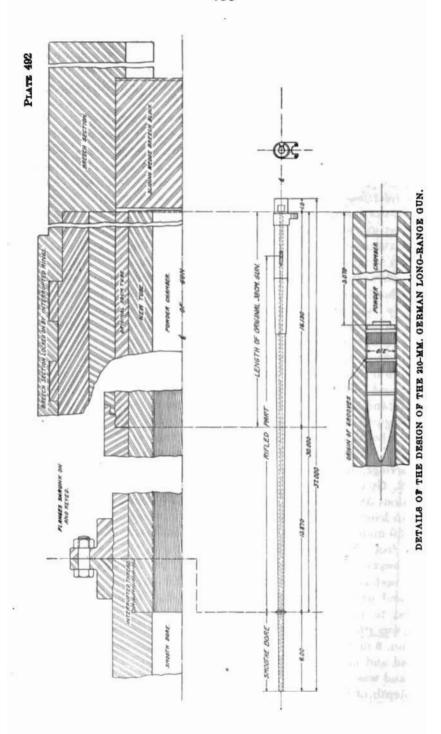


LOCATION OF ALL THE BURSTS WITHIN THE WALLS OF PABIS.

it in action. It was not until a few months before the armistice that the three guns were sent to Pilsen for conversion into long-range guns. Evidently the Germans had considered the bombardment a success, or sufficiently so to warrant the use of manufacturing facilities for the construction of a greater number of guns than they were able to handle at the Krupp Works at Essen.

711. The details of the design of the carriage for the gun were not learned until April, 1919, although it had been quite certain since August, 1918, that the emplacement found north of Chateau-Thierry was intended for the carriage of the long range gun. Until July 1. 1919, no direct information had been received from the Germans with reference to the design of any part of the entire mechanism except the gun on which, as mentioned before, information had been received at various times before the armistice; the guns themselves were examined at the Skoda Works at Pilsen. Just why the Germans refused to talk about this gun is not known. In December, January, and February, 1918 and 1919, a German engineer who was working with the American forces in the region northeast of Verdun helping identify long delay fuses and assisting on other technical matters said that he was acquainted with the design of the gun and had seen it in operation. Very curiously, however, he refused to give any information with reference to the details of the design; was quite positive in his assertions that the Allies would never see any of the guns, and certainly not any of the carriages. This was difficult to understand in view of his perfect willingness to talk about the details of design of any other piece of ordnance that he was at any time asked about, and it was more curious in view of the fact that there is really nothing wonderful about the design of the long-range gun, its carriage, or its emplacement.

712. Gun.-All of the long-range guns were constructed from worn-out 38-centimeter (15-inch), 45-caliber guns (17.1 meters or 56 feet in length). The converted gun was in two parts, the main section 30 meters (98.5 feet) in length and the forward section 6 meters (19.7 feet) in length. The 38-centimeter gun was bored out and a very heavy tube with inside diameter of 21 centimeters was inserted; 12.9 meters (42.3 feet) projected beyond the end of the original gun and over this projecting portion another hoop was shrunk and locked to the forward hoop of the old gun. This 21-centimeter tube was rifled at a uniform twist throughout its length. The other section, 6 meters in length, was attached by means of an interrupted thread and heavy outside collars or flanges. This section was unrifled and was of an inside diameter equal to 21 centimeters plus twice the depth of the grooves in the rifled section. It was assembled to the gun in the field and not removed until the gun had been worn out. The total weight of the original 38-centimeter gun was 152,550



pounds and the weight of the reconstructed gun approximately 318,000 pounds. The 21-centimeter liner was of such thickness that on being worn out at this caliber it could be rebored first to 24 centimeters (9.45 inches) and later to 26 centimeters (10.024 inches). Its probable life at any one caliber was not more than 50 rounds and the maximum powder pressure did not exceed 3,000 atmospheres or 44,000 pounds per square inch. The design of the breech mechanism of the original 38-centimeter gun did not require modification.

- 713. The long-range guns constructed by the British and French Governments do not follow the German design to the extent of having a smooth-bore section on the front. The purpose of this feature was for some time in doubt and is worthy of some discussion.
- 714. The gun just described is approximately 3 meters longer than either the British or French long-range guns, both of which are rifled throughout their length. Two reasons might be given for the extra section.
- 715. Possibly additional linear velocity was imparted to the projectile as it traveled through the 6-meter smoothbore section. seems improbable, however, that this could be its primary purpose. inasmuch as the muzzle velocity was such a variable quantity. is more probable that its purpose was to align the axis of the projectile more perfectly with the axis of the bore of the gun and reduce to a minimum the angular velocity of yaw as the projectile left the When it is understood that this projectile was to mount to a height of about 24 miles and travel a horizontal distance of 76 miles, it can easily be appreciated that any tendency that the projectile might have to throw its axis out of alignment with its theoretical path would have disastrous results. Through the impracticability of making projectiles fit perfectly in a gun, they have a tendency to hammer the walls as they travel down the bore. hammering action of the projectile is the result of the operation of two forces, the one tending to increase its linear velocity and the other to increase its rotational velocity. The latter force is acting only while it is traveling through the rifled section. It is invariably true that just as the projectile is leaving the ordinary gun it is on one of its up, down, or crosswise hammer strokes, and that the axis has a tendency to yaw or deviate from its theoretical path at a certain angular velocity. Cardboard screens placed in front of guns in proof firing invariably show elongated holes, and not infrequently very decidedly so, even at no greater distances than a hundred feet from the muzzle. This tendency to vaw has a detrimental effect on the accuracy of even our comparatively short-range guns, but no effective means have yet been devised to neutralize it. With the extreme range gun it is so much more serious that it seems quite likely that the Germans adopted this method of neutralizing it,

thereby reducing the dispersion both in range and in direction. It is not improbable that the German gun was first constructed without the smoothbore section and that its shooting was found to be so erratic as to require the addition of this feature.

716. This gun was operated at a muzzle velocity of from 1,500 meters (4,920 feet) to 1,600 meters (5,248 feet) per second and at an elevation of 55 degrees. This 55 degrees is worthy of comment inasmuch as it has ordinarily been supposed that nothing could be gained in range by elevating a gun above 45 degrees. It is known, of course, that if a projectile is fired in a vacuum its maximum range is attained when it starts at an elevation of 45 degrees. in the air, however, the initial angle which permits it to attain its maximum range depends both on the caliber and weight of the projectile, and the velocity at which it leaves the gun. With reasonably large and well-designed projectiles it may be said that for each muzzle velocity (A) there is a density of air (b) into which the projectile should enter at an approximate angle of 45 degrees. For this projectile and the muzzle velocity of 1,500 meters per second the initial angle is 55 degrees. It is very doubtful whether any additional range can be secured with any projectile at any muzzle velocity at an angle above 55 degrees.

717. Attention was called in the discussion of the first day's bombardment to the tremendous dispersion in range. Some of the projectiles fell just within the wall at the northeast side of Paris, and some within the walls at the southwest side. This is accounted for by the fact just mentioned, that the muzzle velocity of the projectile varied as much as 100 meters per second. It was impossible with the powder that the Germans were using to secure a muzzle velocity with a variation of less than 100 meters per second.

718. CRADLE.—The cradle is a cylinder of simple design having ribs at long intervals and of a depth of only about 3 centimeters, plate 410. The walls of the cylinder have a minimum thickness of 10 centimeters and a maximum thickness of 13 centimeters over the ribs. The diameter of the main trunnion is 46 centimeters, and the length 33.5 centimeters. A collapsible counterweight is attached to the top of the cradle. In firing, the two sections of this counterweight are raised and locked together for the purpose of raising the center of gravity to such an extent that the gun may be elevated and depressed more easily. This cradle is of a naval design, the front section being so shaped as to close the opening in a turret. It is not improbable that the cradle as well as most of the 38-centimeter guns were removed from German ships or coast fortifications.

719. RECOIL MECHANISM. -- The recoil mechanism is composed of two hydraulic recoil cylinders and one spring-pneumatic recuperator cylinder, all attached to the bottom of the cradle, plate 403. Each of

the recoil cylinders is a separate cylinder carried in brackets cast on the cradle, and each is provided with a buffer approximately 32 centimeters long. The plugs through which the cylinders are filled are on the ends of the buffers. The approximate length of recoil is 1.3 meters (50.5 inches). This distance is of course approximate and was arrived at after careful examination of the cradle. A report examined in the office of the Chief of Artillery of the Belgian Army at Brussels gives the length of recoil as 1.16 meters. Inquiry disclosed the fact that this length of recoil was approximate also.

720. Two rods screwed to the recoil lug of the gun, plates 403 and 405, and extending to the rear, carry a heavy crosshead to which the piston of the recuperator cylinder is attached. The recuperator cylinder is likewise a separate cylinder carried in brackets cast on the cradle. At the rear on both sides it is planed to serve as a guide for the recoil lug to prevent rotation of the gun.

721. ELEVATING MECHANISM.—The elevating mechanism of this mount is extremely heavy and unique in design. The cradle was evidently originally provided with the screw type of elevating mechanism, the screw being hinged to the cradle at the rear end.

- 722. The specification that the gun be provided with an elevation of 55 degrees necessarily led to the discarding of the screw mechanism. The straight racks shown on plates 400, 407, 408, 409 slide in ways which are parallel to the inclined forward ends of lower chords of the side girders. It was necessary to put them in this position to secure sufficient movement to attain 55 degrees. At the lower end they are connected with each other by a heavy shaft to which are attached the two connecting rods running up to the bottom of the cradle, plate 409. Provision is made for two handles on each side of the car, each for two men, plate 409, and a two-speed transmission is provided, permitting the mechanism to be operated at low or high speed. The ratio of the gearing at low speed is 41 turns of the handle for 1 degree of movement of the gun. It was not possible to determine the ratio of high speed since the two men making the examination could not operate it. It seems probable, however, that eight men could operate the mechanism at high speed without undue difficulty.
 - 723. TRAVERSING MECHANISM.—(See "Anchorage.")
- 724. Railway Car Body.—The railway car body shown on plates 400, 413, 415, 416 is made up of two single-web side girders connected at the front and rear by heavy structural steel transoms. They are further reenforced in the front by the heavy east-steel housing for the elevating gear. The trunnion seats are of cast steel and are simply bolted to the top chord with single-key plates at their rear. This single-key plate has the positive backing of one top-cover plate. The face of the horizontal section of the lower chord of the side girders is planed and is provided with key plates at each end, plate 416. Eight

2-inch holes are provided in each lower chord at the front end and six at the rear for bolting the mount to the emplacement.

725. Anchorage.—When the German army had retired from the salient between Soissons and Rheims in August, 1918, the emplacement shown on plates 417 and 418 was found in the Bois du Chatelet, 9 kilometers directly north of Chateau Thierry. This emplacement was in process of installation and had not been completely erected. The Germans attempted to destroy it, but succeeded only in ripping loose a few plates. At the time the emplacement was captured no description of any kind was available of the carriage for which it was intended. The writer's failure to find any emplacement in Belgium from which the mount examined there could be operated, led to further examination of the emplacement in France, and it was found that they fitted perfectly.

726. The emplacement is in two main sections, one a base and the other a rotating section. The rotating section, plates 419 and 420, is about 28 feet 6 inches in diameter and is supported on 112 8-inch steel balls. The base is about 35 feet in diameter and 6 feet in depth. On plate 417 there can be seen at right angles to the direction of the track of the rotating section two girders, on the ends of which are key plates or pads. The plate which is labeled has six holes in it and the plate on the opposite end of the girder has eight.

727. The mount is run onto the emplacement with the rotating section in the position shown in plate 420. It is then raised by the four jacks which can be seen at the left of plate 417, and are shown in their exact positions in plate 420. When the mount is raised the trucks are removed and the rotating section of the emplacement turned through 90 degrees. On lowering the mount onto the emplacement, the key plates on the bottom chords of the carriage are fitted to the corresponding key plates on the emplacement. The emplacement is shown in process of installation, with the Gantry crane still in place, plate 421.

728. The carriage on which the gun is so mounted as to be capable of movement in a vertical plane only, is traversed by rotating the top section of the emplacement. A complete circular traversing rack made up of angles and steel pins is bolted to the structural base, plate 422. A pinion carried on a vertical shaft on the side of the rotating section which corresponds to the rear of the carriage engages with this rack and the mechanism is driven by two-man handles on a horizontal shaft carrying a worm engaging with a worm wheel on the top of the vertical shaft, as shown at the right of the top view, figure 420. This shaft may likewise be driven by means of the four handles mounted on the two cases in the center of the rotating section and connected with the worm wheel and shaft through two shafts

carrying two universal joints each. Apparently the mount was generally traversed by means of these latter handles, if one may judge of the scheme of operation from plate 422.

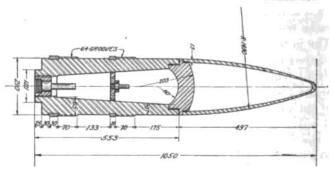
729. CAMOUFLAGE.—In the case of the emplacement found in the Bois du Chatelet, sockets were placed in the center of the approach track at intervals of about 30 feet, into which trees with trunks up to about 6 inches in diameter could be placed for the purpose of concealing these tracks. The Gantry crane, as well as the emplacement, while in the process of installation, were covered with tree branches, plate 421, and raffia nets were stretched over the mount from the trees on either side, plate 422.

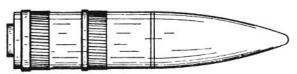
730. Trucks.—All of the trucks as well as the span bolsters are constructed entirely of structural steel, as shown on plate 423. The front trucks contain five axles each, and the rear trucks four axles each. The journals are approximately 14 centimeters in diameter by 22 centimeters in length. The wheels are 95 centimeters in diameter. On the front trucks three wheels are provided with two brake shoes each; on the rear trucks the end wheels are provided with two shoes each and the inner wheels with one shoe each. The braking is done by hand only. The axles are equalized in pairs only. The center axles of the front trucks have no connection with the others. On plate 400 a portion of a circular rail can be seen on the top of the front truck on which the pads attached to the span bolster on each side bear.

731. Ammunition Supply System.—The provisions made for supplying ammunition are shown on plates 424, 425, and 426. same provisions were used for the operation of the 38 centimeter, 45-caliber naval guns from which the long range guns were made. The extension of the car body shown on plate 426 was used for the operation of the 38-centimeter gun under certain conditions. was not required and was removed when the long-range gun was operated on the carriage. On plate 425 a removable plate can be seen between the shot truck rails. Above this removable plate is a light bridge in the center of which is seen a ball on the end of the cable used in hoisting projectiles through the hole in the floor. This cable runs over a series of pulleys to a small drum in the box on the top of the left side girder. The ammunition was supplied from the storehouse over the narrow-gauge track shown on plate 424, the circular portion of the track being under the opening in the center of the floor of the mount. The gear in the box on the side girder is of the double speed variety, the high speed being provided probably for rapid operation in the hoisting of powder.

732. Ammunition.—The projectile used with this gun is shown on plate 493. Its weight is 120 kilograms or 264 pounds. The length of the main portion of the projectile is 490 millimeters or approxi-

PLATE 493





DESIGN OF THE GERMAN LONG-RANGE PROJECTILE.

mately 19.3 inches. To this is attached a false ogive or cap, the exact length of which is not known; it is probably as long, if not slightly longer than the main portion of the projectile. The radius of the curve of this ogive is about 7 calibers or 58 inches. noted that the charge is separated into two parts by a diaphragm which has a number of holes in it. Two fuses are used, the one in the diaphragm and the other in the base. All of these projectiles are most carefully machined to elaborate specifications in order that the weight and dimensions might be practically exact and the center of gravity perfectly located; even after they are thus machined they are sorted out into lots according to their characteristics by weight, dimensions, and location of the center of gravity and the various lots of projectiles marked with center punch marks. The necessary corrections in elevation and deflection are calculated for the projectiles of these various lots. The projectiles which fell in Paris were successively marked with three center punch marks in a triangle or four center punch marks in a square, etc.; projectiles of the same marking arrived consecutively.

733. The outside of the projectile is provided with two copper bands which served as gas checks and in front of each of these copper bands the projectile is enlarged and rifled for a length of 70 millimeters (2.7 inches). The shear from the extreme acceleration necessary to produce the required muzzle velocity is such that the ordinary copper bands could not be made to serve as rotating bands. shearing strength of copper is not sufficient to stand the strain that would have been put on the bands with so great an acceleration. The friction between the lands of the gun and the projectile is so great as to wear the gun appreciably on each round fired. This was evident from examination of the copper bands of successive projectiles. As a result of the necessity for providing rifled projectiles, it is necessary in placing the projectiles in the bore of the gun to fit the forward rifled section of the projectile into the beginning of the rifling of the gun. plate 514. The exact details of the design of the portion of the tube between the beginning of the rifling and the powder chamber are not known. It seems quite probable, however, that there is a smooth section of about 12 inches into which the portion of the projectile back of the first copper band fits, bringing the base of the projectile to the end of the powder chamber. The fact that the forward rifled section of the projectile is already fitted into the grooves of the gun makes it certain that the rifled section at the rear would likewise fit as the projectile begins to move up the gun.

734. It has been noted before that this projectile departed at a muzzle velocity of from 1,500 to 1,600 meters per second. The velocity remaining on its arrival in Paris was approximately 700 meters per second and the time of flight about three minutes.

735. The analyses made of the various parts of the shell showed:

	Shell.	Cap holder,*	Cap.	Dis- phragm.•	Copper band.	Dunkirk sheils,
C	.0410 .0106 1.82-2.82 .83-1.45			.04	0, 12 . 21 99 67	

1 Practically a casting.

* Cast.

* Forging.

736. Not a single one of the 303 projectiles that fell in or about Paris failed to detonate. Evidently the two fuses were responsible for this excellent record. The practice of separating the charges into two parts by a diaphragm is not new. The diaphragm had been used before in French heavy projectiles as a guarantee against the effects of inertia which might either provoke a premature explosion in consequence of the friction of the molecules of the charge against each other or might bring the charge beyond the critical density point after which it would probably not detonate. At one time a theory was advanced to the effect that this diaphragm separated two liquids which mixed and detonated upon the fall of the projectile. There seems no good reason to believe that this could have been so.

737. Previous Designs and Limits in Design.—It has already been mentioned that investigation disclosed shortly after the beginning of the bombardment that an almost identical design had been proposed to the French Government not many years before. Further search of French and English records has brought to light the fact that the rifled projectile is quite old and seems to antedate the copper band considerably. In 1892 Sir Alfred Noble made a 100-caliber 6-inch gun which gave a muzzle velocity of 3,700 feet per second; in the same year the French Government constructed a 10-centimeter 80-caliber gun from which they attained almost the same muzzle velocity. It is not known what range was secured in either case. The forms of most standard projectiles at that time was not such, however, as to make it possible to secure the maximum range from the above noted velocity.

738. In taking up the design of such guns again the French and English services found that with guns of practicable length and muzzle velocities attainable with guns of such length, and with available powders, the projectile that would permit the greater range to be realized would be approximately 8 inches in diameter and weigh from 225 to 250 pounds. An appreciable change up or down in the diameter or the weight of the projectile would result in a loss

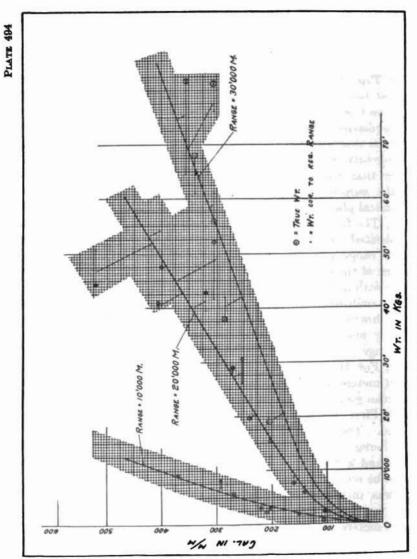
of range. The gun designed by one of our allies uses a projectile weighing 240 pounds and a powder charge of 350 pounds. One of the pieces of powder examined was about 2.5 feet in length and roughly elliptical in cross section, the axes being about 1 inch and one-half inch, respectively. It is interesting to note in this case that the powder charge has a weight about 50 per cent greater than that of the projectile. If the weight of the charge were increased, calculations indicate that most of the energy of the gas would be absorbed in the work of accelerating the charge rather than in accelerating the projectile and no greater muzzle velocity would be obtained.

739. One of the vital requirements made of the powder'is that it burns at a rate sufficiently slow to avoid excessive pressures and to give a uniform pressure through a large portion of the period of the travel of the projectile in the bore of the gun. The powder made by one of our allies for their long-range gun is in flat strips resembling cardboard. These strips are 3-ply, the various sections burning at different rates. The large sticks of powder mentioned above for the gun of the other of our allies is special and is expected to live up to the characteristics just noted.

APPENDIX II.

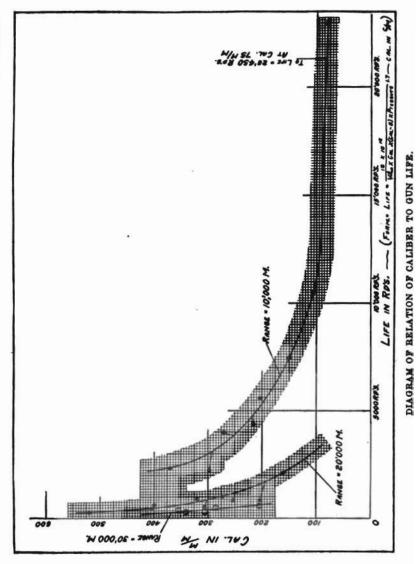
STUDY OF THE RELATIVE EFFICIENCY OF DIFFERENT CALIBERS.

- 740. Prior to the European war guns were not constructed above 50 or at most 55 calibers length, and, in general, for greater range, larger and larger calibers were employed. The German long-range gun emphasized the fact that such practice did not rest on any fundamental theoretical difficulty in making a smaller caliber shell carry to the greater range. The French, in their program for new guns of greater than the previous ranges, planned on fairly small calibers, and the question at once arises as to whether this is not a more economical plan than the old one of using a larger caliber.
- 741. The following calculations are based on the assumption that it is desired to shoot a certain total weight of projectiles across a certain range into enemy territory, and that for this purpose, on account of the nature of the target, the number and caliber is immaterial (within limits), provided the total weight is the same. This is the condition that is believed to exist for fire upon industrial establishments, railway yards, ammunition dumps, and the like—in fact, for most of the targets that are presented for destruction at long range.
- 742. For this purpose, the three ranges of 10,000, 20,000, and 30,000 meters were taken, and data were obtained on French and American guns shooting, at maximum elevation, to these ranges.
- 743. First, the relation between caliber and weight of piece was studied. This relation is shown by the curves of plate 494, one curve being given for each range. As practically no guns were found which had a maximum range exactly that considered, a correction had to be made in each case, as indicated on the curve, the weight of gun was increased or decreased proportionately as its maximum range was below or above the range in question (10,000, 20,000, or 30,000 meters).
- 744. Next, the relation of life in rounds and caliber was studied. Life was computed from the Jones formula, using a corrected velocity, obtained similarly to the corrected weight. That these values of life are near to the absolute correct life may be seriously questioned. But for comparison between the different guns at the larger calibers, they are probably quite close, plate 495.

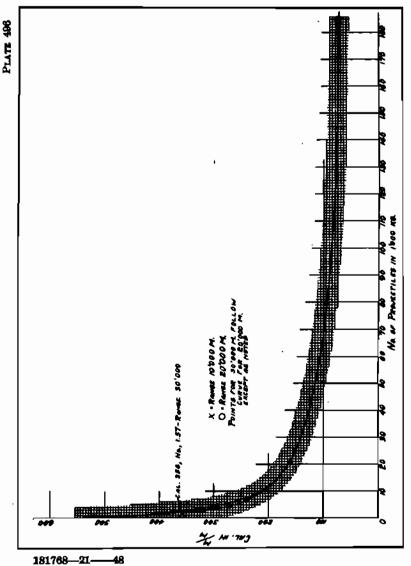


DESIGN OF RELATION OF CALIBER TO GUN WEIGHT.

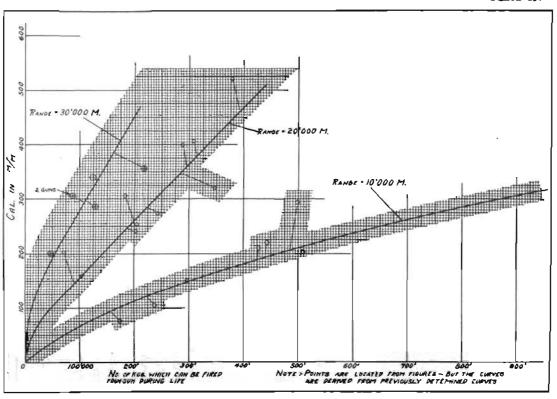




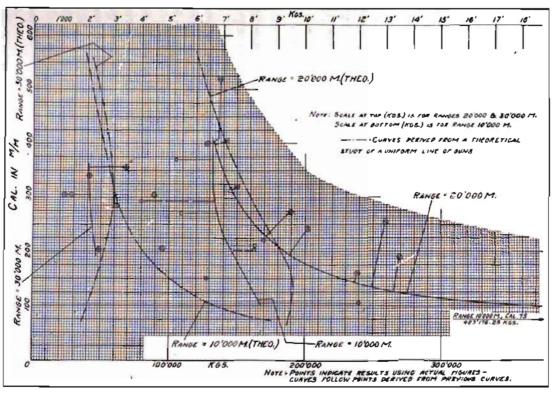
- 745. A standard of 1,000 kilograms is taken as the weight of projectile to be delivered on the target. The number of shots necessary to accomplish this delivery for different calibers is approximately a cube curve, and is plotted from actual values on plate 496.
- 746. From the preceding data, it is now possible to calculate the weight of projectiles which each gun can deliver before it is worn out. This is shown on plate 497, the points representing computations from the actual values for the preceding guns and the curves, computations from values read off the previous curves.
- 747. It is now assumed that the entire weight of metal in the guns is used up when it is worn out, or that it becomes ineffective. Hence, if we compute the total weight of projectiles which can be delivered by each caliber per 1,000 kilograms of gun wear (computed as above noted), we have a direct measure of the relative efficiency and economy of the different calibers of guns at different ranges. This has been computed and plotted on plate 498. On this diagram there are shown also similar curves derived from purely theoretical considerations on a line of similar guns.
 - 748. The conclusions from this are as follows:
- (a) At 10,000 meters, it is much more economical to deliver a given total weight of projectile with the smallest practicable caliber. A given weight of 75's will deliver during their life three times the weight of projectiles to this range that the same weight of 400's would deliver during their life.
- (b) At 20,000 meters, the same tendency is evident but to a somewhat smaller degree. The theoretical curves indicate about 150-millimeter caliber is most economical.
- (c) At 30,000 meters, the tendency has disappeared so far as the points from actual guns indicate, and the curve derived from previous curves indicates only a very small advantage in favor of the smaller calibers. The theoretical curve also shows little difference, but indicates maximum efficiency around 300 millimeters.
- 749. For the ranges and calibers considered for powerful railway artillery the above would indicate that there is a most efficient caliber from the standpoint of gun wear for each range. At the shorter ranges (20 kilometers) the smaller guns are most economical, but at the longer range (30 kilometers) economy does not vary greatly with caliber and therefore does not determine it. Very long guns of small caliber would seem to have about the same economy as shorter and more normal guns of larger caliber carrying to the same maximum range.
- 750. In order, possibly, to make clearer the steps by which the preceding curves were derived, the table below is given of the various values computed for the 20,000-meter curve, from a theoretical standpoint.



RELATION OF CALIBER TO NUMBER OF PROJECTILES IN 1,000 KILOORAMS.



RELATION OF CALIBER TO WEIGHT OF PROJECTILES PER LIFE OF GUN.



RELATION OF CALIBER TO WEIGHT OF PROJECTILES PER 1,000 KILOGRAMS OF WEAR OF GUN,

Calculations for 20,000 meter range.

Cal. in inches.	Weight projectile, lbs.	Velocity, meters per sec.	Velocity, foot p. s.	Travel projectile, iu.	Weight gun, lbs.	Life gun, rounds.	Kgs. projectile delivered during life.	Kgs. projectile delivered per 1,000 kgs. gun.
1	2	3	4	5	6	7	8	•
3	15 108 438 1,200 2,330	1, 145 770 882 592 558	8,755 2,525 2,170 1,942 1,830	235 191 206 231 253	4, 239 13, 752 41, 200 90, 552 223, 146	2,668 1,210 762 596 413	16, 153 59, 975 151, 397 323, 653 623, 816	9,460 9,502 8,100 7,800 6,163

Column 1 is assumed to give a good point distribution. Column 2 is assumed from standard projectiles. Column 3 is taken from ballistic curves prepared by Capt. Kent. Column 4 is merely a translation of column 3 to English units.

751. Column 5 is found by assuming that the same maximum pressure, 38,000 pounds per square inch, and the same type of expansion, giving the same average pressure, will be used on all guns. A consideration of the mechanics of the problems will show that, under these circumstances, the travel is equal to

Constant × weight of projectile × velocity² caliber²

The value of the constant is found from a study of existing guns using the maximum pressure in question and the travel is computed from the formula and recorded as shown.

- 752. Column 6: It is assumed that the weight of any of a line of similar guns will vary as the travel of the projectile multiplied by the square of the caliber. A constant derived from practice is used to get the actual weight in each case.
- 753. Column 7: The life of the gun is computed in each case from Jones's formula, elsewhere mentioned. In this case, however, a correction has been applied, based on recorded lives of French guns, so that the tendency is to lengthen the life on large calibers and shorten it on small as compared with the values given by Jones's formula. It is thought these revised figures are more nearly correct than those gotten directly from the formula.
- 754. Column 8 is the product of columns 2 and 7 and the factor for converting pounds to kilograms.
- 755. Column 9 is column 8 divided by the weight of the gun in thousands of kilograms (derived from column 6). This figure is a direct measure of the efficiency of the gun in delivering projectiles to the range in question.

APPENDIX III.

A REPORT ON THE GERMAN DEFENSES ON THE COAST OF BELGIUM (44).

PURPOSES OF INVESTIGATION AND SOURCES OF INFORMATION.

756. The investigation on which the following report is made was made primarily for the purpose of determining whether the Germans had followed fixed policies in the designs of the various mechanisms of their heavy gun carriages. With ordnance designers, there have been a number of questions on which there has been a sharp difference of opinion. Some believe that the cradles of heavy guns should be heavily braced by ribs, while others feel that there is no reason why they should not be simple smooth cylinders. Some designers are in favor of a front pintle type of carriage with simple friction bearings, or at best, roller bearings with racers of small diameter and more or less crude wheels or large rollers at the rear of the carriage on which it may be traversed. Others believe in a central pintle type of carriage with large roller paths. It is seen at once that there is a vast difference in the difficulties involved in the manufacture of carriages designed under these different principles. Cradles with heavy ribs on the outside are difficult to cast, and do not lend themselves to rapid manufacture. If smooth cylinders will answer just as well, it does not seem wise to hamper the manufacturer with the other design. Front pintle carriages are in general easier to manufacture than the center pintle type, hence unless there is something very vital to be gained in the central pintle type of carriage with its large and difficult to manufacture roller paths, it would seem that the first design should have preference.

757. In this investigation, the methods of reducing the friction of the trunnions, the designs of the elevating and traversing mechanisms, the ammunition supply system, as well as the design of the guns, were studied.

758. A report has been made on these same coast defenses from the standpoint of the problems of the coast artilleryman by Majors Armstrong and Norton. This report is dated December, 1918, and was published in the Artillery Journal in three parts, the last appearing in August, 1919.

755

759. Information contained herein was secured through study of reports in the offices of Gen. Arnoulde in Brussels, through conversation with Gen. Arnoulde, through inspection of all of the guns and carriages discussed, from discussion with French officers who have inspected the same material, and from the "Renseignements de l'Artillerie" of January and February, 1919.

760. The writer wishes to acknowledge his indebtedness to Lieut. Gen. Arnoulde, Chief of Artillery of the Belgian Army, for the courtesy extended by him for this inspection. Acknowledgment is made likewise of the excellent service of Sergt. J. P. Ferris, who assisted on this inspection.

HISTORY OF THE INSTALLATION.

761. The coast of Belgium was occupied by the Germans during the month of October, 1914. They occupied Ostend on October 15. It is probable that they at once installed some minor caliber guns for its defense against landing parties, but the evidence available indicates that the major caliber guns described in this report were installed during the years of 1916 and 1917, in preparation for and support of their major submarine campaign.

762. When the writer was with the British Fourth Army at Ypres in February, 1918, he was told by the British ordnance officers of that army that they had received very authentic reports to the effect that the Germans had been rapidly dismantling their second navy and were mounting the guns on railway carriages for both coast defense and land service. The 28-centimeter guns on railway mounts that were operated in the Batteries Preussen, Hanover, and one other battery not indicated on the map, were probably some of the guns removed from the second navy. The emplacements for these railway mounts did not make their appearance in the air photographs until the year 1918.

763. It is likely that the 38-centimeter gun, Battery Pommern, near Leugenboom, was placed primarily for the purpose of bombarding Dunkirk and Ypres. Both of these places were heavily shelled by a gun of this caliber during the years 1916 and 1917. Battery Goeben, at Zeebrugge, was made up of four complete turrets. In this battery the original turret equipment was complete even to the inclusion of the ammunition hoists, electrical traversing mechanism, etc.

764. During the spring of 1918, April 23, an attempt was made to block the harbors of Zeebrugge and Ostend. The mole at Zeebrugge was pierced and the boat, *Vindictive*, loaded with concrete, was placed across the entrance of the Ostend harbor. The boats engaged in these undertakings received terrific punishment, but apparently accomplished their mission. It seems probable that had the Allies cared to make the sacrifice, it would have been possible to force either

harbor, although it is not very likely that they could have retained possession of them for any great length of time. At the time of the inspection of these defenses, the writer observed the *Vindictive* still at the entrance to the Ostend harbor. It had been raised and moved to a position as close as possible to and parallel with the north side of the entrance.

765. It is significant to note that when it became necessary for the Germans to evacuate this area in August, September, and October, 1918, the only artillery that they were able to get out was the railway artillery. From the inhabitants of Ostend it was learned that all of the batteries in that vicinity had been operated quite continuously against the allied land forces for some days before the evacuation.

766. Just before the area was evacuated all the guns were destroyed with the exception of the 38-centimeter gun at Leugenboom. One method seems to have been employed on all of the guns for their destruction. In most cases they removed the rotating band from one projectile and rammed it up into the bore of the gun. A second projectile was then rammed in and the gun fired. When the rear projectile struck the forward projectile it exploded, and in every case except in the Battery Pommern, as noted above, the breech of the gun was completely blown off and in most cases the carriage practically wrecked. In some cases the forward projectile likewise exploded, swelling or tearing off the muzzle of the gun; in other cases it was simply projected a short distance out of the gun. The guns and carriages after being wrecked were practically valueless, and no attempt was made to keep them in condition.

GEOGRAPHICAL PLAN OF THE DEFENSE, SCOPE OF SERVICE, ETC.

767. The distribution of the guns of various calibers along the entire Belgian coast is shown on plate 499. Plate 500 shows somewhat better the distribution of the batteries about Ostend.

768. It is improbable that the Germans installed any considerable number of guns along this coast until it was definitely decided to inaugurate their major submarine campaign. It was vital that they have a convenient base for these submarines as close as possible to their theater of operations. The harbors at Zeebrugge and Ostend are neither very large, but both are quite ample for submarines, and both are connected by large canals with Bruges, where the submarines could be maintained. The fortifications, hence, centered about two ports, Ostend and Zeebrugge, with the battery Pommern some distance out of Ostend and placed primarily for land service. It will be noted, plate 500, that the smaller guns were all installed upon the top of the dune that parallels the coast, while the heavy guns were all placed a kilometer or more back of the dune. Except for the dune, the land along the coast is quite level—so much so, in

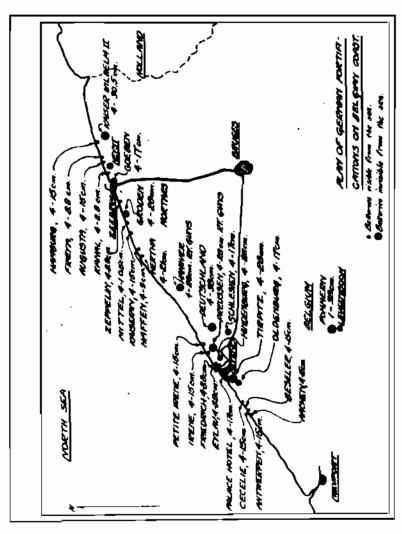
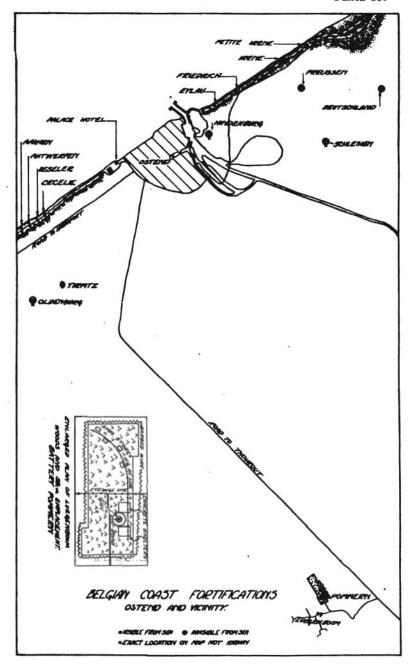


PLATE 499

PLATE 500



fact, that it is inclined to be swampy unless well drained. The guns on the dunes ranged from 8.8 to 17 centimeters, the 8.8 centimeter guns being for service against aircraft. For the heavy batteries located behind the dunes, there were heavily constructed concrete observation stations in the dunes. The stations for the batteries centered about Ostend were located one in front of the Royal Palace Hotel (near the Palace Hotel Battery) and the other in the dune near the Battery "Petite Irene."

769. All of the batteries shown on plate 499 by solid dots were located on top of the dunes and were visible from the sea. Those batteries indicated by solid dots inclosed in rings were behind the dunes and had to depend upon the stations located in the dunes for their observation. The Palace Hotel Battery of 17-centimeter guns was installed on the broad promenade just in front of the Royal Palace Hotel. This battery was particularly conspicuous. Battery Tirpitz just south of the city of Ostend was located in very swampy land, and it is understood that a great number of piles had to be driven to render the concrete emplacement stable. Considerable attention was paid to the drainage of the region around this battery and Battery Oldenburg. All of the other inland batteries were installed on comparatively dry and solid ground. The Battery Pommern, southeast of Ostend, was located on the eastern edge of a small wood known as the Bois de Leugenboom. There is no evidence that this battery was ever used against any except land targets.

770. DAMAGE FROM SHELL FIRE AND BOMBS.—In spice of the fact that a majority of the batteries were located on top of the dunes and in plain sight of the sea, there is no evidence that any of them were damaged by shell fire. It is probable that no firing was done against the Palace Hotel Battery because of the damage that would be done the large buildings roundabout. It is understood on good authority that the allied ships paid constant attention to both those batteries installed on the dunes, as well as those located behind the dunes. As early as 1916 the exact locations of practically every battery behind the dunes were determined from airplanes. Some of the pictures taken of some of these batteries are shown on plates 510. 518, and 528. Other photographs are available of the remaining inland batteries. It is understood that the monitors came in within a few kilometers of the coast at night, camouflaging their gunfire by blinding flares. It is reported that on practically all occasions when the ships shelled the coast fortifications during the day heavy smoke screens were at once set up by the Germans which evidently afforded effective protection. Just back of the Battery Irene, between the dune and road, the writer found a large number of steel pots or cylinders 18 inches in diameter by 24 inches in height, which had been used by the Germans in setting up their smoke screens.

The writer saw many of the holes made by airplane bombs and shown on plate 529, but could not find any single case in which either the inland batteries or the batteries in the dunes had been struck by shell firing from sea or by bombs dropped by airplanes.

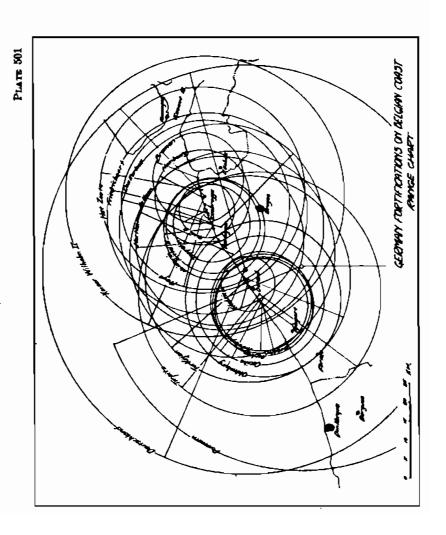
771. It is understood that the British monitors controlled their fire by the scheme of triangulation. Knowing that the Germans would at once set up a smoke screen between the batteries fired upon and the monitors firing, they were in the habit of placing one boat of inconspicuous construction a great distance off to serve as observer. This observing boat was so located as to be able to see behind the smoke screen. For firing on the heavier batteries, behind the dunes, it was of course necessary to operate by indirect fire.

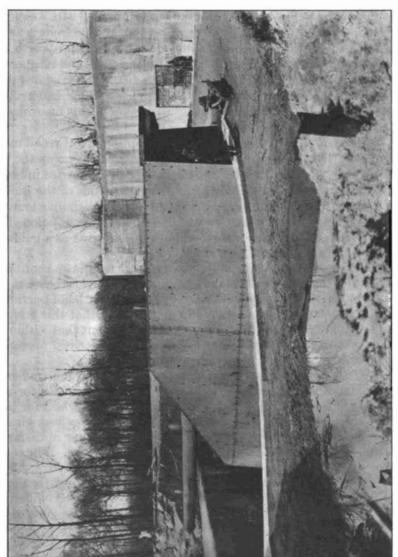
772. Scope of Service.—The range and scope of service of the various batteries is shown on plate 501. All of the guns, except the 38-centimeter gun Pommern at Leugenboom, were capable of being traversed 360 degrees. The range of 55 kilometers reported for the Deutschland seems extreme. Various reports conflict in this respect, some crediting the batteries with a range of 42 kilometers, some with a range of 47 kilometers, and the last report, given in the Bulletin Renseignements de l'Artillerie of January and February, 1919, with 55 kilometers. The ranges given on plate 501 are in accordance with the report in the bulletin just mentioned.

DISCUSSION OF THE MECHANISMS. 38-CENTIMETER GUN BATTERY PÖMMERN (45).

773. Gun.—This battery, plate 502, consisted of but one gun. model 1914, Krupp, No. 15 L. Its weight is 77,530 kilograms, over-all length 17.13 meters, and length from breech block to the muzzle, 16.13 meters, giving it an effective length of 42 calibers. It seems to be rated in some reports as a 45-caliber gun. This rating is evidently based on its over-all length. There are 100 grooves, and the twist of the rifling is to the right 1 centimeter in 10. The diameter of the powder chamber is 42.5 centimeters, and the outside diameter of the breech 1 meter. The breech is of the usual Krupp sliding wedge type and its mechanism is identical with that on the 38 centimeter gun on the railway mount. The design of the gun is likewise identical with that of the gun on the railway mount, and with the 38centimeter guns of the battery Deutschland, plate 506. On this plate it will be observed that the breech section has been blown away. The scheme of attaching the breech section by the interrupted ring method is well shown. As in the case of the railway mount, the recoil lug has a bearing at the bottom on the two sides of the recuperator cylinder to prevent rotation of the gun.

774. CRADLE.—The cradle is a cylinder of simple design, having ribs at long intervals and a depth of only about 3 centimeters. The





38-CM. GUN, GERMAN BATTERY POMMERN.

walls of the cylinder have a minimum thickness of 10 centimeters and a maximum thickness of 13 centimeters over the ribs. The diameter of the main trunnion, plate 503, is 46 centimeters and the length 33.5 centimeters; the diameter of the small trunnion 20 and the length 19 centimeters. It will be observed that the antifriction mechanism is of the rolling wedge type. This cradle was provided with a counterweight identical with that shown on plate 506, and its front is so designed as to close the opening in the turret. Its total length is 3 meters, and it is provided with brackets for the recoil and recuperator cylinders on the bottom as shown in plate 403. The cradle is lined with a bronze liner, approximately 6 millimeters thick and 1 meter in length both at the front and rear. A portion of this liner may be seen on plate 506.

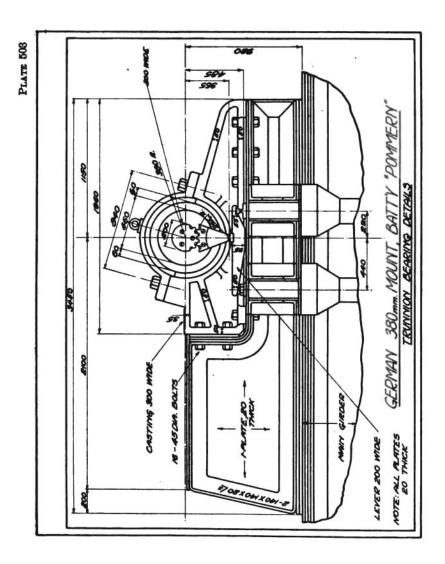
775. RECOIL MECHANISM.—For the description of the recoil mechanism, see "Recoil mechanism" of the 38-centimeter gun on the railway mount. The two recoil cylinders, plate 403, are carried in brackets on either side and the filling plugs are on the ends of the buffers. The recuperator cylinder is carried in the center in similar brackets and likewise has a filling plug on its forward end. As mentioned before, its rear end, which is planed on both sides, serves as a guide for the breech lug to prevent rotation of the gun.

776. ELEVATING MECHANISM.—See the same for the 38-centimeter guns of the Battery Deutschland. The only difference between the two is that in this battery there was no provision for hand operation. The report found in Gen. Arnoulde's office stated that this gun had been originally provided for hand operation only, but that within the last year it had been equipped with motors for electrical operation. The maximum elevation obtainable is 45 degrees.

777. Traversing Mechanism.—See description of the traversing mechanism of the Battery Deutschland. There is provision for both hand and power operation of this mechanism. The wheel for hand operation, however, is located on the left of the carriage very close to and on a level with the traversing rack. It is 1 meter in diameter. The maximum traverse provided for is about 157 degrees. The center line of this field of fire passes approximately through Dunkirk.

778. CARRIAGE.—See detailed description of the carriage for the 38-centimeter guns of the Battery Deutschland. The only difference between these carriages is in the armor provided on the guns of the Battery Pommern. This will be described later under the heading of "Protection."

779. EMPLACEMENT.—The emplacement for this carriage is of exceedingly massive concrete construction. The diameter of the central pit or well in which the carriage is placed is approximately 22.439 meters. The form of the pit is not a complete circle, but is so shaped as to allow the carriage to traverse 157 degrees. The



depth to the level of the traversing rack is 3 meters and the additional depth to the floor on which the center pintle rests 1.5 meters, making a total depth of 4.5 meters. On either side are practically identical concrete structures for the housing of ammunition and personnel. The structure on the right is for projectiles and tools. Between these two structures at the front, plate 502, there is a concrete parapet 2 meters high and 3 meters thick. The earth slopes gradually away from the top of the parapet at the front, dropping about to the level of the main floor of the emplacement on which men are seen standing. The thickness of the roof of the structures on the right and left is 3 meters, the total height above the floor being 5.5 meters.

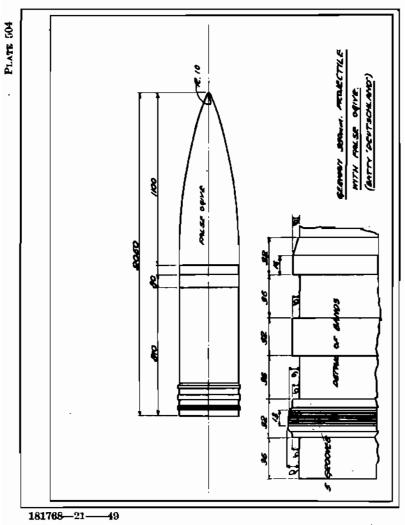
780. Ammunition and Ammunition Supply System. - As just noted under the heading of "Emplacement" the projectiles were stored in the concrete storehouse on the right and the powder in the storehouse on the left. Three weights of projectiles were used, one of which is shown on plate 504. This projectile has a false ogive. The ammunition was supplied entirely by hand, the shot truck being of the design shown on plate 505. The arrangement of the storehouse is in general similar to that for the 305-millimeter gun of the Battery Kaiser Wilhelm II, plate 517, the projectiles being piled two high. Gen. Arnoulde's report states that the projectiles were rammed by 12 men and that the rate of fire was one shot in five minutes with electrical operation of the elevating mechanism, and one shot in 10 minutes with hand operation of the elevating mecha-Gen. Arnoulde's report further states that according to reports of people living at Leugenboom, the personnel originally provided for operation of the mount when it was operated by hand was 1 captain, 2 lieutenants, 10 noncommissioned officers, and 160 men. After provision was made for electrical operation of the various mechanisms, the personnel was reduced to 1 captain, 2 lieutenants. 5 or 6 noncommissioned officers, and 70 men.

781. The shells fired by the 38-centimeter gun are:

Name.	Weight.	Puse.	Range.
H. E. 38 cm. Sp. Gr. L/4.1 Bds., with base fuse. H. E. 38 cm. Sp. Gr. L/3.6 m. Bds. (m Haube), with false ogive and base fuse. H. E. 38 cm. Sp. Gr. L/4 Bds. A. Kz (m Haube), with double fuse at head and base false ogive.	696 kg. (600 without false ogive).	8p. Gran. K	44 km.

The charges are three in number:

- (a) Hutzenkartasch, cartridge containing 87 kg.
- (b) Vorkartasche, charge containing 96 kg.
- (c) Vorkartasche, charge containing 118 kg.



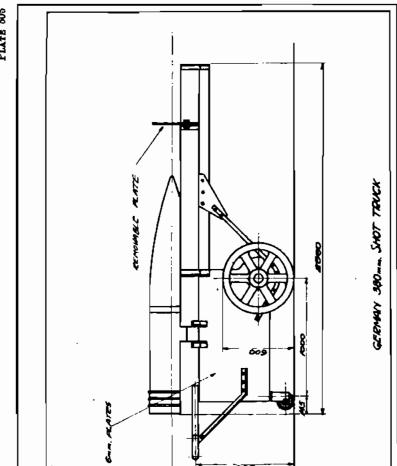


PLATE 505

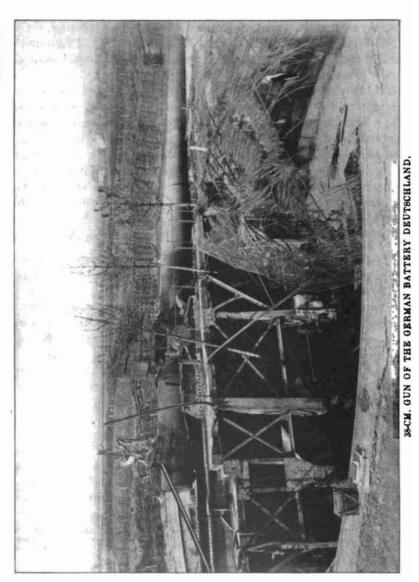
It seems then that the gun can fire with two charges; that is:

- (1) 87 kg. plus 118 kg. 205 kg.
- (2) 87 kg. plus 118 kg. plus 96 kg. 301 kg.
- 782. PROTECTION.—To protect the personnel operating this gun against aircraft bombs and aircraft machine—gun fire, the carriage was covered with 6-centimeter flat armor. This plating extended to within a few centimeters of the floor of the pit. The hole in the front through which the guns extend is sealed by the small shield on the front of the cradle.
- 783. Discussion. On plate 502 it will be observed that the parapet just in front of the gun has been blown away in the center. There is evidence to the effect that the Germans used their characteristic method in attempting to destroy this gun, but that in this case neither projectile detonated until they struck the parapet in front. Neither projectile could be found, hence it is assumed that both detonated. The gun was damaged only to a slight extent at the muzzle, where some fragments of the projectiles were blown back into the bore, scoring it deeply.

38-CENTIMETER GUNS, BATTERY DEUTSCHLAND.

- 784. Gun.—See description of the 38-centimeter gun of the Battery Pommern. The design of these four guns is identical with the design of the model 1914 Krupp gun, No. 15-L. The gun, plate 506, is a model 1916, No. 36-L. Its weight is given as 77,562 kilograms. This gun is No. 4 of the battery; No. 3 is likewise a model 1916, and numbered 35-L. Gun No. 2 is model 1916, No. 41-L, and gun No. 1 is model 1914 No. 9-L.
- 785. Each of these guns had been destroyed by the characteristic German method of placing one projectile in the bore of the gun and firing another projectile into it. This procedure had resulted, in this case, in the blowing off of the entire breech and in the wrecking of the carriage. There was little evidence that any of these guns had been used to any great extent. The lands and grooves were in well-nigh perfect shape: at least, it was evident that such damage as was visible had not been caused through ordinary fire. The width of the lands is 6 millimeters, and the depth of the grooves 3 millimeters. In connection with the procedure in destroying the guns, reference is made to plate 532, on which is shown one of the projectiles from which the band had been removed. This projectile was found beside gun No. 3.
- 786. CRADLE.—The cradle on each of these four guns is identical in design with that of the 38-centimeter gun of the Battery Pommern and of the 38-centimeter gun of the railway mount. The counterweight on the cradle of the railway mount is collapsible. The counterweights on the Battery Pommern and Battery Deutschland cradles are as shown on plate 506. The one point of difference be-

PLATE 506



tween the cradles of three of these guns and the cradle of the gun on the Battery Pommern is in the lack of any provision for the reduction of the friction of the trunnions. On plate 506 it will be observed that there are no auxiliary trunnions and no friction reducing mechanism. There was no friction reducing mechanism on guns Nos. 2, 3, and 4, but gun No. 1 had a friction reducing mechanism identical with that of Battery Pommern, plate 503. This omission of anti-friction devices on guns Nos. 2, 3, and 4, which, by the way, are model 1916 guns, can hardly be attributed to the tack of time for the installation, since the small amount of machine work necessary in the shop might have been handled without difficulty, and the work finished in the field if desired. Apparently they preferred to rely on a surplus of man power in elevating their guns.

787. RECOIL MECHANISM.—The recoil mechanism is composed of two recoil cylinders and one spring pneumatic recuperator cylinder all located at the bottom of the cradle. It is identical in design with the recoil mechanisms of the Battery Pommern gun and the 38-centimeter railway mount, plate 404.

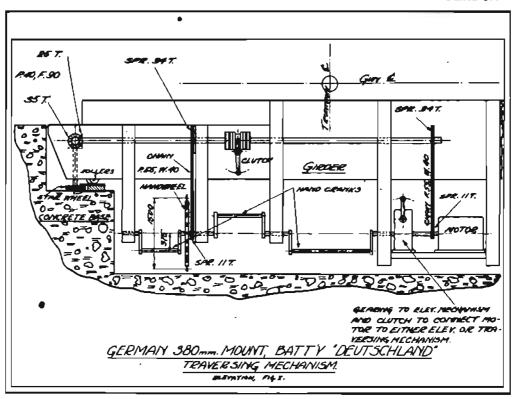
788. ELEVATING MECHANISM.—The elevating mechanism on all of these guns, as well as on the 38-centimeter gun of the Battery Pommern, is composed of two large telescoping screws, the larger screw passing through a nut carried in the crosshead at the bottom of the cradle, plate 506. On this plate the larger of the elevating screws can be seen about in line with one of the elevating and traversing handles at the bottom of the carriage. The larger of these two screws is about 24 centimeters in diameter and the smaller about 15 centimeters. The large nut in the crosshead is driven either from the motor, or by the hand mechanism which is used likewise for the traversing mechanism.

789. The maximum elevation at which the gun is operated is not known. There were no elevating arcs remaining on any of the cradles that would indicate to what extent it could be elevated. It is assumed, however, that the maximum elevation obtainable is the same as that in the Battery Pommern gun, which is 45 degrees. On plate 506 the motor driving the elevating and traversing mechanisms is hidden by the wire camouflage which has fallen. The box just to the rear of the camouflage is the housing for the clutch connecting the elevating mechanism with either the motor or the hand drive. All of this mechanism is duplicated on the left side of the carriage.

790. Traversing Mechanism.—The various details of the traversing mechanism are shown on plates 507 and 508. Provision is made for its operation by hand as well as by motor. This hand mechanism is operated by eight men.

791. The rear of the carriage is supported on two heavy rollers 96 centimeters in diameter by 23 centimeters on the face, which are carried on 21-centimeter spindles. A complete circular steel bearing





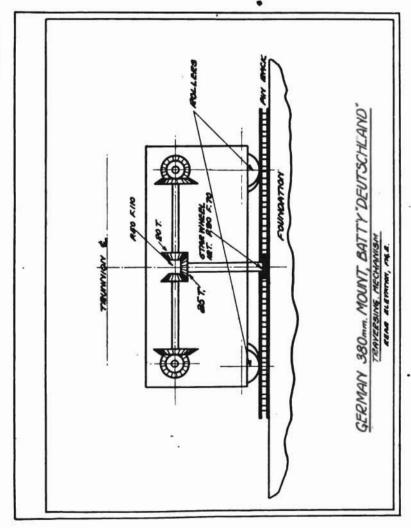
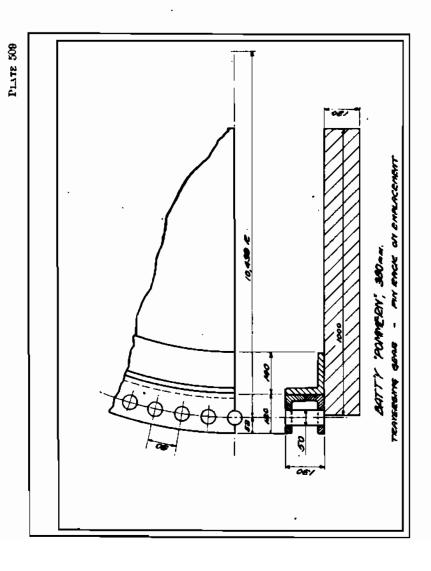


plate is boited to the first shelf of the pit. This plate is 12 centimeters thick by 1 meter in width and to its outer edge, plate 509, is bolted a traversing arc made of 3 angles and a series of 5-centimeter steel pins. The star traversing pinion, 21 centimeters outside diameter, meshes with this rack and is driven by either the motor or the hand mechanism. The radius to the center of the traversing rack is 10.439 meters.

792. Carriage. -- The carriage is entirely of structural steel, plate It is of the front pintle type, the front being carried on steel The hall path is 2 meters in diameter and the balls 15 centimeters in diameter. It is assumed that some provision is made for direct contact between the racer and base to transmit the horizontal component of the force of recoil into the foundation. possible to see the details of construction to confirm this supposition. Examination of some other carriages of similar design indicated that at least in some cases the racer was simply permitted to climb the balls when the gun was fired, no provision being made for positive contact. As noted under "Traversing mechanism," the rear of the carriage is supported on two rollers 96 centimeters in diameter. These rollers have a face of 23 centimeters and are carried on steel spindles 21 centimeters in diameter. The distance between the centers of these journals is approximately 3.3 meters. The rollers . appeared to be perfectly cylindrical, with rounded edges. struction of this carriage for one of their heaviest guns is exceedingly simple. The only heavy castings are those for the pintle, the elevating cross head, and the trunnion bearing. The only parts of the entire mechanism which obviously require fine machine work are the trunnion bearings, the heavy steel balls, and the ball paths.

793. EMPLACEMENT.—With the omission of the heavy concrete structures described under Battery Pommern for ammunition and personnel, the emplacements for the Batteries Pommern and Deutschland are nearly identical. Battery Pommern was finally fitted up for electrical operation only, and most of the mechanism for hand operations is removed. In the lower part of the Battery Deutschland pit a wood floor made up in sectors raised the floor to such an extent that the men operating the traversing and elevating mechanisms would be on the proper level. As seen in plate 506 the pit was filled with water at the time of the inspection to such an extent that these sectors had come loose and were floating. The emplacement provided for 360 degrees traverse of the carriage as against 157 degrees for the Battery Pommern.

794. AMMUNITION SUPPLY SYSTEM.—See description of the ammunition supply system for the Battery Pommern. There was no evidence of any provision of any mechanical handling of the projectiles except in the lifting of them from the floor to the storehouse and placing



them on the shot trucks. Between guns Nos. 2 and 3 of this battery, there was found a practice shell ramming tray somewhat similar to that shown on plate 517 for the Battery Kaiser Wilhelm II. This tray was made of a steel trough about 10 feet long with an ordinary railway car buffer at the end. In the tray there was a rather blunt nosed projectile with its rotating band removed. This projectile had evidently been used for practice in ramming.

795. Protection.—It is significant to note with reference to the three of the newest of these guns, that is, Nos. 2, 3, and 4, that there was absolutely no protection provided either for the gun carriage or personnel. Evidence of their scheme of camouflage can still be seen This camouflage was unable to hide the guns from the on plate 506. air photographers since photographs taken on August 9, 1916, plate 510, showed the emplacements quite plainly. In spite of this fact. there was no evidence to the effect that any of the guns or emplacements had ever been damaged by either shell fire from sea or by bombs from the air. Several holes that had been made, either by bombs or by shells, were visible in the fields in front of the guns. Gun No. 1 was protected with 6-centimeter armor in the same fashion as the gun of Battery Pommern. Gun No. 1 of this battery and the 28-centimeter gun of the Battery Pommern are identical in design throughout. Both are model 1914 guns, and it is probable that the hand elevating and traversing mechanism of the Pommern gun was identical with those of the Deutschland guns before the electrical equipment was provided.

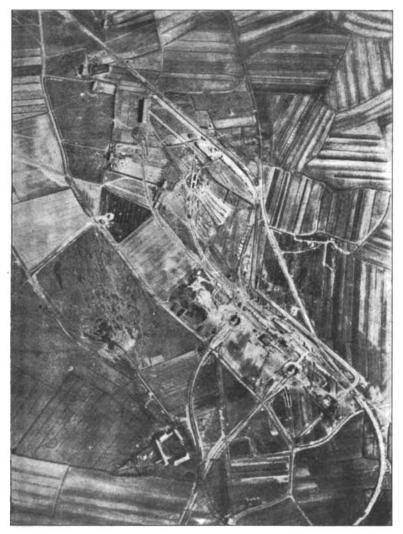
796. Discussion.—Significant points with reference to this battery are that guns Nos. 2, 3, and 4 are not provided with either trunnion antifriction device or positive protection in the form of steel armor.

305-MILLIMETER GUN, BATTERY KAISER WILHELM II.

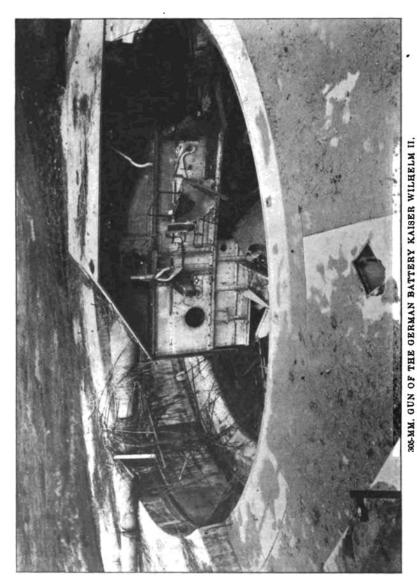
797. Gun.—With each of these four guns, plate 511, the scheme of destruction was so effective that it was impossible to find a breech after a half day's search. It is assumed that they were of a model at least as late as 1916. The Bulletin de Renseignements de l'Artillerie states that they were 50 calibers in length. One breech block was found; this was of the usual Krupp sliding wedge type. There were 88 grooves and the twist of the rifling is to the right 1 centimeter in 10 centimeters. Projectiles found in the storehouse and shown on plate 574 have two rotating bands from which it may be assumed that the pitch of the rifling is uniform.

798. CRADLE.—The cradles for all of these guns are smooth cylinders, the walls of which are 10 centimeters thick. The brackets at the bottom of the cradle provided for the recoil and recuperator cylinders, are quite similar to those shown on plate 419 of the 38-centimeter gun. The front of the cradle is provided with shield, plate 552,

PLATE 510



AIR PHOTOGRAPH OF THE GERMAN 38-CM. BATTERY DEUTSCHLAND (TAKEN AUGUST 9, 1916).



which closes the opening in the armor; it is not improbable that these were likewise some of the guns removed from the second navy. The cradle is likewise provided with a heavy counterweight which can also be seen on plate 403. The antifriction device, plate 512, is of the rolling wedge type. It is significant that in this case the auxiliary trunnion is very little less in diameter than the main trunnion. In practically all other cases observed, the diameter of the small trunnion was approximately one-half of the diameter of the large trunnion.

799. RECOIL MECHANISM.—The recoil mechanism for this gun is in general a duplicate of that shown on plate 403 for the 38-centimeter gun. The breech lug with the method of attaching the recoil pistons, and the bearing of the lug on the recuperator cylinder to prevent rotation of the gun are shown on plate 515. In contrast to the 38-centimeter gun in which the recoil pistons pass through holes in the recoil lug and the recoil lug hears on two planed sides of the recuperator cylinder, it will be observed in this case that the lug is slotted on the sides to receive the recoil pistons and the bearing on the recuperator cylinder is circular instead of flat.

800. The outside diameter of the recoil cylinder is 38 centimeters and the length is 1.68 meters. The diameter of the piston is 15 centimeters and the length of recoil 1.37 meters. These cylinders are both smooth forgings with flanges at the front bearing against the cast bracket on the cradle. There was no evidence of a counter-recoil buffer. On the front end of the cylinders, there are filling plugs similar to those found on the 38-centimeter cradles. The single recuperator cylinder is likewise a smooth forging with one large flange on its forward end. It is of the combined air-spring type and is approximately 45.6 centimeters in diameter by 4.25 meters in length. This cylinder likewise has a filling plug at the front end.

801. This is a timely opportunity to mention a fact that seems to the writer quite striking. Although the Germans follow, in general, fixed policies in their designs, their methods of application differ very widely. Apparently general specifications are given to the manufacturers who are permitted to modify them in details to suit their convenience. It does not seem probable that any designer or groups of designers would make such radical differences in the design of the details of their mechanisms as is evident on these guns and carriages. This is even more striking on their 21, 24 and 28-centimeter railway mounts.

802. ELEVATING MECHANISM.—The elevating mechanism for these guns is in principle the same as the elevating mechanism for the 38-centimeter railway mount. The design of its details are, however, quite different, plates 513 and 514. Apparently it was operated entirely by hand. There are two two-man handles below the

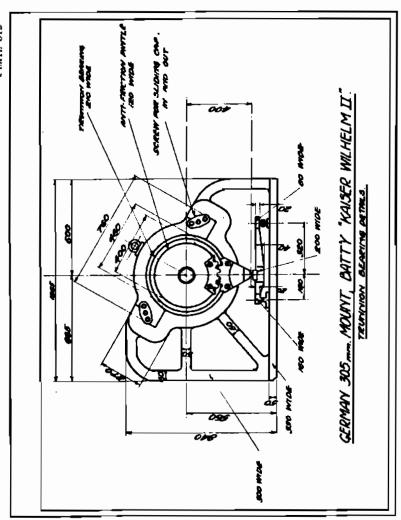
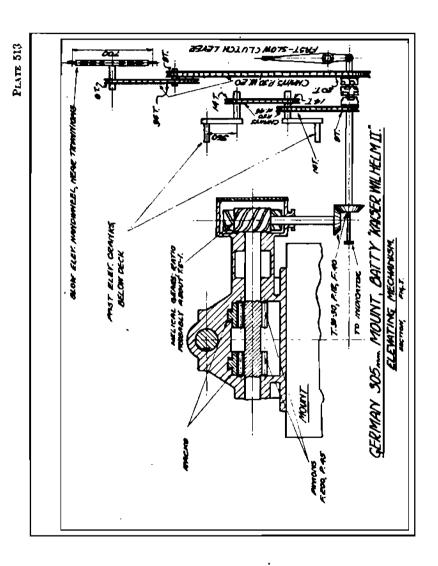
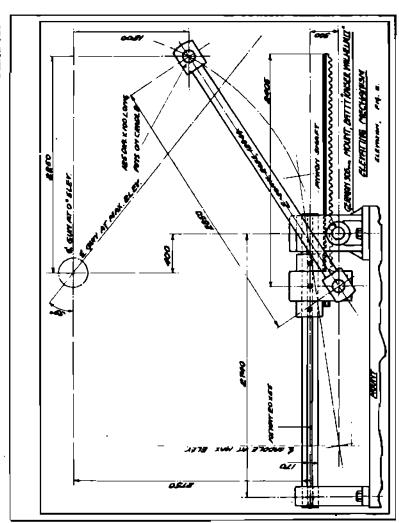


PLATE 512





deck of the carriage for rapid elevation and above the deck a single handwheel of large diameter for final and careful setting. The clutch for shifting from the low gear to the high is located below deck. Motion is transmitted from the handwheels to the horizontal shaft at the bottom and through the bevel and helical gears to the two pinions on the main horizontal elevating shaft. The two straight racks, which in this case are horizontal, plate 513, are connected to the crosshead which slides on a single round shaft as a guide. This crosshead in turn transmits motion to the gun through the two connecting rods. The two racks have guides on the top which slide in ways in the forward support of the main horizontal guide shaft, plate 554. It was not possible to elevate the gun, and the ratio of the gearing is not This mechanism, together with its companion mechanism on the 38-centimeter railway mount, are quite unique among the mechanisms observed on all German artillery. The reasons for the design seen on the railway mount seem obvious, but the same reasons do not hold for this carriage. Certainly, a simpler mechanism of equal efficiency could have been provided. The maximum elevation obtainable is 45 degrees.

803. Traversing Mechanism.—The traversing mechanism, figures 1 and 2, plate 515, is operated both by hand and motor. The roller track set in the concrete emplacement is shown in figure 1. In this case, contrary to the design of the same mechanism for the Battery Pommern and Deutschland, there is no traversing rack provided in connection with the roller track. Motion is transmitted through chains and gears from the motor or handwheel to the traversing pinion which meshes with the two gears bolted to the faces of the traversing rollers, figure 2. The simplicity of this mechanism is very striking, especially for guns of this size. Apparently, it worked satisfactorily, or it would not have been retained in a gun of such value. It is certainly worthy of serious consideration for similar carriages for our own service. An azimuth circle is embedded in the vertical walls of the concrete emplacement about 2 feet from the top, plate 512. An indicator is provided on the rear of the carriage, with a vertical wire quite close to this azimuth circle. The switchboard and seat for the traversing operator are located beside this indicator.

804. Carriage.—The carriages are constructed entirely of structural steel. The side girders are in three main sections, comprising a central section of uniform depth, a top brace for the trunnion support, and a bottom section for the pintle, plate 511. The pintle design is shown in figure 1 of plate 515. It is ball bearing, the balls being about 15 centimeters in diameter. In this case the racer serves as a pintle, having a positive bearing against the base ring for the transmission of the horizontal component of the force of recoil into the foundation.

LEVERS 4LATCH HOLD SHILL FOR BRANK CYL. BREEKH LUG, SHOWING METHOD GWID-MSTON ROOM SHOT TRUCK BATTY "KAISER WILHELM IT, 305 BENEMY AGAMST CYL. 11.0 C.STEEL DASE DETAILS SECTION OF EMPLACEMENT CONCRETE PIT ROLLER TRACK 6. BALLS TRAVI SING GENE

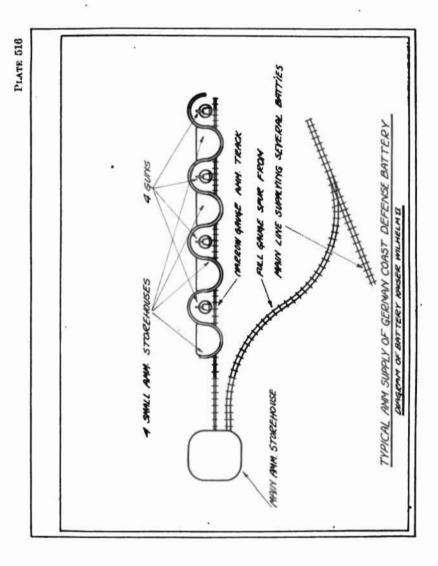
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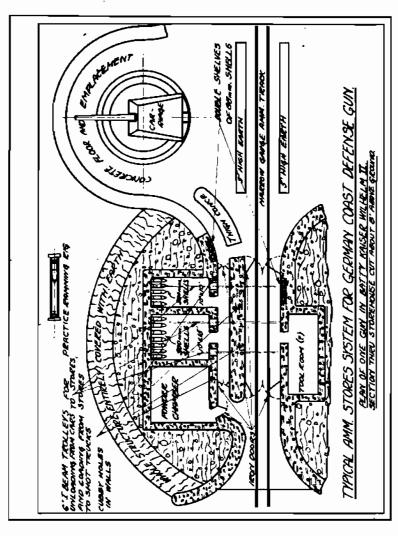
805. Ammunition Supply System.—The general plan of the Battery Kaiser Wilhelm II is shown on plate 516. Storehouses are located on the left of each gun and the main storehouse is 100 meters to the left of the battery. The narrow-gauge line shown extending from the main storehouse, passes through each auxiliary storehouse. A typical plan of one gun and its storehouse is given on plate 511. The double narrow-gauge lines shown passing through the storehouse are the same as those shown on plate 517. These storehouses are of excellent construction and are typical of the design of the storehouses for most of the heavy batteries inspected. The plan for the Battery Deutschland was almost identical. The external plan for the Battery Pommern was slightly different, but the interior arrangement was well nigh the same.

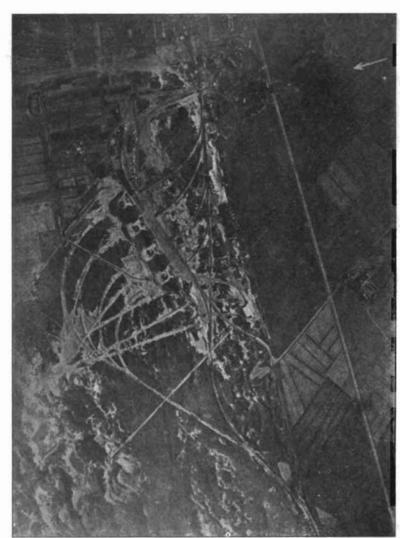
806. Projectiles are transported from the main storehouse to the individual storehouses on narrow-gauge railway trucks. From these trucks they are carried by means of an overhead trolley through openings in the walls into the projectile rooms, where they are stacked two high. Later they are picked up and carried by the same trolley into the corridor just outside the shell room and placed on the shot trucks, figure 4, plate 514. The table of this truck is quite broad and the shell is placed on one side where it is held by two arms until it is to be rammed. The truck is provided with a shelf, presumably for powder. There was no evidence of any scheme of handling the ammunition except by hand. The rammer found beside one of the guns is of such a length as to indicate that the projectile was probably rammed by eight men. The guns are loaded at zero elevation. Another practice shell-ramming tray, plate 517, was found beside one of the emplacements.

807. EMPLACEMENT.—The design of the emplacement for these guns is shown on plate 511. It will be observed that all the space about the gun leading to the ammunition storehouse is floored with concrete. In this respect the emplacement differs from that of the Battery Deutschland in which the concrete work did not extend much beyond the vertical walls of the pit. It is not known just why the walls of the pit are higher in front than in the rear. There seems to be no particular reason for it. The depth of the pit to the roller path is 2.4 meters, and the total depth 3.6 meters.

808. Protection.—Each of the four guns of this battery is protected with 6-centimeter flat armor. The guns and carriages were likewise elaborately camouflaged to hide them from the sight of the airmen, but air photographs taken on August 9, 1916, plate 518, indicate that it was perfectly possible to see the emplacements. In spite of all this there was no evidence that any of these guns, carriages, or emplacements had ever been damaged by shell fire from sea or by bombs from airplanes. Some holes were visible some distance



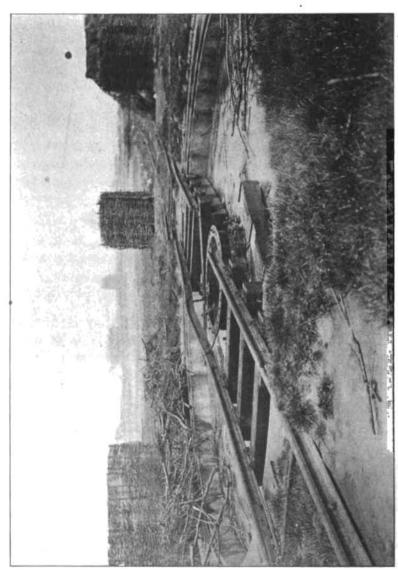




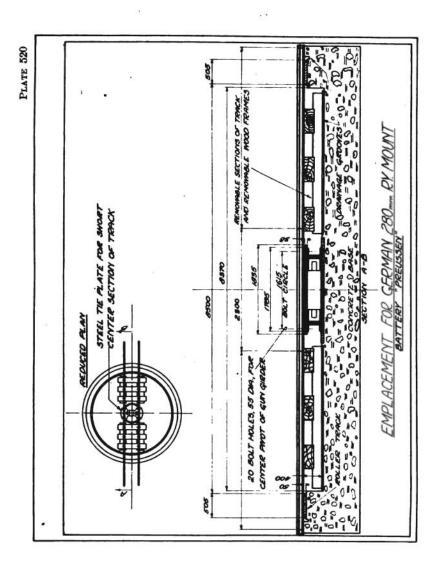
in front of the emplacements which may have been made by either bombs or shells. A few similar shell holes were visible some distance to the rear.

28-CENTIMETER GUN RAILWAY MOUNT, BATTERY PREUSSEN.

- 809. Gun, Cradle, Recoil Mechanism, Elevating Mechanism.—See description of the same for the 28-centimeter Railway Mount, paragraph 367 to 380.
- 810. Traversing Mechanism.—A description of the details of the mechanism attached to the mount is given under the description of the traversing mechanism for the railway mount. The writer had not had the opportunity to examine the concrete emplacement at the time the description of the railway mount, plate 386, was written. The emplacement shown on plate 519 is typical of the 12 emplacements provided for the three 4-gun batteries along the Belgian coast. There was a steel plate on top of the central base section which was blown off when the Cermans were demolishing their fortifications. The standard-gauge track extends a short distance beyond the emplacement, for the forward truck when removed from the mount. It was mentioned under the 28, 24, and 21 centimeter railway mounts that the carriages were so designed that they could all be used on the same emplacement.
- 811. The auxiliary sections of track that are laid inside the emplacement for the placing of the gun are shown on plate 519. As soon as the gun is in position, the central sections of rail, one piece of which is shown removed, are removed and the base section of the pivot dropped and bolted in place. The carriage is then raised a few inches by means of the jacks shown with the mount, plate 386, and the trucks removed. The short sections of track within the emplacement are likewise removed and the rear of the carriage let down until the traversing rollers rested on the roller path.
- 812. Carriage.—The details of design of the carriage have been fully described in paragraph 373.
- 813. EMPLACEMENT.—The various details of the emplacement are shown on plates 519 to 521. The two short central sections of rail, figure 1, plate 520, are connected by a steel plate which rests on top of the base for support as the mount passes over. Some curious markings on the vertical wall of the pit are shown on plate 521. The central vertical line is obtained approximately by passing through the center of the emplacement a line perpendicular to the general line of the coast. The distance between the vertical graduations labeled 0-50 and 50-100 is about 2 feet, and the total angular distance covered from the center to the graduation 250 is about 60 degrees. A complete azimuth circle was found painted at the outer edge of the roller track. This circle, however, could not have been



EMPLACEMENT OF THE 28-CM. RAILWAY BATTERY PREUSSEN.



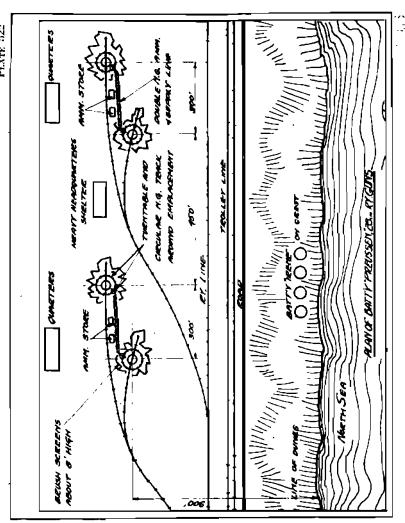
O AT MONT APPROXY MAGTELY OPPOSITE TO GENERAL LINE OF COAST GERMAN EBOMM RY GUN EMPLACEMENT, PARUSSEN MANTED GEROUATIONS ON NEPTICAL WALLS ON OPPOSITE SIDE OF EMPLACE-MENT. NEITHER IS CONTINUED NOTE: IDENTICAL GENOUNTIONS ABOVE 250.

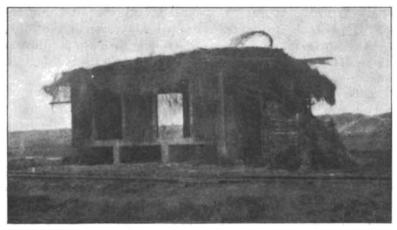
used, except for the approximate laying of the gun, since it was not made with sufficient accuracy. It seems more probable that the mount was laid in azimuth from some aiming point.

- \$14. The general location of the emplacements with reference to the main railway line on which the mounts were brought in and likewise with reference to the coast line is shown on plate 522. Two spur lines were run in from the main line. t is not quite clear why this was done; it would obviously have been possible to run short lines to the two guns on the left from the spur line in the center connecting the main line with the two guns on the right of the plate.
- 815. Ammunition Supply System.—The location of the ammunition storehouses and the narrow-gauge connection with the emplacements is shown on plate F22. In each case the standard-gauge line runs at the rear of the quite simple concrete storage houses which are provided with two doors both at the front and at the rear, plate 523. The powder is kept in the one storehouse and the shells in the other. A double line of 30-centimeter track connects the storehouses with the two emplacements. These narrow-gauge lines connect with turntables just inside the wicker protection. A complete circle of narrowgauge track is provided about each emplacement, making it possible to supply the shells to the mount in any position. There was no evidence of any scheme of storing the projectiles or powder closer to the mounts than the storehouses. Evidently a sufficient number of shot trucks are provided for these narrow-gauge lines that the shells can be provided directly from the storehouses at the maximum firing rate of the gun. The ammunition storehouses were well camouflaged. plate 522, but in spite of this camouflage air photographs taken in 1918 indicate clearly the position of all of the guns as well as the storehouse.
- 816. Protection.—The gun crew was protected to a certain extent by the light sheet metal cab on the mount, plate 386. The mounts were likewise well screened with wire and brush, remains of which can be seen on plate 519. In spite of this camouflage air photographs showed quite clearly the positions of the emplacements. There was no evidence of damage from shell fire or air bombs on the emplacements or storehouses. A heavy concrete headquarters shelter with telephone connections from the observation stations in the dunes and telephone connections to the various guns was provided between the pairs of guns. In each case there is a cable through the central pintle base which evidently carries the telephone connections between headquarters and the mount.

28-CENTIMETER GUN, BATTERY TIRPITZ.

817. Gun.—Battery Tirpitz is a four-gun battery and all of the guns are of model 1911. The gun of the four which was examined in detail was model 1911, No. 5. Its weight is 33,875 kilograms.





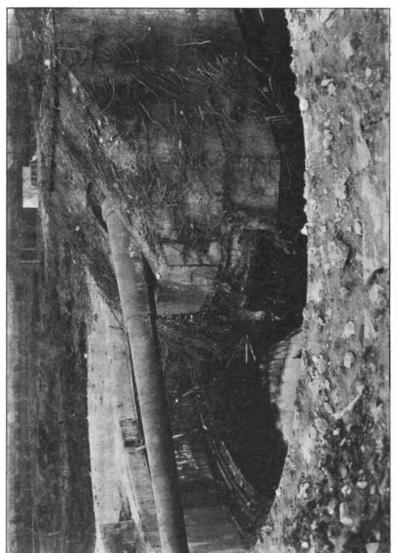
AMMUNITION STOREHOUSE OF THE 28-CM. RAILWAY BATTERY PREUSSEN.

The length of the tube from the face of the breechblock to the muzzle is 11.220 meters, and the over-all length of the gun is 11.950 meters. There are 80 grooves, and the twist of the rifling is to the right 1 centimeter in 10 centimeters. The diameter of the powder chamber is 30 centimeters. The breech is of the usual Krupp sliding wedge type. As with the 38-centimeter gun found on the railway mount, the tube of this gun has lengthened from firing, thereby separating the forward hoop a noticeable distance from the hoop to the rear, plate 524. Apparently, these hoops are not locked to each other. The lower extension of the breech lug, plate 525, is machined to bear against the planed inner surfaces of the lower recuperator cylinders, thereby preventing rotation of the gun. The gun did not show signs of very great wear, both the lands and the grooves being quite sharp.

818. CRADLE.—The cradle is a smooth cylinder, the walls of which are 10 centimeters thick. It is lined with bronze liners about 6 millimeters thick by 1 meter in length, at both the forward and rear ends. The trunnions are located noticeably close to the forward end. The antifriction device is of the rolling wedge type illustrated on plate 511. There were no unusual features in this design, and no sketch has been made.

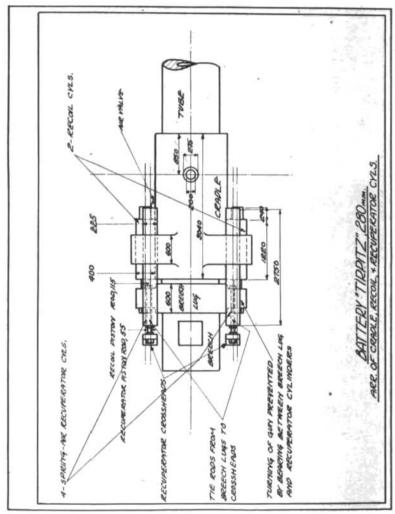
819. Recoil Mechanism.—The recoil mechanism, plate 525, comprises two recoil cylinders located on the top and bottom of the cradle and four recuperator cylinders. The two recoil cylinders are smooth forgings carried in the cast brackets on the top and bottom of the cradle. Their length, not including the buffer, is 1.22 meters, and the length of the buffer is 24 centimeters. The piston rods, 11.5 centimeters in diameter, pass through holes in the extensions of the breech lug. The length of recoil is approximately 76 centimeters. The four recuperator cylinders are placed symmetrically above and below; the upper cylinders are combined spring and air recuperators, while the lower are spring only. A common air line is connected to the valves on the forward ends of the upper two cylinders. It is believed that the air is supplied from bottles since there was no evidence of an air pump about the carriage. Both above and below, two rods connect the extensions of the breech lug with the crossheads attached to the piston rods of the recuperator cylinders. These rods taper from 4 centimeters at the crosshead to 5 centimeters at the breech lug, and are turned down to 4 centimeters through the breech lug. This design strikes one as being close to the limit of safety as it placed these rods, which are not of very great diameter, always under compression.

820. ELEVATING MECHANISM.—The general design of the elevating mechanism is shown on plate 526. It is operated by hand power only and the ratio of the gearing, as indicated, is five turns of the



28-CM, GUN OF THE BATTERY TIRPITZ,

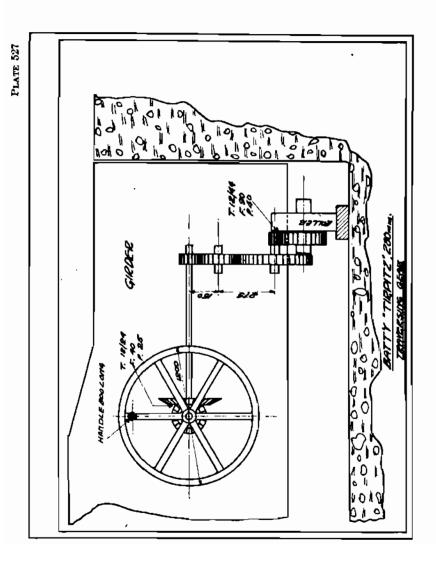
PLATE 525

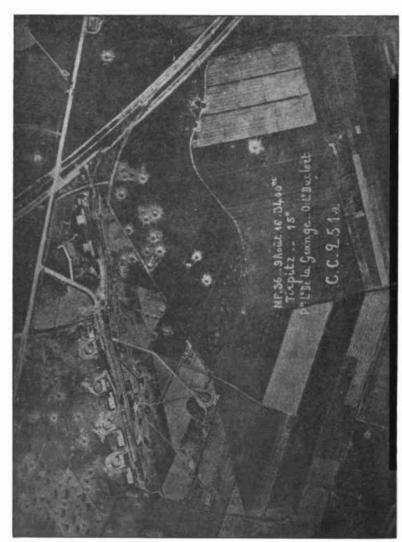




handwheel for four degrees of elevation. The elevating rack is double, although cast in one piece. Identical pinions on the same shaft and of the dimensions shown mesh with these racks. The range of elevation is from zero to 45 degrees.

- 821. Traversing Mechanism.—The traversing mechanism is quite similar to that found on the guns of the Battery Kaiser Wilhelm II. Details of this traversing mechanism are shown on plate 527. As with the 305-millimeter battery, there is no traversing rack attached to the roller path. The operation is by hand only from a large handwheel located on the left side of the carriage and about on a level with the roller path. In the case of the 305-millimeter carriages the single pinion meshed with spur gears attached to the face of the two large rollers. In this case, the motion from the large handwheel is transmitted directly to only one of the four rollers on which the rear of the carriage is supported. Although the mechanism was seriously damaged, it was possible to traverse the carriage just far enough to indicate that one man could operate the mechanism without difficulty.
- 822. Carriage.—It was not possible to secure such a photograph of these mounts as would show satisfactorily the construction of the carriage. In general, the design is not unlike that of the carriages for the 305-millimeter guns. There are two main girders, each of which is in three sections, a central section of uniform depth, a top section for the trunnion support, and a bottom section carrying the pivot. It is made of standard structural plates and angles throughout. The racer is attached to a heavy yoke which is supported by its trunnions in heavy trunnion bearings attached to the carriage. The design of the racer connection with the carriage is not at all unlike that found on the 28, 24, and 21 centimeter railway mounts.
- 823. EMPLACEMENT.—The emplacement is quite similar to that already described for the 305-millimeter guns. The traversing roller path is practically identical and the general dimensions of the pit are nearly the same. Again there is a raised section of concrete in front of the gun, the purpose of, or necessity for, which is not clearly understood. It is understood that unusual difficulties were encountered in constructing these emplacements, inasmuch as the ground is quite swampy, and it was necessary to drive numerous piles in order that the emplacement might be sufficiently stable.
- 824. Ammunition Supply System.—The ammunition supply system for this battery is quite similar to that shown and described for the 305-millimeter gun. The shot trucks are of the same design.
- 825. Protection.—Each of these four guns is armored with 6-centimeter flat armor. In spite of the camouflage, the remains of which can be seen on plate 524, legible air photographs were secured on August 9, 1916, plate 528. The camouflage is carried on a framework attached to the carriage and rotates with it. Most of the con-



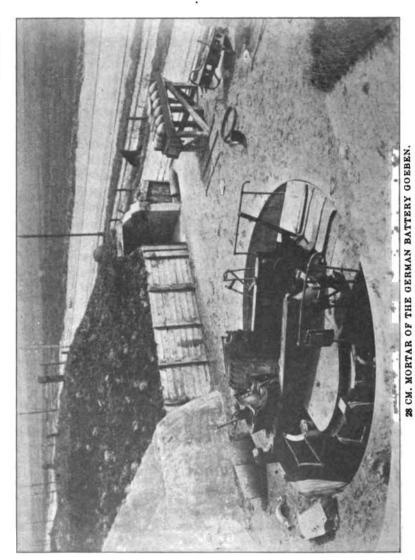


AIR PHOTOGRAPH OF THE 28 CM. BATTERY TIRPITZ (TAKEN AUGUST 9, 1916).

crete work about the guns is completely demolished, but there is no evidence that would indicate to the writer that any of the destruction had been effected by shell fire from the sea. It is certain at least that none of the carriages had been so struck or damaged. There are numerous holes to the front and rear of the batteries that were probably made by air bombs.

28-CENTIMETER MORTAR BATTERY GRODEN.

- 826. Top Carriage.—These mortars are supported directly by means of trunnions on a structural steel top carriage of the design shown on plate 529. This carriage was supported on the inclined sides of the main carriage by means of four rollers, two on each side.
- 827. RECOIL MECHANISM.—The recoil mechanism, which does not show very clearly on plate 529, comprises two recoil cylinders, the pistons of which were attached to the forward ends of the main carriage body; the cylinders are carried in the sides of the top carriage. The length of recoil is estimated as 1 meter, the gun returning to battery by force of gravity. On the front of the main carriage, there are four buffers, each made up of seven pairs of Belleville washers, 15 centimeters in diameter by 5 millimeters in thickness.
- 828. ELEVATING MECHANISM.—The elevating mechanism comprises a single circular rack bolted to the gun and meshing with a single pinion on a horizontal shaft in the top carriage. The handwheel operating the elevating mechanism is located on the right side of the carriage on a platform rotating with the carriage. On the end of the horizontal shaft in the top carriage, there is a worm wheel meshing with the worm carried on a long shaft parallel to the inclined rails on which the top carriage rolls. The worm is simply keyed to the shaft, moving with the top carriage as it recoils. This is the only elevating mechanism observed in which a slip friction device is provided. This slip friction device provides for the slipping of the worm on the end of the horizontal shaft through the top carriage. It includes two sets of Belleville washers.
- 829. Traversing Mechanism.—The traversing mechanism is made up of one rack attached to the base ring, a traversing pinion, vertical shaft, and simple spur gear mechanism leading to the handwheel. There is nothing unusual in the design and from the condition of the carriage, it was impossible to traverse it to learn the ratio of the gearing. The extent of traverse is 360 degrees.
- 830. Carriage.—It is believed that the carriage is shown in such detail on plate 529 as to make any lengthy description unnecessary. The diameter of the ball path is 3.5 meters, and the balls are about 10 centimeters in diameter. The carriage is constructed throughout of standard structural steel.
- 831. EMPLACEMENT.—The pit is 6 meters in diameter, and 1.5 meters in depth. In front of each mortar there is a concrete parapet



about 5 meters high, having a slope of about 45 degrees. A part of this parapet is shown at the left foreground of plate 529, and is evidently a continuation of the concrete storehouse which is covered with earth.

832. Ammunition Supply System.—The ammunition supply system is shown on plate 529. Between the shell table and the road, a narrow gauge line can be seen, which leads to the main storehouse. At the end of the shell table on the concrete floor there are guides to place the shot truck in loading projectiles from the table. It is assumed that the mortars were loaded at zero elevation, although this is not certain. The shot truck is similar in design to those used with the 38-centimeter guns and shown on plate 505. Since the powder charge was not of great weight, it is probable that it was carried in a two-man tray.

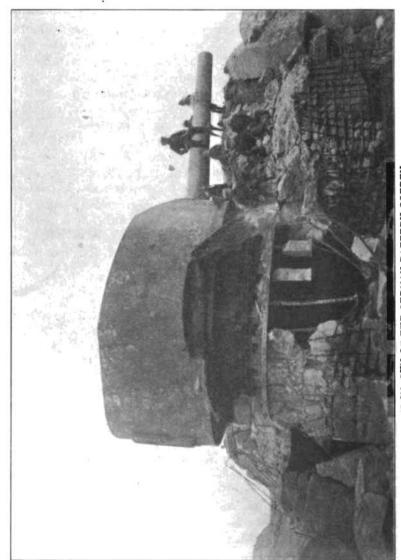
833. Protection.—The only protection afforded these mortars has been mentioned under "emplacement." There was no evidence of any camouflaging, although it is assumed that some sort of camouflage was provided. Air photographs taken in 1916 revealed the presence of these mortars, and it is quite certain that no amount of camouflage could effectively conceal them. There is no evidence, however, that any of them had ever been either struck or damaged by shell fire or bombs.

17-CENTIMETER GUN, BATTERY GOEBEN.

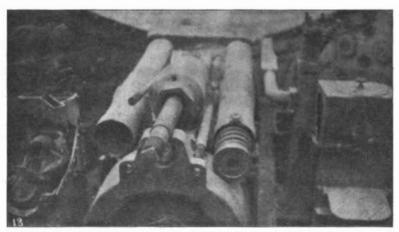
834. Gun.—All of the guns of this battery, plate 530, are model 1914, and the gun examined in detail is model 1914, No. 71-L. Its weight is 10,701 kilograms, the length of the tube 6.44 meters, and the total length of the gun is 6.980 meters. There are 52 grooves, and the twist of the rifling is to the right 1 centimeter in 10 centimeters. The diameter of the powder chamber is 19 centimeters and the breech is of the standard Krupp sliding-wedge type.

835. CRADLE.—The cradle is identical in design with the cradle found with the 21-centimeter railway mount. There are two hydraulic buffer cylinders, one on the top and the other directly below the cradle, and each is attached to the cradle by a heavy pin, about which it can rotate in a vertical plane. Four spring cylinders are arranged about the cradle symmetrically, two above and two below. The design of this type of cradle is shown on plate 374. The diameter of the trunnions is 22 centimeters and the length 15 centimeters. The antifriction device is of the design shown for the 15-centimeter guns on plate 535.

836. RECOIL MECHANISM.—The outside diameter of the recoil cylinder, plate 531, is 25 centimeters and the estimated length of recoil 40 centimeters. As noted before, the recuperator cylinders are four in number and they are 1.6 meters in length. There are two columns of springs in each cylinder, the mean diameter of the outside



17 CM. GUN OF THE GERMAN BATTERY GOEBEN.



CRADLE RECOIL CYLINDERS AND RECUPERATORS OF THE 17 CM. BATTERY GOEBEN.

spring being 17 centimeters, diameter of wire 2.4 centimeters, and the pitch 5 centimeters. The mean diameter of the inside spring is 11 centimeters, the diameter of the wire 1.5 centimeters, and the pitch 3 centimeters. Tension rods connect the crosshead at the front of each spring column with the recoil lug.

837. ELEVATING MECHANISM.—The elevating mechanism includes a circular rack bolted to the side of the gun near the breech. The pinion meshing with this rack is driven by an electric motor carried on the part of the carriage below the floor.

838. Thaversing Mechanism.—A complete circular rack is attached to the base ring. The traversing motor is carried on the section of the top carriage which extends below the deck and connects with the traversing rack through two sets of bevel gears and one spur gear. The entire original gun and turret mechanism, without any modifications, were installed on the concrete emplacement as shown on plate 530.

839. Carriage.—The one detail of the carriage which seems of interest to describe is the traversing ball bearing. A portion of the light shield protecting the bearing has been torn away approximately at the center of the turret and almost above the long-exposed anchor bolt. It was found on removing this shield that the carriage is provided with a double ball path, the diameter of the outer path being 3.2 meters and the inner path 2.8 meters. The balls in the outside bearing are about 5 centimeters in diameter and in the inside bearing 7.5 centimeters.

840. EMPLACEMENT.—These guns, all placed in the shore dunes at Zeebrugge, are easily visible from the sea. The concrete emplacement shown on plate 530 is about level with the top of the dune. A railway line, evidently constructed by the Germans, runs along the top of the dune just in front of the gun. The thickness of the concrete wall at the rear is about 1.5 meters. This wall increased in thickness on the sides to several meters, flaring off to the right and left at the front. There was a door leading into the operating room under the turret just under the two short anchor bolts seen in the center of the picture.

841. Ammunition Supply System.—Ammunition was supplied to the gun through the door just mentioned in the emplacement and was hoisted by the usual type of electrical turret hoist. Apparently there was no provision for supplying ammunition in any other way.

842. Protection.—All of the guns were protected as shown in plate 530. This turnet was made up of 10-centimeter armor.

843. DESTRUCTION.—Apparently the usual scheme of destroying the gun was not employed in these cases. Instead, by some method they detonated a number of projectiles inside the turret and in the operating room below. All but one of the emplacements was de-

stroyed as badly as the one in the plate. In each case the roof of the turret was blown off. The explosions which destroyed the emplacements do not seem to have destroyed the turret mechanism, as one would have expected. In the case of the gun shown there were about half a dozen unexploded projectiles in the turret and twice that number in the operating room below. All of these projectiles were of the design shown on plate 532.

15-CENTIMETER GUN, BATTERY IRENE.

844. Gun.—All of the guns of the Battery Irene, plate 533, are of the model 1900, and the gun inspected is model 1900, No. 478-L. The weight is 4,861 kilograms, the total length 6 meters, and the length of the tube to the face of the breechblock 5.57 meters. The number of grooves is 44 and the twist of the rifling is to the right 1 centimeter in 10 centimeters. The diameter of the powder chamber is 18 centimeters. The breechblock is of the standard Krupp sliding wedge type.

845. Cradle.—The cradle, which is not unusual in design, is shown on plate 534. The trunnions are provided with an antifriction device of the design shown on plate 535. Two lugs are cast on the bottom of the cradle near the rear to which the recoil piston is attached by means of a pin. Two other lugs are provided to which the spring recuperator cylinders are bolted.

846. Recoil Mechanism.—Attention is called to the rather unique design of the recoil mechanism. This is the only case observed in which the cylinder is carried in the breech lug, the piston being attached to the cradle by means of a pin passing through the two lugs just mentioned. The recuperator cylinders are two in number. Two 3-centimeter tension rods connect the breech lug with the crosshead at the forward end of the spring cylinders. These recuperator cylinders are faced off on the inside at the rear to serve as a guide for the breech lug to prevent rotation of the gun.

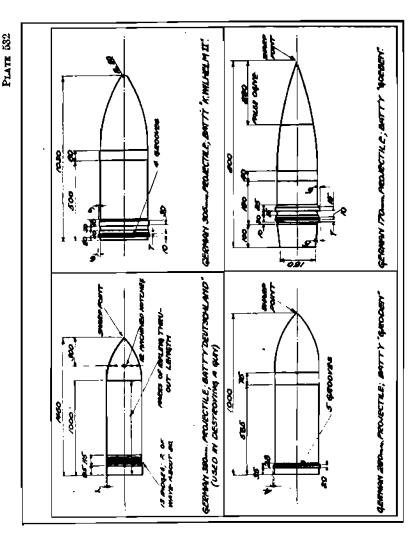
847. ELEVATING MECHANISM, TRAVERSING MECHANISM, CARRIAGE EMPLACEMENT, AMMUNITION SUPPLY SYSTEM, PROTECTION.—There are no features of any of these items that are worthy of description.

848. On the inside of the armor of another carriage of identical design, but of the Battery Kaiserin, near Blankenburg, there was printed firing data, as shown on plate 536.

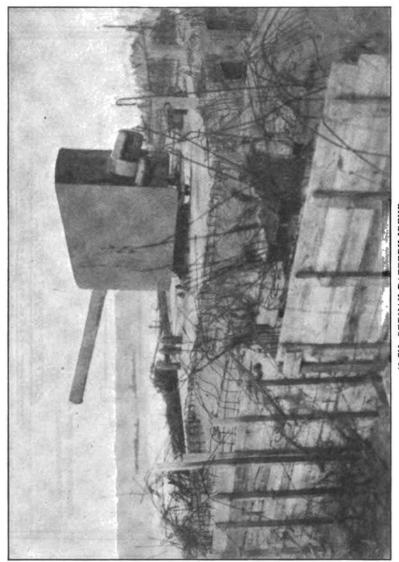
CONCLUSIONS.

849. Gun.—Most of the guns inspected are about 42 calibers in length, measuring from the face of the breechblock, or about 45 calibers in total length. All guns are provided with the standard Krupp type of sliding wedge breechblock. In all cases, except with the 28 centimeter mortars, which are model 1892, the twist of the rifling is uniform to the right 1 centimeter in 10 centimeters. There

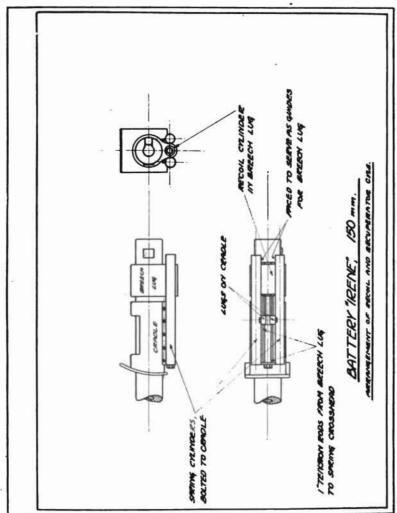




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15 CM. GERMAN BATTERY IRENE.



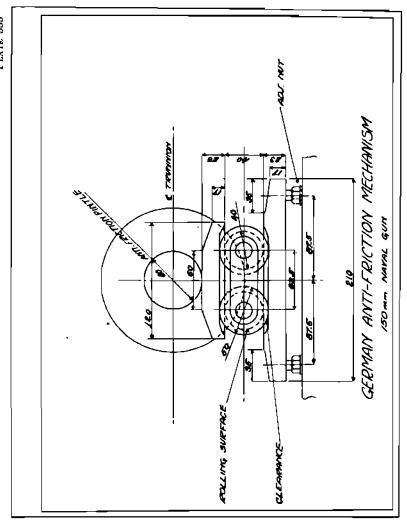


PLATE 535

PLATE 536

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FIRING DATA PAINTED ON THE SHIELDS OF THE 15 CM, GERMAN GUNS.

are no guns older than 1904. Quite a number of the guns are as late as 1916. If the data given in the Bulletin de Renseignement d'Artillerie of January-February, 1919, can be accepted, it is certain that the Germans were securing ranges from these guns at ordinary muzzle velocity far in excess of the ranges that we are securing from our guns. This is probably through the improvement in their projectile design.

850. CRADLES.—All cradles constructed may be termed smooth cylinders, and the maximum thickness of the walls is 10 centimeters. The cradles of the larger guns are provided with bronze liners about 6 millimeters thick and 1 meter long, at both forward and rear ends. In all cases, the cradles are provided with the simplest types of brackets for the attaching of the recuperator and recoil cylinders.

851. Provision to Prevent Rotation of the Gun.—All breech lugs are fastened to the gun by the interrupted ring method. All lugs are so shaped as to bear either between two recuperator cylinders or on two sides of a single recuperator cylinder to prevent rotation of the gun. There is no evidence in any case of the use of the spline, typical in American design, for the prevention of rotation of the gun.

852. Hydraulic Buffers.—In most cases, two hydraulic buffers are provided. Apparently, there is no fixed policy of balancing these since, in many cases, the two cylinders are located on the bottom of the cradle. In some cases, the hydraulic cylinders are provided with extensions on the forward end which are evidently counterrecoil buffers. In a number of other cases, no such extensions are visible.

853. RECUPERATORS.—The designers seem to have favored the combined air-spring recuperators for the heavy guns. There is no attempt at balancing them, and the number of cylinders varies from one to four. All of the 380 and 305 millimeter guns are provided with only one recuperator cylinder each. As noted under the heading of "Rotation of gun," in every case the recuperator cylinders are used as guides for the extension of the breech lug to prevent rotation of the gun.

854. Gun Carriage—Traversing Mechanism.—In all cases, the heavy gun carriages are constructed entirely of structural steel, and with the exception of the 28-centimeter mortar carriages, are of the front pintle type. The pintle bearings in all cases are ball bearing and there is only one case of actual provision for direct contact between the racer and base ring for transmission of the horizontal force of recoil into the emplacement. The rear of the carriages is carried on heavy rollers (two to four in number, 10 to 20 centimeters across the face and 0.60 to 1 meter in diameter) running on circular tracks set in the concrete emplacement. In some cases (38-centimeter guns) the traversing pinion meshes with a rack attached to the roller path. In other cases (380 and 305 millimeter guns) the traversing pinion meshes with gears bolted to the face of the rollers.

855. ELEVATING MECHANISM.—The variations in the design of the elevating mechanism found on German coast carriages as well as railway carriages is very striking. On the 38-centimeter railway mount found at Brussels, and the 305-millimeter carriages of the Battery Kaiser Wilhelm II, there are double straight racks, but the dimensions and designs differ quite radically. With the 38-centimeter guns of the Batteries Pommern and Deutschland, there are double-telescoping screws. On the Battery Tirpitz there is a double-curved rack attached to the bottom of the cradle. On the Battery Croden, 28-centimeter mortars and the guns of several other batteries, there are single-curved racks attached to the bottom of the cradle. On the Battery Coeben, 17-centimeter guns, circular racks are attached to the sides of the cradles.

856. Ammunition Supply System.—In all cases, the ammunition is conveyed from the storehouses into the gun by hand. The shot trucks are all of extremely simple design, and the projectiles in all cases are rammed by hand.

857. AMMUNITION STORAGE.—With all of the heavier batteries, the layout of the ammunition storehouses is as shown on plates 557 and 558. In each case, the storehouses are designed to house projectiles and powder for the main guns as well as ammunition for the anti-aircraft guns provided for the protection of each of the big batteries.

858. Protection.—It is very significant that there is no evidence of a policy of providing heavy protection for these large caliber and valuable guns. Apparently, all of the guns which are provided with the 6-centimeter flat plate armor have been removed from other coast fortifications where they had been previously provided with the same armor. Nearly all of the guns were elaborately camouflaged, but air photographs taken in 1916, 1917, and 1918 show quite clearly the positions of all of the guns, ammunition storehouses, approach tracks, etc.

859. In spite of the lack of protection and the clear evidence of the position of the batteries from air photographs, there is no evidence that any of the guns was ever damaged, or even hit, by shell fire or by bombs from airplanes. It is understood that the coast fortifications were shelled constantly by the heavy guns of the Allies' monitors. The positions of the guns were known, but either the smoke screens that were at once put up by the Germans were unusually effective, or the systems of fire control that were employed were defective. The reasons for the failure of the aviators to obtain any satisfactory results are not certain. They dropped many bombs in the vicinity of the various batteries. It is probable that the accuracy of the antiaircraft guns provided with all of the large batteries was such as to compel the aviators to operate at a very great height.

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- 37. See also "Camouflage for Railway Mounts," Journal of the United States Artillery, May, 1919.
- 38. Original recommendation with reference to shop equipment submitted by Maj. Ralph Plumb, commanding officer of the R. A. R. repair shop, Haussimont, France.
- 39. War Department Document No. 967.
- See also Report of Heavy Artillery Board, A. E. F., dated Aug. 16, 1918, on "Equipment for the 12-inch Batignolles Railway Mount," signed H. S. Miller, Lt. Col. C. A. C.; Library, Fort Monroe.
- 41. A more complete treatment on Clearance Diagrams, with maps and diagrams of all of the principal American railways has been made up by the Railway and Seacoast Carriage Section, Artillery Division of the Ordnance Department; copies on file, Library, Fort Monroe; Office Chief of Coast Artillery.
- 42. See "Table of United States Army Cannon and Projectiles," Ordnance Pamphlet No. 1676; "Elements of United States Naval Guns," Navy Bureau of Ordnance; "Super-Heavy Flat Trajectory Guns" (German; see reference 30 above.)
- 43. See also "L'Illustration" (French) for Jan. 4, 1919. See "Genie Civil" (French) for Apr. 20, 1918, for reconstitution and measurement of projectiles. Analyses of projectile made in laboratory of Andre Citroen, Paris. Fragments of projectiles in Museum of Municipal Laboratory in Paris.
- 44. See also "Journal of the United States Artillery," June, July, August and December, 1919.
- 45. See also "L'Illustration" (French) for Jan. 4, 1919.

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